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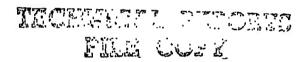
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ANALYSIS AND COMPUTER PROGRAM FOR EVALUATION OF AIRBREATHING PROPULSION EXHAUST NOZZLE PERFORMANCE

S. Wehofer and W. C. Moger ARO, Inc.

May 1973



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FOREWORD

The work reported herein was conducted at the Arnold Engineering Development Center (AEDC). The initial development of the work was sponsored by the Air Force Aerospace Propulsion Laboratory (AFAPL), Air Force Systems Command (AFSC), Wright-Patterson Air Force Base, Ohio. The final phase of the work was sponsored by the Air Force Flight Dynamics Laboratory (AFFDL), Air Force Systems Command (AFSC), Wright-Patterson Air Force Base, Ohio, under Program Element 65401F.

The results of the research presented were obtained by ARO, Inc. (a subsidiary of Sverdrup & Parcel and Associates, Inc.) contract operator of AEDC, AFSC. The bulk of the research was conducted from January 1969 to June 1970 under Project Number RD0850. Refinement and extension of the work was conducted from July 1970 to June 1971 under Project Number RW5113, and from July 1971 to the present under ARO Project Number RF242. This report was submitted for publication on November 30, 1972.

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This technical report has been reviewed and is approved.

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ABSTRACT

An analytical technique based on the time-dependent flow equations has been developed to predict the inviscid transonic flow field in axisymmetric propulsion nozzles. The analysis includes the treatment of axisymmetric nonuniform nozzle inlet profiles of total pressure, total temperature, specific heat, and molecular weight. The analysis is also capable of considering convergent-divergent, convergent, and shrouded or unshrouded plug nozzle geometries. A computer listing and three sample calculations are presented to illustrate some of the capabilities of the program.

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NOMENCLATURE

A Cross-sectional area

a, b, c Constants in expression for specific heat

CD Discharge coefficient

CF Thrust coefficient

cp Specific heat at constant pressure

c_p Specific heat at constant pressur
 c_v Specific heat at constant volume

D Diameter

E Internal energy per unit volume

e Energy per unit volume

l
Time station index

M Mach number or downstream boundary axial station

m Axial station index

n Radial station index
P Static pressure

P Static pressure
Po Total pressure

R Gas constant

R_c Normalized radius of wall curvature (radius of

curvature/throat radius)

r Radial distance from nozzle centerline

si Radial coordinate of nozzle centerbody

so Radial coordinate of nozzle wall

T Static temperature

Total temperature

t Time

u Axial velocity component

V Vector velocity

v Radial velocity component

W, F, G, H Variables

W_f Weight flow

w Tangential velocity

x Axial distance from nozzle inlet

y Transformed radial coordinate

Δ Small increment

 θ Flow angle

ρ Density

SUBSCRIPTS

1-D One dimensional

g Gas w Wall

[®] Ambient

SUPERSCRIPTS

* Sonic

Differentiation with respect to x

SECTION I

An analytical method for predicting the exhaust nozzle performance of airbreathing propulsion systems must consider a wide variety of flow conditions for both convergent-divergent and convergent conical nozzle geometries. There are several analytical analyses available (i. e., Refs. 1, 2, and 3) which can be used to evaluate the performance of some turbojet nozzle flow fields. Unfortunately, there are inherent limitations in the analytical approaches generally available to systems groups which preclude their use in the quantitative evaluation of some of today's turbojet nozzle flows. One of the most restrictive features is that the flow is assumed to have uniform flow stagnation conditions and gas properties. The purpose of the present work was to develop a computer program to predict the inviscid subsonic-transonic flow field for actual operating conditions in axisymmetric turbine engine exhaust nozzles.

The most logical candidate for solving the general nozzle flow field is the direct numerical integration of the main governing differential equations - continuity, axial and radial momentum, and energy. The equations are posed in time-dependent form and use a Lax-Wendroff (L-W) (Ref. 4) finite differencing scheme. The present computation method was adopted after the work presented in Ref. 5. The first version of the present computer program was reported in Ref. 6. Since publication of Ref. 6, a centerbody option has been added to the program, and the analysis has been extended to evaluate flow fields for both subsonic and supersonic nozzles. Also, several programming improvements have been made to reduce machine time requirements and to improve the accuracy near the boundaries.

This report presents the method of analysis, a description of the numerical scheme, and a description of the program boundary conditions. Sample calculations for a supersonic convergent-divergent, plug, and unchoked convergent-divergent nozzle are presented. A complete computer listing is presented in Appendix VI.

SECTION II METHOD OF ANALYSIS

The fluid is assumed to be inviscid, non-heat conducting, and thermally perfect. The flow field is assumed to be axisymmetric. The general solution consists of solving the following relations:

Continuity:

$$\frac{\partial}{\partial t} (\rho r) + \frac{\partial}{\partial x} (\rho u r) + \frac{\partial}{\partial r} (r \rho v) = 0$$
 (2.1a)

Axial Momentum:

$$\rho \frac{\partial}{\partial t} (ur) + \rho u \frac{\partial}{\partial x} (ur) + \rho v r \frac{\partial u}{\partial r} = -\frac{\partial}{\partial x} (Pr)$$
 (2. 1b)

Radial Momentum:

$$\rho \frac{\partial}{\partial t} (vr) + \rho u \frac{\partial}{\partial x} (vr) + \rho v r \frac{\partial v}{\partial r} - \rho w^2 = -r \frac{\partial P}{\partial r}$$
 (2.1c)

Tangential Momentum:

$$\rho \frac{\partial}{\partial t} (wr) + \rho u \frac{\partial}{\partial x} (wr) + \rho vr \frac{\partial w}{\partial r} + \rho vw = 0$$
 (2.1d)

Energy:

$$\frac{\partial}{\partial t}(er) + \frac{\partial}{\partial x}[(e+P)ur] + \frac{\partial}{\partial r}[(e+P)vr] = 0$$
 (2.1e)

¹While this expression is included in the derivation, the tangential velocity has not been added to the computer program.

Multiplying the continuity equation (2.1a) by u, v, and w successively and adding each expression successively with (2.1b), (2.1c), and (2.1d), give

$$\frac{\partial}{\partial t} (\rho u r) + \frac{\partial}{\partial x} (\rho u^2 r) + \frac{\partial}{\partial r} (\rho u v r) = -\frac{\partial}{\partial x} (P r) \qquad (2.2a)$$

$$\frac{\partial}{\partial t} (\rho v r) + \frac{\partial}{\partial x} (\rho u v r) + \frac{\partial}{\partial r} (\rho v^2 r) = -\frac{\partial}{\partial r} (P r) + P + \rho w^2 \qquad (2.2b)$$

$$\frac{\partial}{\partial t}(\rho wr) + \frac{\partial}{\partial x}(\rho uwr) + \frac{\partial}{\partial r}(\rho vwr) = -\rho vw \qquad (2.2c)$$

Letting

$$h = \rho r$$
, $d = \rho u r$, $k = \rho v r$,
 $z = \rho w r$, $f = e r$, $q = P r$ (2.3a)

and noting that

$$\frac{d^2}{h} = \rho u^2 r , \frac{k^2}{h} = \rho v^2 r , \frac{dk}{h} = \rho u v r , \frac{dz}{h} = \rho u w r ,$$

$$\frac{kz}{h} = \rho v w r , \frac{z^2}{h r} = \rho w^2 , \frac{kz}{h r} = \rho v w$$
(2.3b)

then Eqs. (2.1a), (2.1e), (2.2a), (2.2b), and (2.2c) can be written as

$$\frac{\partial h}{\partial t} + \frac{\partial d}{\partial x} + \frac{\partial k}{\partial r} = 0 ag{2.4a}$$

$$\frac{\partial^{d}}{\partial t} + \frac{\partial}{\partial x} \left(\frac{d^{2}}{h} + q \right) + \frac{\partial}{\partial r} \left(\frac{dk}{h} \right) = 0$$
 (2.4b)

$$\frac{\partial k}{\partial t} + \frac{\partial}{\partial x} \left(\frac{dk}{h} \right) + \frac{\partial}{\partial r} \left(\frac{k^2}{h} + q \right) = \frac{q}{r} + \frac{z^2}{hr}$$
 (2.4c)

$$\frac{\partial z}{\partial t} + \frac{\partial}{\partial x} \left(\frac{dz}{h}\right) - \frac{\partial}{\partial r} \left(\frac{kz}{h}\right) = -\frac{kz}{hr}$$
 (2.4d)

$$\frac{\partial f}{\partial t} + \frac{\partial}{\partial x} \left[(f + q) \frac{d}{h} \right] + \frac{\partial}{\partial r} \left[(f + q) \frac{k}{h} \right] = 0$$
 (2.4e)

These are the desired conservation forms for the main differential equations. Next, these conservation forms will be expressed as one single vector equation.

2.1 VECTOR FORM OF CONSERVATION EQUATIONS

Using a second order polynominal to represent the specific heat temperature relation gives

$$c_n(T) = a + bT + cT^2$$
 (2.5)

and from the definition of E

$$E = \frac{e}{\rho} - \frac{V^2}{2} \tag{2.6}$$

the equation of state may be written as,

$$E = \int c_{v} dT = \frac{P}{\rho} \left(\frac{a}{R_{g}} - 1 \right) + \left(\frac{P}{\rho} \right)^{2} \frac{b}{2R_{g}^{2}} + \left(\frac{P}{\rho} \right)^{3} \frac{c}{3R_{g}^{3}}$$
 (2.7)

Now noting from Eq. (2.3) that

$$V^2 = \frac{d^2 + k^2 + z^2}{h^2} \tag{2.8}$$

Then Eq. (2.6) may be written as

$$q(\frac{a}{R_g}-1) + \frac{b}{2R_g^2} + \frac{q^2}{h} + \frac{c}{3R_g^3} + \frac{q^3}{h^2} = f - \frac{1}{2} + \frac{d^2 + k^2 + z^2}{h}$$
 (2.9)

This relation shows that q can be expressed in terms of only the variables appearing in the first terms of Eq. (2.4).

Now consider four vectors (W, F, G, and H) defined by the variables h, d, k, z, and f. Let these vectors be defined by the following components:

From these definitions and Eq. (2.9), it is seen that the vectors F, G, and H are a function of W. Therefore, the conservation forms of Eq. (2.4) may be expressed in terms of the above vectors as one single vector equation.

$$\frac{\partial}{\partial t} W + \frac{\partial}{\partial x} F(W) + \frac{\partial}{\partial r} G(W) = H(W)$$
 (2.11)

The system (2.11) is called the conservation-law form.

2.2 FINITE DIFFERENCING SCHEME (LAX-WENDROFF)

The components of the vectors in Eq. (2.11) from Eq. (2.10) can also be written as

$$\begin{split} &W_1 = h \ , \ W_2 = d \ , \ W_3 = k \ , \ W_4 = z \ , \ W_5 = f \\ &F_1 = W_2 \ , \ F_2 = \frac{W_2^2}{W_1} + q \ , \ F_3 = \frac{W_2W_3}{W_1} \ , \ F_4 = \frac{W_2W_4}{W_1} \ , \ F_5 = \frac{W_2}{W_1}(W_5 + q) \\ &G_1 = W_3 \ , \ G_2 = \frac{W_2W_3}{W_1} \ , \ G_3 = \frac{W_3^2}{W_1} + q \ , \ G_4 = \frac{W_3W_4}{W_1} \ , \ G_5 = \frac{W_3}{W_1}(W_5 + q) \\ &H_1 = 0 \ , \ H_2 = 0 \ , \ H_3 = \frac{W_4^2}{W_1} + \frac{q}{r} \ , \ H_4 = -\frac{W_3W_4}{W_1} \ , \ H_5 = 0 \end{split}$$

Also from Eq. (2.9),

$$q(\frac{q}{R_g}-1) + \frac{b}{2R_g^2} \frac{q^2}{W_1} + \frac{c}{3R_g^3} \frac{q^3}{W_1^2} = W_5 - \frac{W_2^2 + W_3^2 + W_4^2}{2W_1}$$
 (2.13)

Let $W_{m,\,n}^{\ell}$ represent the function $W(t+\ell\Delta t,\,x+m\Delta x,\,r+n\Delta r)$ where ℓ , m, n can be integers or $\pm 1/2$. $F(W_{m,\,n}^{\ell})$ will be abbreviated by $F_{m,\,n}^{\ell}$. Finally, $<\!W\!>_{m,\,n}^{\ell}$ will stand for the difference approximation to the partial derivative, W_t , centered at ℓ , m, n.

All functions are assumed to be known at the grid points of the initial data surface, $\ell = 0$. The function W can then be calculated at $\ell = 1$ by a forward difference scheme. Second-order accuracy is achieved if the differences are centered at $(t + \frac{\Delta t}{2}, x, r)$. Thus, the difference approximation to Eq. (2.11) reads:

$$\langle \overline{W}_{1} \rangle_{0,0}^{\frac{1}{2}} = -\langle F_{x} \rangle_{0,0}^{\frac{1}{2}} - \langle G_{y} \rangle_{0,0}^{\frac{1}{2}} + \langle H_{y} \rangle_{0,0}^{\frac{1}{2}}$$
 (2.14a)

where

$$\langle W_{t} \rangle_{0,0}^{\frac{1}{2}} = \frac{1}{\Delta t} (W_{0,0}^{1} - W_{0,0}^{0}) , \langle F_{x} \rangle_{0,0}^{\frac{1}{2}} = \frac{1}{\Delta x} (F_{\frac{1}{2},0}^{\frac{1}{2}} - F_{-\frac{1}{2},0}^{\frac{1}{2}}) , \langle G_{p} \rangle_{0,0}^{\frac{1}{2}} = \frac{1}{\Delta r} (G_{0,\frac{1}{2}}^{\frac{1}{2}} - G_{0,-\frac{1}{2}}^{\frac{1}{2}})$$

$$(2.14b)$$

Substituting Eq. (2.14b) into Eq. (2.14a) gives

$$W_{0,0}^{1} = W_{0,0}^{0} + \Delta t \left[-\frac{1}{\Delta x} (F_{\frac{1}{2},0}^{\frac{1}{2}} - F_{-\frac{1}{2},0}^{\frac{1}{2}}) - \frac{1}{\Delta r} (G_{0,\frac{1}{2}}^{\frac{1}{2}} - G_{0,-\frac{1}{2}}^{\frac{1}{2}}) + H_{0,0}^{\frac{1}{2}} \right]$$
 (2.15)

To calculate the function $F_{\pm 1/2,\,0}^{1/2}$, etc., first the calculation of $W_{\pm 1/2,\,0}^{1/2}$, $W_{0,\,\pm 1/2}^{1/2}$, and $W_{0,\,0}^{1/2}$ is required. These terms can be obtained from a truncated Taylor series expansion as

$$W(t + \frac{\Delta t}{2}, x \pm \frac{\Delta x}{2}, r) = W(t, x \pm \frac{\Delta x}{2}, r) + \frac{\Delta t}{2} W_t(t, x \pm \frac{\Delta x}{2}, r)$$
 (2.16a)

$$W(t + \frac{\Delta t}{2}, x, r \pm \frac{\Delta r}{2}) = W(t, x, r \pm \frac{\Delta r}{2}) + \frac{\Delta t}{2} W_t(t, x, r \pm \frac{\Delta r}{2})$$
 (2.16b)

$$W(t + \frac{\Delta t}{2}, x, r) = W(t, x, r) + \frac{\Delta t}{2} W_t(t, x, r)$$
 (2.16c)

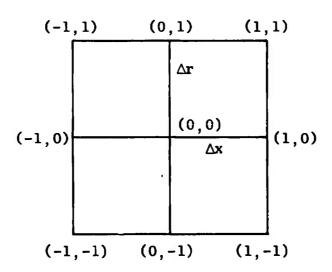
Here the first terms of Eq. (2.16a) can be taken as the average of $W_{0,0}^0$ and $W_{\pm 1,0}$. Similarly, the first term of Eq. (2.16b) can be taken as the average of $W_{0,0}^0$ and $W_{0,\pm 1}^0$. The first term of Eq. (2.16c) is assumed given by

$$W_{0,0}^0 = \frac{1}{4}(W_{1,0}^0 + W_{-1,0}^0 + W_{0,1}^0 + W_{0,-1}^0)$$

The second term in Eq. (2.16) can be replaced by spatial derivatives using the differential equation (2.11). In this way the following equations are obtained:

$$\begin{split} & W_{\pm^{1}_{2,0}}^{\frac{1}{2}} = \frac{1}{2} (W_{0,0}^{0} + W_{\pm^{1},0}^{0}) + \frac{\Delta_{t}}{2} [-\langle F_{x} \rangle_{\pm^{1}_{2,0}}^{0} - \langle G_{r} \rangle_{\pm^{1}_{2,0}}^{0} + \langle H \rangle_{\pm^{1}_{2,0}}^{0}] \\ & W_{0,\pm^{\frac{1}{2}}_{2}}^{\frac{1}{2}} = \frac{1}{2} (W_{0,0}^{0} + W_{0,\pm^{1}}^{0}) + \frac{\Delta_{t}}{2} [-\langle F_{x} \rangle_{0,\pm^{\frac{1}{2}}_{2}}^{0} - \langle G_{r} \rangle_{0,\pm^{\frac{1}{2}}_{2}}^{0} + \langle H \rangle_{0,\pm^{\frac{1}{2}}_{2}}^{0}] \\ & W_{0,0}^{\frac{1}{2}} = \frac{1}{4} (W_{1,0}^{0} + W_{-1,0}^{0} + W_{0,1}^{0} + W_{0,-1}^{0}) + \frac{\Delta_{t}}{2} [-\langle F_{x} \rangle_{0,0}^{0} - \langle G_{r} \rangle_{0,0}^{0} + H_{0,0}^{0}] \end{split}$$

Now approximate the derivatives by difference quotients (refer to the sketch below):



Sketch Showing the Grid Points and the Values of Indices (m and n) around a Point (m = n = 0)

$$\langle F_{x} \rangle_{\pm \frac{1}{2},0}^{0} = \pm \frac{1}{\Delta x} (F_{\pm 1,0}^{0} - F_{0,0}^{0})$$

$$\langle G_{r} \rangle_{\pm \frac{1}{2},0}^{0} = \frac{1}{2\Delta r} \left(\frac{G_{0,1}^{0} + G_{\pm 1,1}^{0}}{2} - \frac{G_{0,-1}^{0} + G_{\pm 1,-1}^{0}}{2} \right)$$

$$= \frac{1}{4\Delta r} (G_{0,1}^{0} + G_{\pm 1,1}^{0} - G_{0,-1}^{0} - G_{\pm 1,-1}^{0})$$

$$\langle F_{x} \rangle_{0,\pm \frac{1}{2}}^{0} = \frac{1}{2\Delta x} \left(\frac{F_{1,0}^{0} + F_{1,\pm 1}^{0}}{2} - \frac{F_{-1,0}^{0} + F_{-1,\pm 1}^{0}}{2} \right)$$

$$= \frac{1}{4\Delta x} (F_{1,0}^{0} + F_{1,\pm 1}^{0} - F_{-1,0}^{0} - F_{-1,\pm 1}^{0})$$

$$\langle G_{r} \rangle_{0,\pm \frac{1}{2}}^{0} = \pm \frac{1}{\Delta r} (G_{0,\pm 1}^{0} - G_{0,0}^{0})$$

$$\langle F_{x} \rangle_{0,0}^{0} = \frac{1}{2\Delta r} (F_{1,0}^{0} - F_{-1,0}^{0})$$

$$\langle G_{r} \rangle_{0,0}^{0} = \frac{1}{2\Delta r} (G_{0,1}^{0} - G_{0,-1}^{0})$$

and

Substituting Eqs. (2.18a) and (2.18b) into Eq. (2.17) gives

$$\begin{split} \mathbb{W}_{\pm 1/2,0}^{1/2} &= \frac{1}{2} (\mathbb{W}_{0,0}^{0} + \mathbb{W}_{\pm 1,0}^{0}) \pm \frac{1}{2} \frac{\Delta_{t}}{\Delta_{x}} (F_{\pm 1,0}^{0} - F_{0,0}^{0}) - \frac{1}{8} \frac{\Delta_{t}}{\Delta_{r}} (G_{0,1}^{0} + G_{\pm 1,1}^{0} - G_{0,-1}^{0} - G_{\pm 1,-1}^{0}) \\ &+ \frac{1}{4} \Delta_{t} (\mathbb{H}_{0,0}^{0} + \mathbb{H}_{\pm 1,0}^{0}) \\ \mathbb{W}_{0,\pm 1/2}^{1/2} &= \frac{1}{2} (\mathbb{W}_{0,0}^{0} + \mathbb{W}_{0,\pm 1}^{0}) - \frac{1}{8} \frac{\Delta_{t}}{\Delta_{x}} (F_{1,0}^{0} + F_{1,\pm 1}^{0} - F_{-1,0}^{0} - F_{-1,\pm 1}^{0}) \pm \frac{1}{2} \frac{\Delta_{t}}{\Delta_{r}} (G_{0,\pm 1}^{0} - G_{0,0}^{0}) \\ &+ \frac{1}{4} \Delta_{t} (\mathbb{H}_{0,0}^{0} + \mathbb{H}_{0,\pm 1}^{0}) \end{split} \tag{2.19b}$$

$$W_{0,0}^{\frac{1}{2}} = \frac{1}{4} (W_{1,0}^{0} + W_{-1,0}^{0} + W_{0,1}^{0} + W_{0,-1}^{0}) + \frac{\Delta t}{2} \left[-\frac{1}{2\Delta x} (F_{1,0}^{0} - F_{-1,0}^{0}) - \frac{1}{2\Delta r} (G_{0,1}^{0} - G_{0,-1}^{0}) + H_{0,0}^{0} \right]$$
(2. 19c)

(2.20c)

Finally, writing Eqs. (2.15) and (2.19) in the notations previously defined gives

$$\begin{split} \mathbb{W}(\ell+1,m,n) &= \mathbb{W}(\ell,m,n) + \Delta t \left\{ -\frac{1}{\Delta_x} \left[F(\ell+\frac{1}{2},m+\frac{1}{2},n) - F(\ell+\frac{1}{2},m-\frac{1}{2},n) \right] \right. \\ &- \frac{1}{\Delta_r} \left[G(\ell+\frac{1}{2},m,n+\frac{1}{2}) - G(\ell+\frac{1}{2},m,n-\frac{1}{2}) \right] + H(\ell+\frac{1}{2},m,n) \right\} \\ &- \frac{1}{\Delta_r} \left[G(\ell+\frac{1}{2},m,n+\frac{1}{2}) - G(\ell+\frac{1}{2},m,n-\frac{1}{2}) \right] + H(\ell+\frac{1}{2},m,n) \right\} \\ &- \mathbb{W}(\ell+\frac{1}{2},m\pm\frac{1}{2},n) &= \frac{1}{2} \left[\mathbb{W}(\ell,m,n) + \mathbb{W}(\ell,m\pm1,n) \right] + \frac{1}{2} \Delta t \left\{ \pm \frac{1}{\Delta_x} \left[F(\ell,m\pm1,n) - F(\ell,m,n) \right] \right. \\ &- \frac{1}{4} \frac{1}{\Delta_r} \left[G(\ell,m,n+1) + G(\ell,m\pm1,n+1) - G(\ell,m,n-1) - G(\ell,m\pm1,n-1) \right] \\ &+ \frac{1}{2} \left[H(\ell,m,n) + H(\ell,m\pm1,n) \right] \right\} \\ &+ \frac{1}{2} \left[H(\ell,m,n) + \mathbb{W}(\ell,m,n\pm1) \right] + \frac{1}{2} \Delta t \left\{ \pm \frac{1}{4} \frac{1}{\Delta_x} \left[F(\ell,m+1,n) + F(\ell,m+1,n\pm1) - F(\ell,m-1,n\pm1) \right] \right. \\ &- \left. F(\ell,m-1,n) - F(\ell,m-1,n\pm1) \right] = \frac{1}{\Delta_r} \left[G(\ell,m,n\pm1) - G(\ell,m,n) \right] \end{split}$$

 $+\frac{1}{2}[H(\ell,m,n) + H(\ell,m,n\pm 1)]$

and

$$\begin{split} \mathbb{W}(\ell_{+}\frac{1}{2},m,n) &= \frac{1}{4} \left[\mathbb{W}(\ell_{+}m+1,n) + \mathbb{W}(\ell_{+}m-1,n) + \mathbb{W}(\ell_{+}m,n+1) + \mathbb{W}(\ell_{+}m,n-1) \right. \\ &+ \frac{\Delta t}{2} \left\{ -\frac{1}{2\Delta x} \left[F(\ell_{+}m+1,n) - F(\ell_{+}m-1,n) \right] \right. \\ &- \frac{1}{2\Delta t} \left[G(\ell_{+}m,n+1) - G(\ell_{+}m,n-1) \right] + \mathbb{H}(\ell_{+}m,n) \right\} \end{split} \tag{2.20d}$$

SECTION III COORDINATE TRANSFORMATION

In Section II, the conservation-law form (2.11) was written in cylindrical coordinates $(x, r, and \theta)$. The finite difference net in these coordinates will be a rectangular lattice. Therefore, on the nozzle wall boundaries, the lattice points will not fall on the wall curve. One way to eliminate this difficulty is to use a variable net size near the boundaries, but this would considerably complicate the finite difference scheme. Another solution is to use a coordinate transformation from x, r to x, y such that the wall shape is expressed as y = const.

This transformation can be accomplished in the following manner: Let s = s(x) be a function describing the nozzle shape. Consider the coordinate transformation:

$$(x,r) \rightarrow \left(x,y = \frac{r - s_i(x)}{s_n(x) - s_i(x)}\right)$$
 (3.1)

Then,

$$\frac{\partial}{\partial x}\Big|_{r} = \frac{\partial}{\partial x}\Big|_{y} - \frac{\left[s_{i}' + y(s_{o}' - s_{i}')\right]}{s_{o} - s_{i}} \frac{\partial}{\partial y}$$

$$\frac{\partial}{\partial r} = \frac{1}{(s_{o} - s_{i})} \frac{\partial}{\partial y}$$
(3.2)

Substituting into Eq. (2.11) gives

$$\frac{\partial}{\partial t} W + \frac{\partial}{\partial x} F(W) - \frac{[s_i' + y(s_o' - s_i')]}{s_o - s_i} \frac{\partial}{\partial y} F(W) + \frac{1}{(s_o - s_i)} \frac{\partial}{\partial y} G(W) = H(W)$$
 (3.3)

It is seen from Eq. (3.1) that, in the x, y coordinate system, the wall shapes are expressed as

$$y_{wall} = constant$$
 (3.4)

and, therefore, a constant value of y can be maintained throughout the entire field and the logic of the computer program considerably reduced.

Let $W_{m,n}^{\ell}$ represent $W(t + \Delta \ell, x + m\Delta x, y + n\Delta y)$ in the x,y system. Also let m = 1 be the nozzle inlet

m = M be the downstream boundary

n = 0 be the centerbody wall

n = N be the outer nozzle wall

Then the finite difference form of Eq. (3.1) becomes

$$\langle W_1 \rangle_{0,0}^{\frac{1}{2}} = -\langle F_x \rangle_{0,0}^{\frac{1}{2}} + K_1 \langle F_y \rangle_{0,0}^{\frac{1}{2}} - K_2 \langle G_y \rangle_{0,0}^{\frac{1}{2}} + \langle H \rangle_{0,0}^{\frac{1}{2}}$$
 (3.5)

where the terms within the brackets are given in (2.14b) with the understanding that Δr is replaced by Δy

and

$$K_{1} = \frac{\left[s_{i}' + n\Delta y(s_{o}' - s_{i}')\right]}{s_{o} - s_{i}}$$

$$K_{2} = \frac{1}{s_{o} - s_{i}}$$

With the coordinate transformation, Eq. (2.15) becomes

$$W_{0,0}^{1} = W_{0,0}^{0} + \Delta t \left[-\frac{1}{\Delta x} \left(F_{0,0}^{\frac{1}{2}} - F_{-\frac{1}{2},0}^{\frac{1}{2}} \right) + K_{1} \frac{1}{\Delta y} \left(F_{0,\frac{1}{2}}^{\frac{1}{2}} - F_{0,-\frac{1}{2}}^{\frac{1}{2}} \right) \right]$$

$$- K_{2} \frac{1}{\Delta y} \left(G_{0,\frac{1}{2}}^{\frac{1}{2}} - G_{0,\frac{1}{2}}^{\frac{1}{2}} \right) + H_{0,0}^{\frac{1}{2}}$$

$$(3.6)$$

and Eq. (2.19) becomes

$$W_{\pm 1/2,0}^{1/2} = \frac{1}{2} (W_{0,0}^0 + W_{\pm 1,0}^0) \mp \frac{1}{2} \frac{\Delta t}{\Delta x} (F_{\pm 1,0}^0 - F_{0,0}^0) + K_1 \frac{\Delta t}{8\Delta y} (F_{0,1}^0 + F_{\pm 1,1}^0 - F_{0,-1}^0 - F_{\pm 1,1}^0) -K_2 \frac{\Delta t}{8\Delta y} (G_{0,1}^0 + G_{\pm 1,1}^0 - G_{0,-1}^0 - G_{\pm 1,-1}^0) + \frac{1}{4} \Delta t (H_{0,0}^0 + H_{\pm 1,0}^0)$$
(3. 7a)

$$W_{0,\pm !;i}^{1/2} = \frac{1}{2} \left(W_{0,0}^{0} + W_{0,\pm 1}^{0} \right) - \frac{\Delta \iota}{8\Delta x} \left(F_{1,0}^{0} + F_{1,\pm 1}^{0} - F_{-1,0}^{0} - F_{-1,\pm 1}^{0} \right) + \frac{\kappa_{1}}{2} \frac{\Delta \iota}{\Delta y} \left(F_{0,\pm 1}^{0} - F_{0,0}^{0} \right) - \frac{1}{2} \kappa_{2} \frac{\Delta \iota}{\Delta y} \left(G_{0,\pm 1}^{0} - G_{0,0}^{0} \right) + \frac{1}{4} \Delta \iota \left(H_{0,0}^{0} + H_{0,\pm 1}^{0} \right)$$

$$(3.7b)$$

$$W_{0,0}^{V_{0}'} = \frac{1}{4} (W_{1,0}^{0} + W_{-1,0}^{0} + W_{0,1}^{0} + W_{0,-1}^{0}) + \frac{\Delta t}{2} \left[-\frac{1}{2\Delta x} (F_{1,0}^{0} - F_{-1,0}^{0}) + \frac{K_{1}}{2\Delta y} (F_{0,1}^{0} - F_{0,-1}^{0}) - \frac{1}{2} \frac{K_{2}}{\Delta y} (G_{0,1}^{0} - G_{0,-1}^{0}) + H_{0,0}^{0} \right]$$

$$(3.7c)$$

The differencing scheme consists of the following two steps:

- 1. Calculate $W_{\pm 1/2, 0}^{1/2}$, $W_{0, \pm 1/2}^{1/2}$, and $W_{0, 0}^{1/2}$ using Eq. (3.7). From these results, evaluate $F_{\pm 1/2, 0}^{1/2}$, $G_{0, \pm 1/2}^{1/2}$, and $H_{0, 0}^{1/2}$ using the algebraic relations (2.13a) and (2.13b).
- 2. Introduce these functions together with $W_{0,0}^0$ into Eq. (3.6) to obtain $W_{0,0}^1$.

Examination of these steps reveals that the calculation of the components $W_{\hat{1}}$ at a point (m, n) on a time level ℓ + 1 required the components $W_{\hat{1}}$ at the points

$$(m,n)$$
, $(m \pm 1,n)$, $(m,n \pm 1)$, $(m \pm 1,n \pm 1)$

on the time level ℓ . That is, in order to calculate a new vector W at a point (m, n) on the time level $\ell + 1$, the values at point (m, n) and its eight nearest surrounding grid points on time level ℓ are required. Therefore, the scheme represents a 9-point forward difference scheme.

The above explanation shows that for every new time cycle the scheme cannot furnish values at the mesh points lying on the boundaries of the region where the flow is desired. As in all problems, these values must come from boundary conditions imposed on the flow.

SECTION IV BOUNDARY CONDITIONS

4.1 WALL BOUNDARIES

The values of W_i 's at the walls of the nozzle can be obtained from consideration that certain wall boundary conditions must be satisfied at steady state.

For the case of no swirl (i.e., W_4 = 0), Eqs. (2.1b) and (2.1c) can be solved for the pressure gradient normal to the nozzle walls. Rewriting Eqs. (2.1b) and (2.1c) for W_4 = 0 gives, respectively,

$$\frac{\partial}{\partial t} u + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial r} + \frac{1}{\rho} \frac{\partial P}{\partial x} = 0 \qquad (4.1)$$

$$\frac{\partial}{\partial t} v + u \frac{\partial v}{\partial x} + v \frac{\partial v}{\partial r} + \frac{1}{\rho} \frac{\partial P}{\partial r} = 0$$
 (4.2)

By making the coordinate transformation and noting that at the wall, Eq. (3.2) is given by

and

$$\frac{\partial}{\partial x}\Big|_{r} = \frac{\partial}{\partial x}\Big|_{y} - \frac{s'}{s_{o} - s_{i}} \frac{\partial}{\partial y}$$

$$\frac{\partial}{\partial r} = \frac{1}{s_{o} - s_{i}} \frac{\partial}{\partial y}$$
(4.3)

then Eqs. (4.1) and (4.2) become, respectively,

$$\frac{\partial \mathbf{u}}{\partial \mathbf{t}} + \mathbf{u} \left[\frac{\partial \mathbf{u}}{\partial \mathbf{x}} - \frac{\mathbf{s'}}{(\mathbf{s_0 - s_i})} \frac{\partial \mathbf{u}}{\partial \mathbf{y}} \right] + \frac{\mathbf{v}}{(\mathbf{s_0 - s_i})} \frac{\partial \mathbf{u}}{\partial \mathbf{y}} + \frac{1}{\rho} \left[\frac{\partial \mathbf{P}}{\partial \mathbf{x}} - \frac{\mathbf{s'}}{(\mathbf{s_0 - s_i})} \frac{\partial \mathbf{P}}{\partial \mathbf{y}} \right] = 0 \quad (4.4)$$

$$\frac{\partial \mathbf{v}}{\partial t} + \mathbf{u} \left[\frac{\partial \mathbf{v}}{\partial x} - \frac{\mathbf{s'}}{(\mathbf{s_0} - \mathbf{s_i})} \frac{\partial \mathbf{v}}{\partial y} \right] + \frac{\mathbf{v}}{(\mathbf{s_0} - \mathbf{s_i})} \frac{\partial \mathbf{v}}{\partial y} + \frac{1}{\rho(\mathbf{s_0} - \mathbf{s_i})} \frac{\partial \mathbf{P}}{\partial y} = 0 \tag{4.5}$$

However, at the walls, $s = \frac{v}{u}$, and $v = u \tan \theta$; therefore, Eqs. (4.4) and (4.5) can be written, respectively, as

$$\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \frac{\partial \mathbf{u}}{\partial x} + \frac{1}{\rho} \left[\frac{\partial \mathbf{P}}{\partial x} - \frac{\mathbf{s}'}{(\mathbf{s} - \mathbf{s})} \frac{\partial \mathbf{P}}{\partial y} \right] = 0 \tag{4.6}$$

and

$$\tan \theta \frac{\partial \mathbf{u}}{\partial \mathbf{t}} + \mathbf{u} \tan \theta \frac{\partial \mathbf{u}}{\partial \mathbf{x}} + \mathbf{u}^2 \sec^2 \theta \frac{\partial \theta}{\partial \mathbf{x}} + \frac{1}{\rho(\mathbf{s}_0 - \mathbf{s}_i)} \frac{\partial \mathbf{P}}{\partial \mathbf{y}} = 0 \tag{4.7}$$

Eliminating $\frac{\partial}{\partial t}$ u from Eqs. (4.6) and (4.7) gives

$$\frac{\partial}{\partial y} P = \frac{1}{2} \sin 2\theta_w (s_o - s_i) \frac{\partial}{\partial x} P - \rho u^2 (s_o - s_i) \frac{\partial}{\partial x} \theta_w \qquad (4.8)$$

Equation (4.8) can be written in finite difference form and used to evaluate the static pressure on both the nozzle outer wall and center-body. In order to define all of the variables on the boundaries, one more flow property must be calculated. Since the flow is inviscid and only the steady-state solution is of interest, the following isentropic relation can be used to solve for static temperature.

$$\frac{P_o}{P} = \left(\frac{T_o}{T}\right)^{a/R_g} \left[\frac{e^{\left(bT_o + \frac{c}{2} T_o^2\right)}}{\left(bT + \frac{c}{2} T^2\right)}\right]^{1/R_g}$$
(4.9)

The density is given by

$$\rho = \frac{P}{R_{\mu}T} \tag{4.10}$$

The velocity is given by

$$V = \left[2a(T_o - T) + b(T_o^2 - T^2) + \frac{2}{3}c(T_o^3 - T^3)\right]^{\frac{1}{2}}$$
 (4.11)

where

$$\mathbf{u} = \mathbf{V} \cos \theta \tag{4.12}$$

and

$$v = V \sin \theta \tag{4.13}$$

Hence, Eqs. (4.8) through (4.13) supply the wall boundary values.

The present analysis assumes that there is always a centerbody present. For nozzles without a centerbody, s_i can be made small with respect to the outer wall (i.e., $s_i < 0.01s_0^+$).

It should be noted that if Eq. (4.9) were applied along interior flow field streamlines, the energy equation (2.1e) could be eliminated entirely from the present solution. Elimination of the energy equation would reduce the computation time and should improve the numerical stability. However, with the energy equation, the present computer program can easily be extended to transfer of energy between streamlines.

4.2 DOWNSTREAM BOUNDARY CONDITION (CHOKED FLOW)

A coordinate line x = constant and m = M is chosen as the downstream boundary several grid stations downstream of the sonic line. In the case of a simple convergent conical nozzle, this may be done by initially assuming that the nozzle after the exit is extended through a short rounded throat section and a short divergent conical diffuser. Since the flow is entirely supersonic, no errors will be generated upstream from this end line. A linear extrapolation will be sufficient to obtain flow properties at the downstream boundary. The extrapolation formula used is

$$P_{M} = 2P_{M-1} - P_{M-2}$$

4.3 DOWNSTREAM BOUNDARY CONDITION (UNCHOKED FLOW)

For subsonic flow, the radial distribution of static pressure and flow angle at the downstream boundary are input. From these two properties, all other flow variables can be defined. In reality, defining the downstream distribution over specifies the problem and, therefore, the input distribution must be reasonably correct. It is planned in the near future to investigate using a linear extrapolation of flow properties similar to the one used for choked flow at the downstream boundary. It must be determined if an extrapolated downstream boundary will converge to a reasonable distribution with time.

4.4 UPSTREAM BOUNDARY CONDITIONS

A coordinate line x = constant at m = 1 is chosen as the upstream boundary. The inputs are the radial distribution of stagnation pressure, stagnation temperature, mass-weighted gas composition, and normalized static pressure. The static pressure can be normalized by either the outer or inner wall static pressure.

4.5 FREE-JET EXPANSION (CHOKED)

To caluctate the flow field for a convergent nozzle exhausting to a prescribed pressure field, the free-jet portion of the outer contour is adjusted with time until the prescribed and calculated pressures on the boundary agree. The free boundary contour is adjusted with the following expression:

$$\theta_{\text{new}} = \theta_{\text{old}} - \frac{1}{2} \frac{(P_{\text{old}} - P_{\text{new}})}{(\rho V^2)_{\text{old}}} (|W_{\text{old}}^2 - 1|)^{1/2}$$
 (4. 15)

The absolute value of M^2-1 is used so that Eq. (4.15) will also apply for slightly subsonic flow (i.e., M > 0.9). If the nozzle exit radius and the new axial distribution of flow angle are known, a new free boundary contour is caluclated from

$$s_o = \sum_{i=s_{oxit}}^{i} (s_o)_i + \Delta x \tan \frac{(\theta_o)_i - (\theta_o)_{i+1}}{2}$$
 (4.16)

By using this subroutine, the computer program is restarted until the specified and calculated pressures agree within some preselected tolerance.

4.6 INITIAL FLOW PARAMETERS

As previously stated, to calculate the components W_i at time level $\ell+1$ requires the components W_i at time level ℓ . The steady-state solution is independent of the path; however, the prescribed initial flow field does have some influence on the time required to reach steady state. The present solution is initiated from a pseudo one-dimensional flow field. To establish the initial flow field, it is assumed that all flow properties are independent of axial distance (x), or

$$P_o(x,r) = P_o \frac{r-s_i}{s_o-s_i}$$
 (4.17)

$$T_o(x,r) = T_o|_{m=1} \left(\frac{r-s_i}{s_o-s_i}\right)$$
 (4.18)

$$c_{P}(x,r) = c_{P_{m=1}}(\frac{r-s_{i}}{s_{o}-s_{i}})$$
 (4.19)

$$\frac{P}{P_{w}}(x,r) = \frac{P}{P_{w}} \Big|_{x=-1} \left(\frac{r-s_{1}}{s_{0}-s_{1}} \right)$$
 (4.20)

The local flow angle is assumed to vary linearly with radius, or

$$\theta_{local} = \theta_i + (\theta_o - \theta_i) \frac{r - s_i}{s_o - s_i}$$
 (4.21)

For choked flow, it is necessary to maximize the weight flow to ensure that the flow downstream of the throat is supersonic, or

$$W_{F}^{*}_{1-D} = 2\pi P \int_{s_{i}}^{s_{o}} \frac{u}{R_{g}T} r dr$$
 (4.22)

where T can be evaluated from Eq. (4.9) and u from Eq. (4.12). For the case of radial nonuniformities of stagnation properties, values of P are assumed until $W_{F\ 1-D}^*$ is a maximum. The value of P at each

axial station is found by iterating on P to satisfy the throat mass flow. Since the static pressure is initially assumed constant, this start procedure will not work for nozzles having large convergence angles (i. e., ≥ 50 deg) since for this case one-dimensional flow is a poor assumption.

4.7 TIME STEP

The finite differencing scheme used in this report is conditionally stable. Stability can usually be achieved if the spatial and time intervals satisfy the following condition:

$$\frac{\Delta t}{\Delta} \approx \frac{\left(M_{\text{mex}} + 1\right)^{-1}}{3u^4 - c^4} \tag{4.23}$$

where Δ is the smaller of Δx or Δy . Large numerical instabilities are readily apparent when negative or large oscillations of pressure are observed in the output for the higher Mach number regions of the nozzle. When this condition is encountered, a smaller time step should

be used and the calculations restarted from time zero. Oscillations in the numerical results can be limited by use of finer mesh size and possibly sometimes by a reduced time step. In general, however, it has been found to be desirable to maintain the largest time step consistent with numerical stability. Numerical oscillations less than one percent in pressure ratio $(P_{local}/P_{stagnation})$ are considered acceptable.

4.8 SPECIAL PROGRAM RESTRAINTS

In calculating various flow fields with the present set of equations, it was found necessary to add some programming restraints. These numerical restirctions could possibly be avoided if adequate computer storage were available so that the variation of flow properties both with time and across grid points could be kept small. These restraints are, (1) smoothing the nozzle density profiles, and (2) maintaining the radial distribution of the flow angle monotonic in the subsonic portion of the nozzle.

The density smoothing process consists of applying a weighting factor (a weighting factor of four is generally used) to the local value of density and then linearly smoothing with the surrounding values of density. All other variables are then recalculated to correspond to the smoothed density distribution. This smoothing process has an effect similar to adding a dampening factor to the numerical procedure to increase the apparent viscosity term. Such factors do not disappear at steady state; however, an analytical investigation of varying the value of the weighting factor and a comparison with experimental data revealed that the smoothing process has no significant influence on the accuracy of the results. Some influence may be felt at a point where the flow is being rapidly expanded.

The flow angle restraint subroutine is optional and is generally only required when there are insufficient grid points to adequately describe the geometry and inlet flow variations. This subroutine ensures that the flow angle is radially monotonic in the inlet region of the nozzle when the flow angle is known to be monotonic such as on a conical convergent nozzle (see sample calculations).

There is also a restriction on the minimum flow Mach number (\sim 0.1 to 0.2), and any calculated value less than this minimum value

is reset to the minimum value. Therefore, flow fields where expected Mach numbers are less than (0.1 to 0.2) should not be attempted.

SECTION V GENERAL PROGRAM INFORMATION

5.1 PROGRAM INPUTS

In order to make a nozzle calculation, the information required is the nozzle and centerbody radial coordinates and slope, radial distribution of total pressure, total temperature, and gas composition, and the normalized radial distribution of static pressure all at the nozzle inlet plane. For the case of an unchoked nozzle, the radial distribution of normalized static pressure and absolute values for the flow angle at the downstream boundary must also be specified. For convergent nozzles the nozzle ambient pressure or ambient pressure distribution must be specified. Appendix II gives the detailed information required to make up the input card deck.

5.2 PROGRAM OUTPUTS

In general, the program prints all the flow parameters at each grid point; that is density, axial and radial velocity, static pressure and temperature, flow angle, and Mach number. In addition the mass flow and axial thrust at each axial station are tabulated. Appendix III gives the specific printouts.

SECTION VI SAMPLE CALCULATIONS

To illustrate capabilities of the computer program, sample calculations for three basic turbine engine exhaust nozzle configurations are presented: (1) choked convergent-divergent, (2) choked unshrouded plug, and (3) unchoked convergent-divergent.

6.1 CHOKED CONVERGENT-DIVERGENT NOZZLE

A schematic of the nozzle geometry is presented in Fig. 1 (Appendix I). The flow stagnation conditions at the nozzle inlet are presented

in Fig. 2. The card format sheets for the program inputs are presented in Appendix IV. First, it should be mentioned that the nozzle was started at an inlet radius of 2,714 in. rather than 3,605 in. It has been found that for choked nozzles the flow conditions at the inlet region for Mach numbers less than ~0.3 have no apparent effect on flow conditions at the throat plane. By limiting the region of interest, a finer grid network can be obtained in the region of the nozzle throat. Second, it should be noted that the nozzle wall forms an apex at the throat plane (the wall slope instantaneously changes from -0.44 to 0.0267). Since only a single value of wall slope can be specified, the average slope (-0. 20664 for the present case) is used. A comparison of experimental (Ref. 7) and theoretical wall pressures is presented in Fig. 3. complete printout is presented in Appendix V. In general, the calculated wall static pressure distribution agrees quite well with experiment. The same is true of the theoretical and experimental thrust and discharge coefficients. In calculating the nozzle performance coefficients, a first order boundary layer correction was applied to the inviscid flow field results. The computer program used for the boundary layer correction is described in Ref. 8.

As the results demonstrate, the present analysis can be used for supersonic flow. This is only true as long as there are no strong shocks present. It is much more expedient, however, to use the rotational method of characteristics for the supersonic flow regime.

6.2 PLUG NOZZLE (UNSHROUDED)

A schematic of the nozzle geometry is presented in Fig. 4. The flow stagnation conditions at the nozzle inlet are presented in Fig. 5. The card format sheets for the program inputs are presented in Appendix IV. Here again, because of the low inlet Mach number, the flow field was started at an outer radius of 3.31R rather than 3.605R. The first guess on the free-stream portion of the outer flow field boundary is a divergent conical section. Three program restarts were used to obtain the specified pressure (960 \pm 40 psfa) along the free streamline. A comparison of experimental (Ref. 7) and theoretical wall pressures is presented in Fig. 6. For this caluclation, the supersonic portion of

²This calculation was made using an earlier subroutine which extrapolated internal flow conditions to obtain wall conditions. The results obtained using this subroutine should closely agree with the results obtained from the present program.

the flow was obtained from the rotational method of characteristics. Except for the aft end of the plug, the calculated and experimental pressures agree quite well. This discrepancy in plug pressure is attributed to flow separation caused by the shock which originates from the flow expansion process at the cowl exit plane. The present calculation assumes that the flow remains attached to the plug. In calculating the nozzle performance coefficients, a first-order boundary layer correction (Ref. 8) was applied to the inviscid flow field results.

When using the free-jet subroutine, some caution is required. First, Eqs. (4.15) and (4.17) assume close agreement between the old and the new values for the boundary pressure. For example, if the calculated pressure ratio at a point is 5.0 and the target pressure is 2.5, it is best to reduce the boundary pressure in several increments (i. e., 5-4, 4-3, 4-3, 3-2.5) rather than in one step (i. e., 5-2.5). Second, for nozzle geometries having large flow expansions the numerical calculations cannot adjust in one grid point. For example, a 40-deg sharp lip convergent nozzle expanding to a pressure ratio greater than 4 can require one and possibly two grid points to make the transition from the last wall pressure to the value for the free-stream pressure.

Nozzle flow separation is another condition frequently encountered. Evaluation of nozzle separation pressure is a function of the particular nozzle geometry and boundary layer characteristics. In lieu of better information, there is some experimental evidence for convergent conical nozzles having small throat radius of curvatures that flow separation will occur when the wall pressure is approximately 0.85 of the freestream pressure. Therefore, in making a convergent nozzle calculation, it is assumed that the nozzle flow remains attached to the wall if the wall pressure is ≥ 0.85 of the external pressure. If the wall pressure is < 0.85 of the external pressure, it is assumed that the flow will separate from the wall and readjust through a weak compression back to the nozzle external pressure. The free-jet subroutine is used to solve the separated portion of the nozzle flow.

6.3 UNCHOKED CONVERGENT-DIVERGENT NOZZLE

The nozzle configuration for this calculation consisted of a circular arc nozzle inlet and throat which merges into a 6-deg half-angle divergent conical section. The flow stagnation conditions at the nozzle inlet are presented in Fig. 7. The card format sheets for the program inputs are presented in Appendix IV. At the nozzle exit plane, a linear

radial variation of flow angle was used and a radial variation of static pressure profile was assumed. The radial distribution of composition was estimated by assuming complete combustion for the local values of fuel and air ratio from Fig. 7. In making this calculation, the flow angle restraint was used for the entire flow field. The first calculation made without the flow angle restraint exhibited some flow divergence near the nozzle centerline. The final plot from the program plot routine is shown in Fig. 8. This plot presents the nozzle geometry and lines of constant static pressure. The blip in the static pressure profile near r = 2.5 is attributed to the dip in the total temperature radial profile and the rapid decrease in fuel-air ratio at this radial position.

SECTION VII

An analytical method and computer program has been presented which is capable of predicting the flow field and performance coefficients for axisymmetric exhaust nozzles representative of turbine engines. To make a calculation for choked nozzle flow, the description of the nozzle geometry and the radial distribution of flow stagnation conditions is required. To make a calculation for choked nozzle flow, a description of the nozzle geometry, radial distribution of flow stagnation conditions, and downstream radial distribution of flow angle and normalized static pressure is required. The magnitude of the radial variation in stagnation conditions which can be handled by this computer program will be a function of the available mesh size and nozzle configuration. This factor can be determined with operating experience for the individual computer.

The computer program in its present state is capable of calculating the inviscid flow field for most nozzles of practical interest. With some modification, additional nozzle configurations could be considered. For instance, the free-jet boundary subroutine can be used on the nozzle centerbody surface for truncated plug nozzles. Also, the case of two intersecting jets could be solved simultaneously by alternately matching the pressure along the jet interface. This case could be representative of ejector nozzles which have a step profile in stagnation conditions providing, of course, viscous effects do not predominate the flow field. Any gas composition can be calculated as long as the specific heat-temperature relation is expressed as a second-order polynominal.

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APPENDIXES

- I. ILLUSTRATIONS
- II. PROGRAM INPUT CARDS
- III. PROGRAM PRINTOUT
- IV. CARD FORMAT SHEETS FOR SAMPLE CASES
- V. SAMPLE PRINTOUT FOR C-D NOZZLE
- VI. COMPUTER LISTING



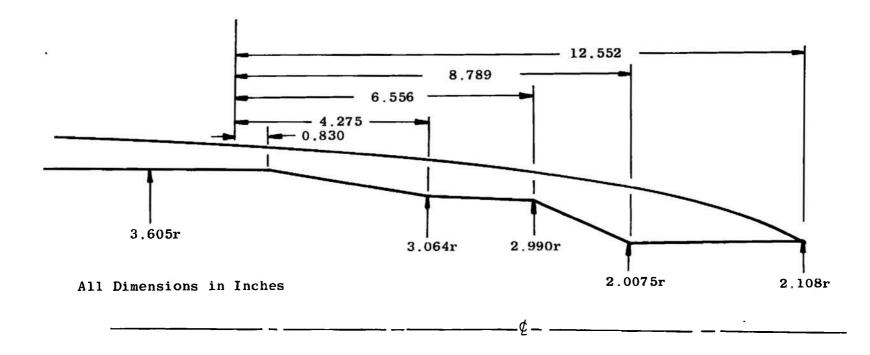


Fig. 1 Convergent-Divergent (C-D) Nozzle Configuration

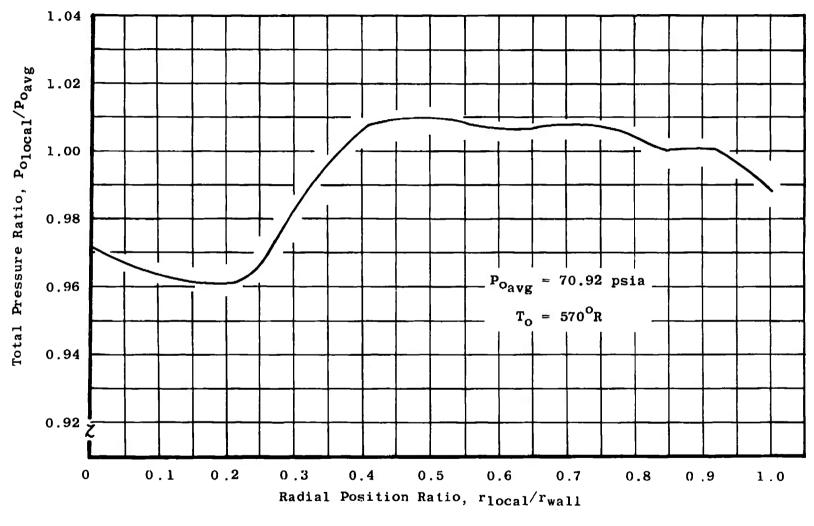


Fig. 2 C-D Nozzle Inlet Radial Total Pressure Distribution

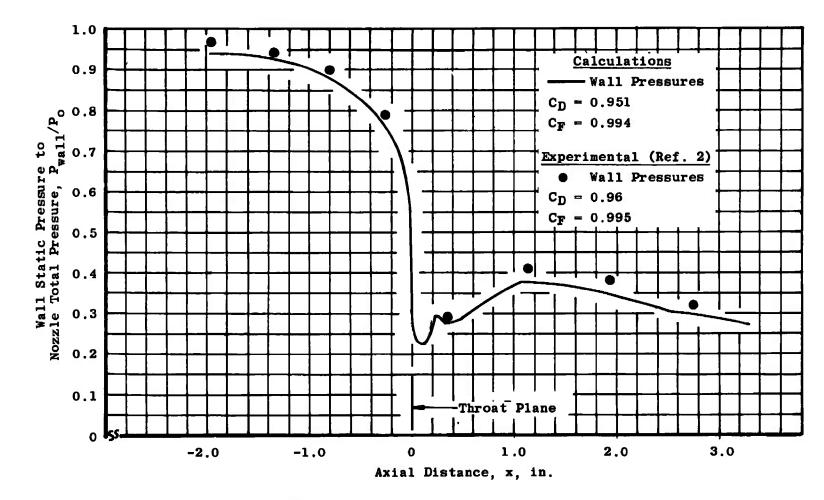


Fig. 3 C-D Nozzle Wall Pressure Profile

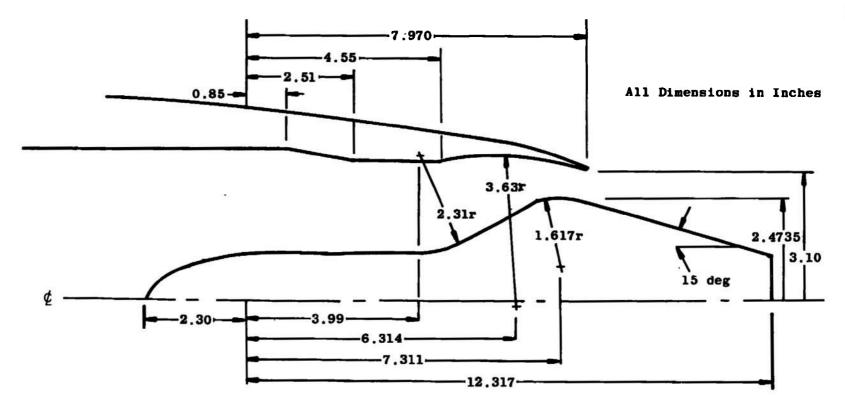


Fig. 4 Unshrouded Plug Nozzle Configuration



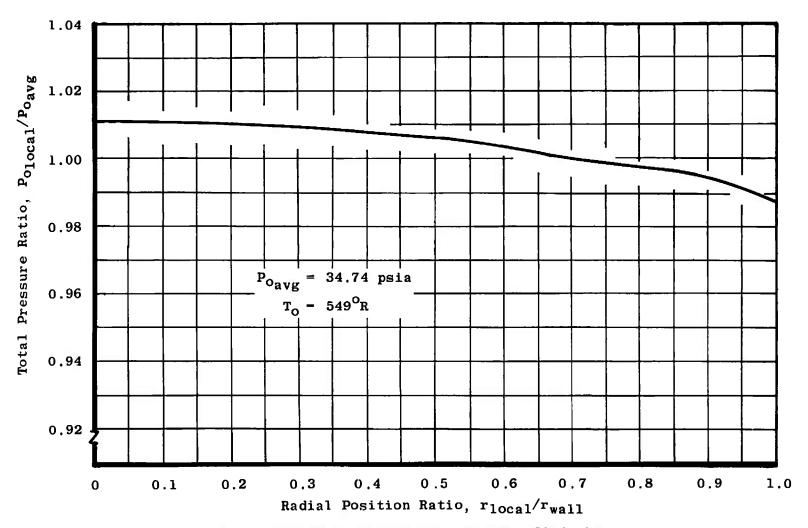


Fig. 5 Unshrouded Nozzle Inlet Radial Total Pressure Distribution

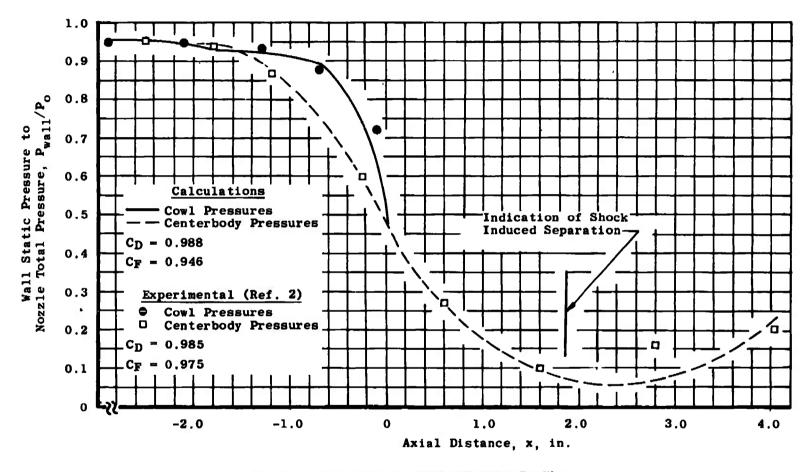


Fig. 6 Unshrouded Nozzle Wall Pressure Profile

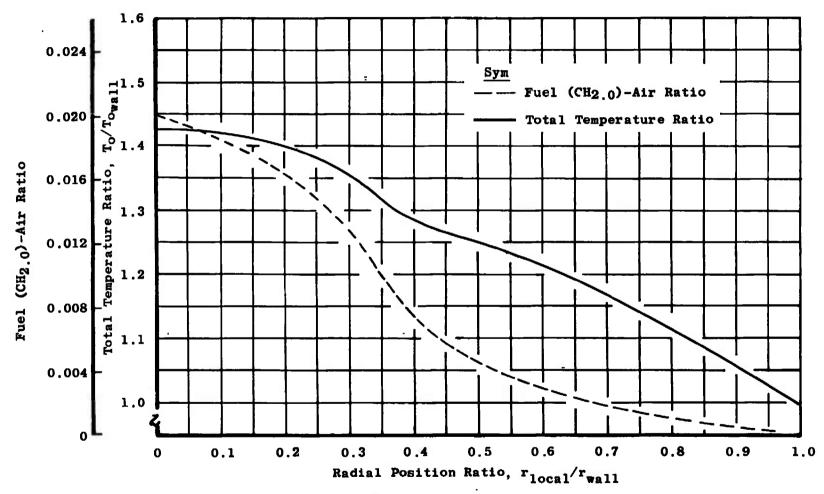


Fig. 7 C-D Nozzle Inlet Radial Profile Distribution of Inlet Temperature and Fuel-Air Ratio

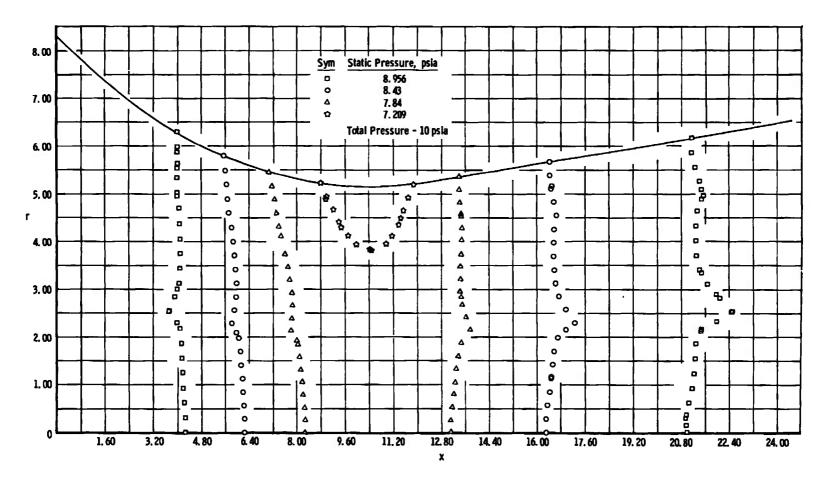


Fig. 8 Isobars for Subsonic Flow in a C-D Nozzle

APPENDIX II PROGRAM INPUT CARDS

Card 1 - Identification Card

Cols. 1-4, 1- **

Cols. 5-80. Title identification

Card 2

This card specifies the number of times printed and the number of cycles per output. For instance, 3 and 50 means that the flow field will print out every 50 iterations for a total of 150 iterations.

Cols. 1-5, Number of times printed (I-5 format)

Cols. 6-10, Number of cycles per output (I-5 format)

Cols. 11-15, any positive number in this space indicates a restart of the flow field, for instance, in going from 150 to 300 iterations. If these columns are left blank, it indicates that a new case is being started. Any negative number in this space indicates a new free-jet boundary is to be evaluated before the calculations are continued.

Additional Cards for Free-Jet Subroutines

These cards are used only if there is a negative number in Columns 11-15, Card 2.

Additional Card 1

Cols. 1-5, First X station for free pressure reset (I-5 format)

Cols. 5-10, Last X station for free pressure reset (I-5 format)

Cols. 11-20, Downstream pressure control (psfa) (E-10 format)

The downstream pressure control is used only for the choked nozzle program. The purpose of this control is to prevent the downstream boundary from becoming subsonic. The magnitude of the control pressure should be approximately equal to the static pressure value for sonic flow on the axis.

Additional Card 2

These cards contain the desired pressure ratio (P stagnation P static) (E-10 format) at each X station. The pressure ratios must be input in consecutive order from upstream to downstream and the number of input pressure ratios must correspond to the number of X stations implied on additional card 1. If the pressure is constant with X, then the pressure ratio should be input as a negative number in Cols. 1-10 (E-10 format).

This is the end of the additional cards.

Card 3 and 4

These two cards specify the lines of constant static pressure to be used in a plot subroutine. Pressure should be input in psia. A total of 16 pressures can be input (E-10 format).

Card 5

This card is for the density smoothing or weighting factors. A

1-4-1 weighting distribution has generally been used. These factors

can be varied to determine if they are influencing the results. As long as the gradients in the flow field are fairly locally uniform (about a point), no significant influence has been found.

Cols. 1-5, upper factor, (i.e., 1) (I-5 format)

Cols. 6-10, lower factor, (i.e., 1) (I-5 format)

Cols. 11-15, left factor, (i.e., 1) (I-5 format)

Cols. 16-20, mid factor, (i.e., 4) (I-5 format)

Cols. 21-25, right factor, (i.e., 1) (I-5 format)

Card 6

Cols. 1-5, the number of y stations (I-5 format)

There are a minimum of 3 and a maximum of 21 stations available. More stations may be added by recompiling. Δy and Δx should be approximately equal at the throat.

Cols. 6-10, the number of x stations (I-5 format)

There are a maximum of 57 stations available. More stations may be added by recompiling.

Card 7

Cols. 1-12. Δx , ft (E-12 format)

Cols. 13-24, Δt sec (E-12 format)

Cards 8 -- N

These cards contain the nozzle geometry, and for a convergent nozzle, the first assumption on the coordinates for the free streamline. The number of geometry cards must be equal to the number of r stations in Cols. 6-10. Card 6. (4E15.0 format)

Cols. 1-15, value of y³ (ft) for the outer nozzle wall

Cols. 16-30, value of $\tan \theta$ for each y value on the outer nozzle wall

Cols. 31-45, value of y (ft) for the centerbody (for no centerbody let s_i centerbody be a very small number, for instance 0.001 s_0^*).

Cols. 46-60, value of $\tan \theta$ which corresponds to centerbody y value (for no centerbody, $\tan \theta = 0$).

The values of y and tan θ are input in sequence starting at the nozzle inlet.

³Since single precision is used, y for the outer wall should not be less than 0.1. The nondimensional flow field is not affected by the units on y; only the relative values of x and y are important.

Card N + 1 Insert blank card

Card N + 2

This card is for the flow angle restraint. Leave this card blank and the subroutine is bypassed. For a conical nozzle having a sharp lip and without a centerbody the flow restraint may be used up to the nozzle exit plane. For a contoured nozzle or centerbody the flow restraint should be used up to the first geometry inflection point (refer to sample cases).

Cols. 1-5, axial (x) station for flow angle control (I-5 format)

Card N + 3

This card specifies whether the real or perfect gas subroutine is used. For real gas, cp is represented with a quadratic in temperature. The constants used for the cp-T relation have a temperature range from 400 to 2000°R. For temperatures greater than 2000°R, new constants are required. The perfect gas calculations drop the temperature coefficients on the quadratic. Perfect air is computed to have a specific heat ratio of 1.4.

Cols. 1-4, for perfect gas calculations, write PERF in Cols. 1-4.

For real gas calculations, write REAL in Cols. 1-4.

Card N + 4

This card indicates the number of radial stations for which flow properties will be input at the nozzle inlet plane. There is a minimum of 3 points that can be input. The flow conditions on the wall and centerbody or centerline must be two of the inputs.

Cols. 1-5, number of inputs (I-5 format)

Cards N + 5 → M

These cards specify the stagnation properties and gas properties radially across the nozzle inlet plane. The sequence of inputs is from the centerline to the nozzle wall.

Cols. 1-12, radial position

$$\left(\frac{r^2-s_i^2}{s_0^2-s_i^2}\right)$$
 (E-12, Format)

Cols. 13-24, stagnation pressure (psia) which corresponds to radial position. (E-12, format)

Cols. 25-36, stagnation temperature (*Rankine) which corresponds to radial position. (E-12 format)

Cols. 37-40, for information or identification. These columns may be left blank.

Cols. 41-45, Mass fraction of air (E-5 format)

Cols. 45-50. Mass fraction of carbon dioxide (E-5 format)

Cols. 51-55. Mass fraction of carbon monoxide (E-5 format)

Cols. 56-60, Mass fraction of water vapor (E-5 format)

Cols. 61-65, Mass fraction of oxygen (E-5 format)

Cols. 66-70, Mass fraction of nitrogen (E-5 format)

Cols. 71-75, Mass fraction of argon (E-5 format)

Cols. 76-80, Mass fraction of hydrogen (E-5 format)

If the total mass fraction does not add up to one, the individual mass fractions will be normalized by the total mass fraction.

Card M + 1

This card indicates the number of radial stations which will be used to specify the nozzle inlet static pressure profile. If a uniform profile is assumed, leave this card blank.

Cols. 1-5, number of radial stations (I-5 format)

Card M + 2 → L (for Choked Flow)

These cards specify the radial position and static pressure profile. The sequence of inputs is from the centerbody to the nozzle wall.

Cols. 1-12, radial position,
$$\left(\frac{\mathbf{r} - \mathbf{s_i}}{\mathbf{s_0} - \mathbf{s_i}}\right)$$
 (E-12 format)

Cols. 13-24, ratio of local static pressure to either the center-body or wall static pressure (E-12 format).

Card $M + 2 \longrightarrow L$ (for Unchoked Flow)

Providing card M + 1 is not blank, these cards specify the radial position and static pressure profile. The sequence of inputs is from the centerbody to the nozzle wall.

Cols. 1-12, radial position,
$$\left(\frac{r-s_i}{s_0-s_i}\right)$$
 (E-12 format)

Cols. 13-24, ratio of local static pressure to either the centerbody or wall static pressure (E-12 format).

If card M+1 is blank, then card M+2 indicates the number of radial stations which will be used to specify the exit plane profile. The following cards $(M+3 \rightarrow \cdots)$ should contain the same information as specified above, that is, the exit plane radial position, static pressure profile, and in addition the tan θ profile (Cols. 25-36). If a uniform exit profile is assumed, leave this card blank.

Card L + 1 (for Unchoked Flow)

This card specifies the mean value of the static pressure at either the inlet or exit plane. For the inlet plane, use a positive value for static pressure. For the exit plane, use a negative value of static pressure.

Cols. 1-12, static pressure (psia) (E-12 format)

APPENDIX III PROGRAM PRINTOUT

- 1. Nozzle Geometry The nozzle coordinates, area, and slope are printed. A check should be made to see that the values of SO' and SI' agree closely with $\frac{DSO}{DX}$ and $\frac{DSI}{DX}$, respectively.
- 2. Gas Properties The specific heat versus temperature for various components, molecular weight, and specific heat ratio versus radial position are printed.
- 3. Stagnation Conditions The ratio of specific heats, enthalpy, speed of sound versus radial position are printed. Also, the minimum velocity is printed. The minimum velocity is the smallest value permitted to be used in the caluclations. A velocity, whose value is calculated to be less than the minimum, is reset to the minimum value.
- 4. Flow Field The flow field is printed at each axial station for each time iteration specified to be printed. The first column of vertical numbers corresponds to the radial station, starting with the centerline or centerbody. The second vertical column (percent streamline) gives the percent of mass flow contained below this radial position. The third number (W_1) is the product of ρr . W_2 is the product of ρur . W_3 is the product of ρvr . W_4 is the product of the internal energy (e) and radius (r). The other printouts are self explanatory.
- 5. Nozzle Coefficients The first vertical column (W_F) is the calculated weight flow (lbm/sec) at each axial station. The second vertical column (W_f/W_f*) is the ratio of the mass flow at each axial station to the mass flow at the throat axial station. If the ratio of W_f/W_f* deviates significantly from unity at any one given axial station, this is an indication that more grid points are required at this station. The next column VD is the value of the

integral $2\pi \int_{s_i}^{s_o} \rho u^2 r dr$ at each axial station, and PD is the value

of the integral $2\pi \int_{s_i}^{s_o}$ Prdr at each axial station. The last vertical column is the nozzle thrust (lbf) at each axial station.

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- 6. Wall and Axis Flow Conditions The flow conditions on the wall and axis are separately tabulated after the last flow field has been printed.
- 7. Plot Coordinates The x, y coordinates for the isobars specified by Cards 3 and 4 are tabulated.
- 8. Convergence Criteria This portion of the printout is used to determine when steady-state conditions are achieved. The first horizontal line gives the axial station for which the wall and axial pressure ratios are tabulated. The last vertical column is the time iteration. The computations should be continued until the variation in pressure with time is considered to be negligible; furthermore, the pressure field should go through at least one or two minimums. Numerical oscillations less than one percent in pressure ratio are considered acceptable. If the flow will not converge, the time step should be reduced and/or increase the number of grid points.

APPENDIX IV PROGRAM INPUTS FOR SAMPLE CASES

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SHEET. 5 OF 5

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APPENDIX V SAMPLE PRINTOUT FOR C-D NOZZLE

NOMENCLATURE FOR COMPUTER PRINTOUT (in chronological order)

DT Increment of time used for calculations

DX Increment of axial distance used for calculations

SO Radial coordinate of nozzle wall

SOP Slope of nozzle wall

SI Radial coordinate of nozzle centerbody

SIP Slope of nozzle centerbody

A Area

A* Minimum area

R Radius

R* Radius at minimum area

S Difference in radial distance, S = SO - SI

DSO Radial increment of nozzle wall

DX Axial increment

SO' Slope of nozzle wall, SO' = SOP

SO'(D) Slope of nozzle wall in degrees

DS1 Radial increment of nozzle centerbody

SI' Slope of nozzle centerbody, SI' = SIP

SI'(D) Slope of nozzle centerbody in degrees

A0, A1, A2 Constants in specific heat-temperature relation

 W_1 Flow variable, $W_1 = pr$

 W_2 Flow variable, W_2 = pur

 W_3 Flow variable, $W_3 = pvr$

 W_4 Flow variable, W_4 = er

P-STAT Static pressure

P-STAG Stagnation pressure

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Temp (R) Static temperature

T-Stag Stagnation temperature

WF Weight flow

VD fpu²rdr

PD fPrdr

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5375			-ccci					
4933			.CO01				9	
4492	-,44		-0001 -0001				<u> </u>	_
4050 3608	44		-0001				9	
3167	44		-C001				10	
2725	44		- 6201				ii	
2284	44		COCI				12	
1842	44		.0001				13	
1400	44		. CCC1				14	
0959	44		.C001				15	
0517	44		.cco1	-,,			16	
C975	ZO	664	•CC31				17	
G1018	.026		- 0001				18	
01286	C26		.0001				19	
61554	•C 26	7 074	•0001				50	
C1822	. 626		-0001				21	
02090		7074	-0001				55	
C2358	-026	7074	.coci					
02627		7974	-0361				25	
02895		7674	-COC1				26	
03431		7674	-CCC1				27	
C 3699		7074		•			28	
C3967		7074	.0001				29	
04235		7074	ccci				30	
04503		7374	.cocl				31	
04771		7074	-C0C1				32	
05039		7974	_C0C1				33	
e53C7		7074	-0701				34	
C\$575		7674	.0701				35	
05843		7074	.0961				36	
C6112		7074	.00C1				37	
C6380		7074	-C001				36	
06644		7074	0301				39	
.06916		7074	-0001				40	
_C7184	• 029	57G74	-CCO1				41	

2.07720	.0267074	.C701		41	5	1 .
2.07789	. 5267074	.0001			5	2
2.09257	.C267374	.00Cl		45	5	5
2.G8525	.CZ67C74	. COO1		40	3	4
2.08763	-C267074	-0091		47	5	5
2-09061	-UZ67J74	.0001		41		<u> </u>
2.09329	.0267074	.0031		49		7
2_09597	.0267074	.0001		-		•
0					5	•
10 .					•	0
PERF					6	1
11					6	ž
	68.93	57C.	1.0		6	3
.0556	65.20	57C.	1.0			•
-3674	71,49	570.	1.0		- 6	5
.277b	71.56	570.	1.0			
.3895	71.25	57C.	1.0			7
.5003	71.49	57C.	1.0		6	0
.6119	71.42	57C	1,0			9
.7205	76.99	57¢.	1.0		1	0
, 0254	71.66	57G.	1.0			1
.9426	70.42	570.	1.0			
1,00	70.14	57C.	1.0			3
				•		14

65.COCO	LINES = 10 2	6C.000C	3	55.0000	4	50.00
45.0C00	6	40.0C00	7	35.C000		3C. 00
25,0000	10	20.0000		·		-
INTERPOLA	TION FACTORS					-
	1 1 4 1			 		
1.000	00 1.00000	1,00000	4.00000	1.000	09 6,09000	
C.1250	0,12500	0.125000	2.500000	0.1250	00	_
MC. POINT	S ON VERTICAL LIP	CIME1= 21 N	O. OF WALL POIN	TSINEL = 50		
MUS PULMI	3 DW AERITCHE ET	SE 1 PF / - Z 1 N	OF IN MULT POIN	13(47) - 30	.	-
						_
07 = 0).C320(MILLISECON	S) OX = 0.	10037 07 = 0	.05000		•
	FAUTURE					-
POSTE C	SOME INA					
	50	SOP	ST	519		-
**********	·····		,			
1	2.714160	-0,440700	0.000100	0.0	1	
2	2.609995	-0.440003	0.000100	0.0	2	
3	Z.e25799	-C. 44 CO30	0.00100	0.0	3	
4	2.561699	-0.440000	C. 300100	0.0	•	
2	2. 23 74 96	-7-440000	0-000100	0-0		
. 6	2.493299	-0.440000	0.707100	0.3		
	2.449220	-C.440C02	0.000100		\$	
8	2.4C5CCC	-C_44CCC	0.000100	0.0		
-9	2.367600	-0.440000	C. C20100	0.0		•
10	2.316700	-0.440000	0.000100	0.0	10	
	***************************************			***************************************		•
-11 12	2.272499	-C-44C000	0.000100	0.0		
12	2.225399	-0.440000	0.300100	0.0		
13	2.164199	-0.440000	0.00100	0.0	13	
14	2-136969	-C. 44 0000	0.500100	0.0	14	
	2.095900	-0.44003	0-370130	0.0	15	
1975		-0-44000	0.300100	0.0	141	
	2.0517 <u>00</u> 2.007500	-C. 2086-0	C. 300100			
		0.026707	0.000100	0.0	16	
16			0.000100	0.0		
16	2,010160	0. 6.4767				
19	2.C12859	0-026767			20	
16		0.026707 0.026707	0.000100	0.0	20	
18 19 20	2.012859 2.015539			0.0	21	
19	2.C12859	0,026707	0.000100	0.0	2021	
16 19 20 21	2.012859 2.015539 2.016220	0,026707 C.026707	0.000100	0.0	21	
16 19 20 21 22 23 24	2.012859 2.015539 2.016220 2.020900 2.023590 2.025270	0,026707 C.026707 C.026707 0.026707	0.000100 0.000100 0.000100	0.0 0.0 0.0 0.0	21 22 23 24	
16 19 20 21 22 23	2.C12859 	0,026707 C.026707 C.C26707 O.026707	0.000100 0.000100 0.000100 0.730100	0.0 0.0 0.0	21 22 23	
18 19 20 21 22 23 24 25	2.012859 2.015539 2.01820 2.020900 2.023590 2.028270 2.028950	0,026707 C.026707 C.026707 O.726707 O.026707 O.026707	0.000100 0.000100 0.000100 0.30100 0.000100	0.0 0.0 0.0 0.0 0.0 0.0	21	
18 19 20 21 22 23 24 25	2.012859 2.015539 2.01820 2.020900 2.023590 2.028270 2.028950 2.031830	0,026707 0.026707 0.026707 0.026707 0.026707 0.026707	0.000100 0.000100 0.000100 0.730100 0.000100	0.0 0.0 0.0 0.0 0.0	21	
16 19 20 21 22 23 24	2.012859 2.015539 2.01820 2.020900 2.023590 2.028270 2.028950	0,026707 C.026707 C.026707 O.726707 O.026707 O.026707	0.000100 0.000100 0.000100 0.30100 0.000100	0.0 0.0 0.0 0.0 0.0 0.0	21 22 23 24	

29	2.039670	0-026707	0.000100	0.0	29
. 30	2,0423.50	707650.0	0.000100	9,0	30
	2.045030	0,026707	0.000100	0.0	31
32	2.047709	0.026707	0.000100	0.0	32
23	2.053389	Q. C26707	0.000100	0.0	33
34	2,053069	0.026707	C. 000100	C. 0	34
	2.05575G	0.026707	0.000100	0.0	35
. 76	2.05843C	0.026707	0.000100	0.0	36
37	2.0e1119	0.026707	0.000100	0.0	37
39	2.543860	9.326707	0.000100	9.0	38
39	2.C4645C	0.026707	0.303100	0.0	39
40	2,C6916C	0.C26707	C. 00C 100	C. 0	40
41	2.071839	0. 026707	0.000100	0.0	41
42	2.074519	3. C26707	G. 207100	C. 0	42
43	2,077200	0.026727	0.000100	C.0	43
44	2.075889	0 267C7	0.300190	0,0	44
_45	2,982569	0.626707	C-00010C	0.0	49
44	2.08525C	0-024707	0.000100	0.0	46
47	2.087930	0.026707	Ç.00010C	0.0	47
48	2-C5061C	C. 226707	0.000100	0.0	48
49	2,053269	0. C267C7	0.070100	0.0	49
5C	2.095969	0.026707	0.000100	0.0	50

										1000000	99090	
	C.occl	2.1358	5.2715	C-4072	0.5429	0.6766	0-5143	0.9500	1.0857	1.2216	1.3571	1.6928
	1.4285	1.7642	1.8995	2.0356	2.1713	2.3070	2.4428	2-5785	2.7142			
	3.0001	0.1:36	0.2671	C. 4006	C. 5341	0. 65 76	3.4011	0.4146	1.0681	1.2016	"1.3250	1.4645
	1.6020	1.7355	1.8690	2.0025	2.1703	2.2695	2.403C	2.5365	Z. 67CO			
3	0.0001	0.1714	D.2677	C. 3540	0.5252	0.6565	9.7478	6.9191	1.3504	1.1017	1.3129	1 4442
•	1.5755	1.7568	1. £381	1. 7654	2.1007	2.2319	2,3632	2.4945	2.625P			
4	C.G.C.	0.1272	C. 2563	C. 3673	0.5164	0.6455	0.7746	C. 9737	1.0327	1-1618	1.2909	1.4200
	1.5451	1.6741	1. *072	1. 9363	2.0654	2.1945	2.3235	2.4:26	2.5517		•••	
5	· icessi ·	0.1270	0. 2538	C. 3807	0.5076	0.6344	5.7617	3. 5562	1.6151	1.1419	1.2668	1.3957
	1.5225	1.6454	1.7763	1.9011	2.0300	2.1569	2.2838	2.4106	2.5375			
	0.0001	9.1248	C. 24 94	C-3741	0.4987	0.6434	C.7481	0. 2727	C. 9974	1.1220	1.2467	1.3714
-	1950	1.6237	1.7453	1.8720	1. 5947	2.1153	2.2440	2.3525	2,4733	100220	102701	203.14
7	0.000	0.1226	C. 2452	C. 36 75	899	2.6124	C.7346	5 777	C 5707	1.1072	1.2246	1.3471
•							2.2043	2. 3267	2.4442	101012	102240	1.34.
	1.4696	1.5520	1. 7145	1.8369	1.9594	2.001h				1.0823	1.2025	1. 1220
•	C.CC01	9-1203	0.2406	C. 3608	G. 4811	0.6013	0.7216	C.8418	9.9621	1.002.	1.2(2)	10 1220
9:		1.5023	. 1.6835	1.8038	1.9246	2. 5443	2-1645	2.2848	2.4050			1.2985
	0.0001	0.1191	0-2362	C-3542	C. 4722	0.5993	C.7353	0-6563	2.9444	1.0624	1.1804	105462
	104165	<u>0455</u> 01	1. 15.76	1.77C6	1.5707	2.0767	2,1247_	2.242 R	2.3409			
10	0.001	0.1157	C ?16	C. 3476	0.4634	0.5757	C-6951	0100	(. C267	1.0426	1.1584	1.2742
	1.7901	1.5059	1.6217	1.7375	1.8534	1.9672	2.0850	2.2009	2.3167			
11	. 6.0001	0.1137	C. 2273	C-3410	C. 4545	2.56.92	0-6818	0.7954	0.9041	1.C227	1.1263	1. 2499
	. 1.3635.	1.4772	. 1.45CP	1.7044	1.8150	1.9316	2.0453	2.1589	. 2-2725			
12	0.0001	0.1115	C. 2225	0.3343	C.4458	0.5572	0.6056	0.7800	C. 8914	1.0026	1.1142	1.2257
	1.3371	1.4465	1.5575	<u> 1.6713</u>	1.78?7	1.8962	2.0056	2.117C	2.2254			
13	C.CCG1	0.16°3	0.2185	C. 32 17	C. 4349	0.5461	C.6553	0.7645	2.8727	L-4654	1.0921	1.2014
		1,4198	1.5290	1.6352	1.7474	1.9566	1.9658	2.0753	2.1642			
14	C.C.01	0.1071	0.2141	C. 3211	0.4281	0.5351	3.6421	0.7-91	0.8561	0.9631	1.0700	1.1770
	1.7640	1.3910	1.4543	1.5050	1.7120	1.8190	1.4260	2.^330	2.1400			
15	0.0001	0.1045		G. 3145	C. 4193	0.5240	0.6788	0.73?5	G. 6354	0.9432	1.0480	1.1520
	1.2576	1.3-24	1.4672	1.5719	1.6767	1.7015	1.8863	1 9911	2.0959			
16	0.0001	0.1327	C. 2C53	C. 3C78	0.4164	C.5130	C.6154	0.7187	0. 8207	0,9733	1.0259	1.1285
	1.2:11	1.2726	1.43e2	1.5386	1.6414	1.7440	1.8465	1.9491	2.0517			
17	0.2001	0.1025	C. 2078	C.3012	0.4016	0.5019	0.6023	0.7027	C. PC31	0.9034	1.0038	1.1042
	1.2345	1.3049	1,4053	1.5056	1.6000	1.7064	1.5068	1.9071	2.5075			
10	C.G.31	0.1006	0. 2C11	C.301e	0.4021	G.5026	C.6731	0.7036	0.8041	C. 9046	1.0051	1.1056
• •	1.2361	1.7067	1.4072	1.5077	1.6092	1.7047	1.1092	1.9097	2.0102			
19	c.ccci	0.1 207	C. 2C1 4	2.302C	G.4027	0.5733	C.6739	0.7046	7.6052	0.9358	1.0065	1.1071
	1.2378	1.30#4	1.4050	1.5097	1.6163	1.7103	1.0116	1.4122	7.0129		10000	*****
20	. c.c.o1	0.1709	0.2016	0.3024	0.4032	3.5040	C.6C47	0.7055	0.8043	0.907C	1 .0076	1.1066
	1.2094	1.3101	1.4129	1.5117	1.6175	1.7132	1.8140	1.9145	2.0155	0	183018	
51		c. 151e.	9. 2C1 5	C.3CZ8	0.4037	0.5040	C.6755	0.7064	C.8773	0.9093	1.0052	1.1101
21	C. C301				1.6146	1.7155	1.5164	1.9173	2.0182	0.11.73	100.45	101100
 ·	1.2112.	1.7119	1.4178	1.5137		0.5753	C-6063	0.7274	3.2054	0.9095	1.0105	1.1115
22	C-CCC1	0-1011	0. 2C2 2	0.3032	C. 4643					0.9095	1.0199	401113
53	1-7126.	1.2136	1,4147	1.5157	1.5167	1.7178	1.5188	1.9199.	2.0209	0.9107	1.0110	1.1130
23	C.C:01	0.1513	C. 5C5+	C-3C36	0.4048		C-6371		0.8795	0.4101	1.7110	1.1130
24	1 • 21 4 2	1.315~	1.4165.	1.5177	1.6119	1.7201	1.5712	1.9224	2.0236			
24	c-ccc1	0.1-14	G. 2C27	C.3C40	0.4053	C-5066	C-403C	0.7093	0.6166	0.9119	1.0132	1.1145
	1 • < 1.58_	1.31.1	1,4144	1.51.57	!.6210	1.7223_	1.9237	1.9750	2.0263			
25	3.5331	0.1015	0.56.0	C. 3G44	0.4059	0.5273	C-6048	0.7102	2.6116	0.9931	1.0145	1.1160
	1.2174	1.3159	1203	1.5217	1.6232	1.7246	1.8 261	1.9275	2.5289			
26	C.7001	0.1217	0.2033	C. 3 04 P	0.4064	0.5080	C.6396	6.7111	2-7127	0.9143	1.0159	1.1174
	1.2190	1.3206	1.4227	1.5237	1.6253	1.7769	1.0285	1.0301	2.0314		🕾 .	
27	0.0071	0.1618	0, 2035	C.3052	0.4059	0.5087	0.4 104	7.7121	0.8138	0.9155	1.0172	1.1169
	1-2234	1.3223	1.4240	1.5758	1.6275	1.7792	1.8339	1.9326	2.6343			
								100				

28	0.0001	0.1019	0.2038 1.4259	0.3C56	C. 4075	0.5093	0.6112	0.7130	2.0370	0.4167	1.6185	1.1264
29	0.0001	0.1C21 1.3258	G. 2041 1. 4278	0.1060 1.5258	0.4680	0.5100	C.6120	0.7139	0.8159 2.0397	0.9179	1.0100	1.1219
30	C.DC01	0.1022	0. 2043	C.3C64	0.4094	0.5107	0.212A	0.7149	0.8170	0.9151	1.0212	1.1233
31	3.CC31	0.1023	C. 2C46	C-305F	0.4071	0.5112	C.6136	0.7158	C. 8181	0.9203	1.0225	1.1248
35	1,2271 0.CC01 1.2287	9,1025	0.2C45	C-3072	0.4096	0.5120	n.5144	1,9429	2.0477 2.0477	0.0512	1.0239	1.1263
33	C .CCui	0.1326	3. 2051	1.5359 C.3076	0.4102	0.5127	C.6152	0.7177	0.8202	0.9727	1.0252	1.1278
34	C-0701	1.3328 C.1327	2.2054	1.5378 C.3082	3.4107	7-29	1.8454 C.5163	0.7186	2.0304	0.9239	1.0266	1.1292
35	1.2419 3.0Cnl	7.1629	1.4372 0.2057	1.5758 C.3064	0.411	0.5140	1.847A C.6148	1.9504 0.7196	0.0531	0. 9251	1.0279	1.1307
36	1.2335 C.OCOL	0.1030	1. 43 <u>91</u> 0. 2055	1.5418 C.3088	1.6446 0.4118	0.2147	0.6176	0. 7205	2.0557	0.9263	1. 5293	1.1322
37	0.ccc1	0.1032	C-7062	1.543B C.3043	C. 4123	G. 5154	0.6184	0.7215	2.0584 C.8245	0.9276	1.0206	1.1337
38	1.2367 C. 2001	0.1033	C. 2C65	1.5459 C.3097	0.4123	1.752C.	0.6152	0.7224	7.8256	0.9268	i.0319	1,1751
39	1.2383 C.CCO1	1.3415	1.4447 C. 2067	1.5479 C.31Ul	l.6511 C.4134	0.5167	0.6230		2.0638	0.9300	1.0333	1.1366
40	1.2399 C.3031	1.3432	1.4466 2.207C	1.5459 C.31C5	3.6°32 3.4139	0.5174	1.9596 C.6305	7. 72 43	2.0565 C. £277	0.9312	1.0346	1.1301
41	1.2415. C.0201	1.3450	1.4484 C. 2C73	1.5519 C.31C9	1.0557 C.4144	1.7589	0.6216	1.9657	7.0692			1.1396
	1.2431	1.3467 C.1038	1.4503		1.6574	1.7611	1647	1.9683	2.0718	0.9336		
43	1.2448	1,3485	1.4522 C. 207A	1.5549 C. 3117	1 • 6 5 9 5 C • 4 1 5 5	0.51+4	1.5671	0.7271	2.6745	C. 5348	1.7396	1.1425
44	1.2464.	1.3572	1.4541	1.557° C.3121	1.6619	1.7654	1.6655	1. 9733	2.0772	0.9360		1.1440
	C.COC1	1.3520	1.4540	1,5557	1,6639	1.7679	1.5719	1.9759	2.0799			
	0.00C1 1.2456	C-1542 1-3547	0.2083	0.3125 1.5619	1.6661	1.7792	1.7743	1.9764	2.08331	=-/STILE!	1.0413	1.1455
46	1.2513	0.1044	C. 2 086 1. 4597	0.3129	1.6682	0.5214	0.0256 1.8767	0.7299 1.910	C-8342 2-0852	0.9384	1.0427	1-1469
47	C.0001	2.1045 1.3572	C.2C85	0.3133 1.5667	1.6704	2.5221 1.7748	1.8791	0.7º08 1.9835	C.8352 2.0879	0.9296		1.1484
48	1.2544	0.1046	^. 2C92 1. 4635	C.3127 1.56e0	0.4182	1.7770	0.6273 1.8516	0.7318 1.9861	0.6363 2.0904	C. 9478	1. 3454	1.1499
49	C.OCC1	0.1748 1.3607	0.2094 1.4653	C.3141 1.57CO	0.4187	C.9234 1.7793	G.6261 1.884G	0.7327 1.9886	0. #374 2.0933	0.9420	1.0467	1.1514
50	0.0C01 1.2576	0.1049 1.3624	0.2697 1.4672	0.3145 1.5720	0.4193	0.5241 1.7816	C.6289 1.8864	0.7337 1.9512	2.0960	0.9432	1.0480	1.1520

AREA	A/A*	R/R+
7.366	1.8279	1.3520
7.366 7.128	1.7689	1.3330
6,694	1.7109	1.3980
6.665	1.6539	1.2860
6.438	1.5077	1.2640
6.216	1.5425	1,2420
5,994		1.2230
5.764		1.1950
9 5.573		1.1760
5.367		1.1540
1 >.164	1.2814	1.1320
2 4,965	1.2322	1.1100
4,770		1,0880
4.579		1.0660
4, 252		1.6440
4.209		1.0220
7 4,020		1.0200
8 4.040		1.0013
9 4.051		1.0027
4.CE2		1.0040
1 4.073		1.0053
4.CE4		1.2267
3 4.094		1.0080
4 4.105		1.0793
5 4,116		1.0167
6 4.127		1.0170
7 4,134		1.2134
8 4.149		1,0147
9 4.160		1.0160
0 4.171		1.0174
1 4.182		1.0187
2 4.151		1.0200
3 4.204		1.0214
4 4.219		1.0227
5 4,226		1.0240
6 4.231		1.0254
7 4.246		1.0267
8 4,259		1.0280
9 4.270		1.0294
G 4.281		1.0307
4.292		1.0320
2 4.303		1.0334
3 4.314		1.0347
4.32		1.0361
5 4.337		1.0374
		1.0367
7 4.25		1.0401
8 4.37		1.0414
4.38		1.0427
C 4.39	1.0901	1.0441

MIN X-STA # 17 MIN AREA 4.0301 EFFECTIVE PAGIUS # 2.0075

	×	APEA	\$	\$0	057/0x	\$G•	20, (0)	\$1	D\$1/0X	51.	STITE!
ĭ	0.0	7.3667	2.7141	2.7142		-0.4400	0.0	0.0001	0.0	0.0	6.0
2	C-1004	7.1 200	2.5659	2.6700	-C-44C2	-0-4400	-27.7495	0.0001	0.5	0.0	0.0
3	0.2007	6.8948	2.5257	2.625#	-0.4398	-0-4400	-23.7495	0.0001	0.0	0.0	0.0
4	0-3011	6.6652	2.5816	2.5617	-C.4398	-0.4420	-23.7495	0.001	0.0	C- 0	0.0
s	0.4015	6,4369	2.5274	2.5375	-0.44.3	-C.445G	~~??7495	0.0001	ç.o.	C• C	0.0
6	C.5319	5.2165	2.4932	2.4933	-0.4398	-0.4400	-23.7495	C-9091	2.0	0.0	0.0
7	0.6022	5. 9986	2.4491	2.4492	-0.4399	-0.4400	-23.7465	0.0001	9-9	0.0	č.o
•	0.7026	5.7840	2.4049	2.4050	-C.4403	-C.4400	-23.7493	0.0001	0.C	0.0	C•0
9	O. RO30	5.5734	2.3eC7	2.3408	-0.4379	-C-4400	-23.7495	0.0001	0.0	C. 0	0.0
10	4. 90 34	5.3671	2.3166	2.3167	-0,4399	-6-4-0G	-23.7495	0.0071	0.6	C-0	0.0
ïï	1.6237	5.1642	2.2724	2.272	···-(.4399	-0.4400	-23.7495	0.0041	0.0	c.ö	¢•0
12	1.1041	4, 9658	2.2263	2-2294	-0.4398	-C-440C	-23.7495	C-C001	c.e	C-0	0.0
13	1.2045	4.7767	2.1841	2.1642	-G. 44C3	-0450	-23, 1495	"f.coct"	0.0	0.0	0.0
14	1.3049	4,9754	2.1399		-0.4398	-0.4400	-23.7465	0.0001	p.0	G. 0	0.0
15	1.4052	4,3520	2.0951	2.0959	-0.4398	-0.4400	-23.7495	0.0001	C.0	C-0	0.0
16	1,5056	4.2095	2.0516	2.0517	-t.4403	-0.4436	-23,7405	0.0001	0.0	0.0	0.0
17	1.6060	4.0301	2.0074	2.0075	->, 20e8	-0-2066	-11.6755	. 1000°J.	c.0	r. 0	
10	1.7064	4.0406	2.0101	2.0102	0.0267	C.C 207	1.5299	0.0501	0.0	0.0	0.0
19	1.0067	4.0516	2.0120	2.6129	0.0267	3.026Y	1.5299	0.0001	o.ć	0.0	0.0
20	1.5071	4.0624	2.0154	2.0155	¥450.5	0.0267	1.5299	c-000 <u>1</u>	0.0	0.0	0.0
21	2.0075	4.6732	2.0181	2.0162	0.0267	0.0267	1.5290	0.0001	0.0	0.0	C.0
	2.1077	4.0840	2.5208	2.0209	C. 3261	0.0267	1.5299	····b.ccoi	·····ò.ö····	0.0	0.9
53	2.2092	4.0949	2.0275	2,0236	1.0866	0.0267	1.5294	0.001.	0.0	0. n	0.0
24	2.3086	4.1758	2.0262	2.0243	0.0268	0.0267	1.5799	0.0001	C.0	0.0	0.0
25	2.4090	4.1166	2.0298	5.0549	¢•6594	0.0267	1.5299	o.coci	0.0	0•0	0.0
26	2.5094	4.1275	2.0215	2,0316	G. 0267	· · · 0.0 267	1.5299	0.001.	۰۰۰۰	0.0	0.0

3.61°2 3.91°4 4.0150 4.1154 4.2157 4.3161	4.2703 4.2814 4.2825 4.3036 4.3148 4.3259 4.3371	2.7664 2.7691 2.7717 2.7744 2.7771 2.7798 2.0798	2.0565 2.0562 2.0718 2.0745 2.0742 2.0749 2.0749	0.0267 0.0267 0.0267 0.0267 0.0268 0.0267	C.0267 O.0267 O.0267 C.0267 C.0267	1.5299 1.5299 1.5299 1.5299 1.5299	0.0001 0.0001 0.0001 0.0001	0.0 0.0 0.0 0.0 0.0	C. G O. O O. O O. O O. O O. O	0.0 0.0 0.0 0.0 0.0
3.9146 4.0150 4.1154 4.2157	4. 2814 4. 2925 4. 3036	2. 5691 2. 5717 2. 7744 2. 7778	2.05°2 2.0718 2.0745 2.0772	0.0267 0.0267 0.0267	0.0267 0.0267 0.0267	1.5299 1.5299 1.5299	0.0001	0.0 0.0	0.0 0.0 0.0	0.0 0.0 0.0
3.9146 4.0150 4.1154	4. 2814 4. 2925 4. 3036	2. 56 91 2. 5717 2. 7744	2.0592 2.0718 2.0745	0.0267	0.0267 0.0267	1.5299 1.5299	0.0001	0.0 0.0	0.0	0.0 0.0
3.9146 4.0150	4. 2814	2. 5651 2. 5717	2.0592 2.0718	0.0267	0.0 267 0.0 767	1.5299	0.0001	0.0 c.0	0.0	0.0
3.9146	4. 2814	2. j691	2.0592	0.0267	0.0267	1.5299	0.0001	0.0	0.0	0.0
3.7139	4. 2593									0.0
										0.0
3, 51 31	4.2371	2.7583	2.C584	C.C267	0.0367	1.5299	0.0001	0.3	0.0	0.0
3.4127	4.2261	2.0554	2.0557	0-7267	0.0267	1.5299	C-0001	0.0	C. 0	0.0
3.3124	4-2151	2.0530	2.0531	0.0267	0.C267	1. 299	0.0001	0.0	0.0	0.0
3-2120	4-2041	2.0503	2-0504	0-0267	0.0267	1.5299	0-00C1	0.0	0.0	0.0
3.1116	4.1931	Z. C476	2.0477	0.0267	C.3267	1.5299	0.6001	0.0	c. o	0.0
3.0112	4.1821	2-0449	2.0450	C. 2267	0.0267	1.5299	0.0001	0.0	0.0	0.0
2. 41 09	4.1712	2.0422	2.0423	0,0267	0.0267	1.5299	0.0001	0.0	C. 0	0.0
2.8105	4.1603	2.7396	2.0397	0.0267	0.0267	1.5299	0.0001		0.0	0.0
2.7101	4.1493	2, 2369	2 - 03 70	C.0267	0.0267	1.5299	C.0001	0.0	0.0	0.0
	2.9105 2.9109 3.0112 3.1116 3.2120 3.3124 3.4127	2.7101 4.1493 2.8105 4.1603 2.9109 4.1712 3.0112 4.1821 3.1116 4.1921 3.2120 4.2041 3.3124 4.2151 3.4127 4.2261 3.5131 4.2371 3.6135 4.2482	2.7101 4.1493 2.7269 2.8105 4.1603 2.7396 2.9109 4.1712 2.0422 3.0112 4.1821 2.0449 3.1116 4.1921 2.0476 3.2120 4.2041 2.0503 3.3124 4.2151 2.0530 3.4127 4.2261 2.0556 3.5131 4.2371 2.7583 3.6135 4.2482 2.3610	2.7101 4.1493 2.7369 2.0370 2.8105 4.1603 2.7394 2.0397 2.9109 4.1712 2.0422 2.0423 3.0112 4.1821 2.0449 2.0450 3.1116 4.1921 2.0476 2.0477 3.2120 4.2041 2.0503 2.0504 3.3124 4.2151 2.0530 2.0531 3.4127 4.2261 2.0556 2.0557 3.5131 4.2371 2.7583 2.0584 3.6135 4.2462 2.3610 2.0611	2.7101 4.1493 2.7269 2.0370 C.0267 2.8105 4.1603 2.7396 2.0397 0.0267 2.9109 4.1712 2.0422 2.0423 0.0267 3.0112 4.1821 2.0449 2.0450 C.5267 3.1116 4.1921 2.0476 2.0477 0.7267 3.2120 4.2041 2.0503 2.0504 0.0267 3.3124 4.2151 2.0556 2.0531 0.0267 3.4127 4.2261 2.0556 2.0557 0.7267 3.5131 4.2371 2.7583 2.0584 C.0267 3.6135 4.2482 2.0610 2.0611 0.0268	2.7101 4.1493 2.7269 2.0370 C.0267 0.0267 2.8105 4.1603 2.7396 2.0397 0.0267 0.7267 2.9109 4.1712 2.0422 2.0423 0.0267 0.0267 3.0112 4.1821 2.0449 2.0450 0.3267 0.0267 3.1116 4.1931 2.0476 2.0477 0.0267 0.0267 3.2120 4.2041 2.0503 2.0504 0.0267 0.0267 3.3124 4.2151 2.0530 2.0531 0.0267 0.0267 3.4127 4.2261 2.0556 2.0557 0.0267 0.0267 3.5131 4.2371 2.0583 2.0584 0.0267 0.0267 3.6135 4.2462 2.0610 2.0611 0.0268 0.0267	2.7101 4.1493 2.7369 2.0370 C.0267 0.0267 1.5299 2.8105 4.1603 2.7396 2.0397 0.0267 0.7267 1.5299 2.9109 4.1712 2.0422 2.0423 0.0267 0.0267 1.5299 3.0112 4.1821 2.0449 2.0450 C.0267 0.0267 1.5299 3.1116 4.1921 2.0476 2.0477 0.0267 0.0267 1.5299 3.2120 4.2041 2.0503 2.0504 0.0267 0.0267 1.5299 3.3124 4.2151 2.0530 2.0531 0.0267 0.0267 1.5299 3.4127 4.2261 2.0556 2.0557 0.0267 0.0267 1.5299 3.5131 4.2371 2.0583 2.0584 C.0267 0.0267 1.5299	2.7101 4.1493 2.7369 2.0370 C.0267 0.0267 1.5299 C.0001 2.8105 4.1603 2.7366 2.0397 0.0267 0.7267 1.5299 0.0001 2.9109 4.1712 2.0422 2.0423 0.0267 0.0267 1.5299 0.0001 3.0112 4.1821 2.0449 2.0450 C.3267 0.0267 1.5299 0.0001 3.1116 4.1921 2.0476 2.0477 0.0267 1.5299 0.0001 3.2120 4.2041 2.0503 2.0504 0.0267 0.0267 1.5299 0.0001 3.3124 4.2151 2.0530 2.0531 0.0267 0.0267 1.5299 0.0001 3.4127 4.2261 2.0556 2.0537 0.0267 0.0267 1.5299 0.0001 3.5131 4.2371 2.0583 2.0584 C.0267 0.0267 1.5299 0.0001	2.7101 4.1493 2.7369 2.0370 C.0267 0.0267 1.5299 C.0001 0.0 2.8105 4.1603 2.7396 2.0397 0.0267 0.7267 1.5299 0.0001 0.0 2.9109 4.1712 2.0422 2.0423 0.0267 0.0267 1.5299 0.0001 0.0 3.0112 4.1821 2.0449 2.0450 C.0267 0.0267 1.5299 0.0001 0.0 3.1116 4.1921 2.0476 2.0477 0.0267 (.0267 1.5299 0.0001 0.0 3.2120 4.2041 2.0503 2.0504 0.0267 0.0267 1.5299 0.0001 0.0 3.3124 4.2191 2.0530 2.0531 0.0267 0.0267 1.5299 0.0001 0.0 3.4127 4.2261 2.0556 2.0557 0.0267 0.0267 1.5299 0.0001 0.0 3.5131 4.2371 2.0583 2.0584 C.0267 0.0267 1.5299 0.0001 0.0	2.7101 4.1493 2.7369 2.0370 C.0267 0.0267 1.5299 C.0001 0.0 0.0 2.8105 4.1603 2.7366 2.0397 0.0267 0.7267 1.5299 0.0001 0.0 0.0 2.9109 4.1712 2.0422 2.0423 0.0267 0.0267 1.5299 0.0001 0.0 0.0 3.0112 4.1821 2.0449 2.0450 C.0267 0.0267 1.5299 0.0001 0.0 0.0 3.1116 4.1921 2.0476 2.0477 0.0267 0.0267 1.5299 0.0001 0.0 0.0 3.2120 4.2041 2.0503 2.0504 0.0267 0.0267 1.5299 0.0001 0.0 0.0 3.3124 4.2151 2.0530 2.0531 0.0267 0.0267 1.5299 0.0001 0.0 0.0 3.4127 4.2261 2.0556 2.0537 0.0267 0.0267 1.5299 0.0001 0.0 0.0 3.5131 4.2371 2.7583 2.0584 C.0267 0.0267 1.5299 0.0001 0.0 0.0 3.6135 4.2462 2.0610 2.0511 0.0268 0.0267 1.5299 0.0001 0.0

INFLECTION POINT NO. 4 16

(SUP-S1P1/S	517/5	1/5
1 -0.162116	0.0	0.168452
2 -0.1548CC	(.0	3.374547
3 -3.167574	C. 0	0.340951
4 -C.170+37	C. 0	C. 387357
5 -C.173406	C.O	0-394104
6 -0.17648C	C-0	0.401791
7 -0.179658	<u>c• č</u>	0,408313
8 -0.1929EC	c.c	0.415614
-0-186385	C. C	2,423603
10 -0.189533	C.O	0-431e67 9-440064
12 -0.197460	·è•ë	C. 446773
13 -0.201496	č. c	0. 457855
14 -0.205617	0.0	C. 467312
15 -0.209944	C. 0	0. 477145
16 -3.214467	C.0	C. 487425
17 -0.102939	C.O	2,496157
16 1.226674E-C2	C. C	C. 4 97 4 93
19 1.3264C5E-C2	_ <u>c. c</u>	2,496830
20 1.325141F-C2	C- C	0.456170
21 1-3233*0E-C2	<u>ç• ç</u>	3-49*511
22 1.321s24E-C2	C.0	0.494854
23 1.319975E-C2 24 1.318122E-C2	<u> </u>	G.494198 C.493542
25 1.1163616-62	C. C	0.492890
Ze 1. 114045E-C2		C. 492240
27 1.3129135-62	C. 0	3.491591
28 1.211186E-C2	C. 0	0.492945
29 1.309462E-C2	Ç. 0	0.49?299
30 1.3077446-02	C. 3	2.489656
31 1.30603CE-C2	C+ C	0.499014
32 1.334321E-C2	C.C	0.498374
33 1. 202616E-CZ	<u>0. c</u>	0.467736
34 1.370916E-C2	C. 0	0.467099
35 1.299219F-C2 36 1.297528E-02	¢, 0	0.486464 0.485831
36 1.297528E-02 37 1.295834E-G2	C. C	0.4551 97
36 1.294151E-G2	2.0	20434507
39 1.292473E-C2	c. 0	2.432938
40 1.296755-02	C. C	3.483511
41 1.2891256-02	C.C	C. 467686
42 1. 2874646-02	0.0	0.482063
43 1.2858625-02	C.C	0-481440
44 1.28414CE-CZ	C.C	O- 480818
45 1.282467E-C2	C.C	0.480199
4e 1.28C836E-52	C.C	0.479592
47 1.279194E-C2	<u> </u>	5.478986
46 1.277554E-C2 46 1.2755195-C2	C. 0	0.476352
49 1.2759194-C2 50 1.274287E-C2	-6.8	0.477749
30 102102212-02		00411127

			* * * *
	-4.843560F-0#	C. 0	1.1053556-04
- 2	-4.94+013E-65	C. 0	1.1236376-04
3	-5.C27231F-C5	C. C	1.1425-16-04
	-5.11310 PF-05		1.16297JE-04
5	-5.2021745-05	C. 0	1.1023136-04
6	-5.29443CE-C5		1.2032738-04
7	-5.2897336-35	C. C	1.224940E-04
8	-5.488752E-C5	C. C	1.247453E-04
•	-5.591560E-05	C.C	1.270839E-G4
10	-5.5 163C3E-C5	C.0	1. 29:001E-04
.11	-5. 60F83AE-C5	C.O	1.3271906-04
12"	-5. ;23798E-C5		1.346718E-04
13	-6.C436782-C5	C. C	1.373554E-04
14	-6.16.512F-05	C. 0	1. 471 935E-04
.15	-6,2983CSE-C5	C. C	1.431434E-64
16	-6.4342016-05	C. C	1.4672738-04
17	- 3. C + 01 71t - C5	C, C	1.4944776-04
16	3.986:2CE-C6	C. 0	1.492478E-04
19	3.98071-F-36	C. 0	1.495451E-04
20	3. 47542 CE-06	C.C.	1.4665796-04
.21.	3.97Ct 35E-C6		1.48+572F-04
22	3. 964 174E-C6	C. 0	1.454560E-04
. 23	3.9556232-06		1.482594E-C4
24	3.954367E-06	C. 0	1. 46C 526E-C4
25	3,9691-2F-CE	<u> </u>	1.47RETGE-04
20	3.943934E-C6	C. 0	1.4767236-04
4.7	3. C38738E-06	0.0	1.474774E-04
26	3. 943555E-C6	C. 0	1.472834E-04
.29	3.928386E-26	<u>C. 0</u>	1.4706996-04
30	3.92 133CE-C6	C. 0	1.44 7 76 36 -04
-21	3. 01 +C9CE- C6	0.0	1.467043E-04
32	3.91296ZE-C6	C. 0	1.46-123F-04
33	3. 907947E-06	<u></u>	1 - 4e 320 8F - 04
34	3.922746E-C6	C. 0	1.461298E-04
. 35	3. 397657E-06		1.459?92F-04
36 37	3. 692582E- Ce	0.0	1.457492E-04
38	3. 8475CZE+06		1.455597E-04
30		C. C	1.4536998-04
40	3.877418E-C6		1.451614E-04
41	3. 657387E-G6	C. 0	1.448058E-G4
	7. #62391E-06		1.4401885-04
43	3. E374C5t-C6	C. 0	1.444321E-04
	3.852418E-C6	C. 6	1. 4424 546-04
45	3. 6474408-04	C. O	1.440547F-04
. 44	3.8425146-06	0.0	1.438745E-04
47	3. 8375821-06	C. 0	1.4368985-04
48	3.932be3E-06	č. č	1.477056F-04
40	3. 62 77566-06	0.0	1.433219E-04
36	3. 522 961 6-06	Ç. 0	1.431387E-04
	20 455 4455 00		

		100						63550	0.000
	1.0000	\$. 6000		3-60000	4.	COCOO	5.0	0000	6- 00000
	7.00000	4. OGCCÓ		9.00000	······································	-00C0	11.	6000°	12.0000
	13.0070	14.0200	· · · · · · · · · · · · · · · · · · ·	15,0005	Je	.codo	17.	0000	18.0000
_	19.0000	¥C-0900		21.0000	22	.00ro	23.	0000	24.0000
	25.0000	26.0GCC		27.0000	21	•0C00	29.	0000	37.0000
•••	31.0000	32.0000		33.0000	34	.0000	35.	6000	36.0000
	37.0003	38,0200		39.0000	40	.0000	41.	0000	42,0000
	43,0000	44,0006		45.0000	46	COCO	47.	0000	48.0000
	49.0000	50.00CC				•			
	Y-PLOT PAR	METERS Y-ZERC	- G. O		UNI	TS/INC	H - 0.40	0000	
	2.7142 2	2.67CO 3 2.4452 6	2.62 9 2.60 9		2.5517 2.3608	10	2.5775		
• • •	2.2725 12	2.2254 13	2.184	2 14	2-1400	15	2.0959		
	2.0517 17	2.0075 18	2.010		7. C129	70	2.0155		
	2.0152 22	2.C209 23	2. C23		2.0263	25	2.0289		
	2.C316 27	2-0343 24	2.037		2.0397	30	2.0423		
•	2.C450 32	2.C477 33	Z. C.50		7.0531	35	2.0557		
	2.0584 37	2.C611 30	2. 36 3		2.9665	42	2.0692		
	2.0710 42	2.0745 43	2.071		2.5799	45	2.0876		
_	2.0652 47	Z-C879 48	2,095	6 49	2.0933	50	2.0960		
	0.0001 57	C.OCO1 53	G- 200	1 54	0.0001	55	C-0001		
	0.6001 57	C.OCOL 53	2.023		0001	<u>ec</u>	0.0001		
		0.0001 63	5.000		8-2001	65	0-0001		
	C.CC0162.	C-0001 68	2.000		0. 0001	····7ċ···			
	0.CCC1 72	C.:001 73	C- C-		0.0001	75	C-6001		
_		C-0031 78	3.0:0		C-C031	- 66	0.0231		
		C.CC71 #3	D- 220		0-0001	85	C.0001		
•-	0.CCC1 92.	0.0001	C. 500		C. 0001	96			,,,,,,,,,,,
		0.CC01 52	2.000		7.0001	95	0-0001		
	C.CCC192 0.6CC1 57	C.0001 58	C. CO		0.0301	too	0-0001		

AEDC-TR-73-29

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EFFICIENTS	FOR CPENTU	/Lb- MA \$51	FIT-RA	IK [NE]				
MOL. MT.	AG	A1+T		A2+T+	• 2			
28.970	0.240096	0-C		0.0				
44,011	0.170765	0.0		0.0				
29.913	0, 241531	0.0		0.0				
18.614	0.430062	0.0		0.0				
•••••								
					_			
39.944	0.154246			C. P				
2.016	3.55500	C.0		0.0	_			
AJR	COS	CO	H20	02		A	н?	CP(STU/LBMASS-R
0.2491	6.1209	0.2615	0-4301	0.1905	C.7464	0.1243	2-2760	C.0
								1cc.6
								200.0
								300.0 400.0
948794.			-75.254.	291, 403			705 400	
C. 2461	0.1206	0.2615	0.4301	0.1905	0.2464	0.1243	2. 2210	500.0
C. 2401	0.1208	"C. 2413	C. 4301	0.1905	C. 2464	C. 1243	3. 2760	60C.0
0.2401	0-1208	C. 2615	0.4301	0.1905	0-2464	3.1743	3.2260	700.0
C. 2431			C. 4301	2.1705			3.2260	802.0
0.2471	0.1264	0. 2615	0.4301	0.1955_	0.2464	C.1243	3.2250	900.0
0 3/01	0 1250	0 2416	0 4303	0 1006	0 3444	0 1 24 2	3 7740	1020.C
								1100.0
								1200.0
								1350.0
		0. 2615	0.4301	0.1905	0.2464	0.1243	7.2760	1400,0
								1960.0
								1600.0
0.2401	C.1208	0.7615	0201	0.1905	0.2464	0.1243	3.2260	1700.0
	MOL. WY. 28.97C 44.011 28.911 18.614 32.000 39.944 2.016 AIR 0.2291 0.2401	MOL. NT. AG 28.97C 0.24009C 44.011 0.170765 28.911 0.241531 18.616 0.436662 32.000 0.24645 39.944 0.124345 2.016 3.2260C AIR C02 0.2401 0.1268	MOL. bY. AG Alaf 28.97C 0.24009G 0.C 44.011 0.170765 0.d 28.911 0.241531 0.0 18.016 0.430062 0.0 32.000 0.153461 0.C 28.000 0.246445 0.0 39.944 0.174345 0.0 2.016 3.2260C C.0 AIR CO2 CO 0.2401 0.1248 0.2615 0.2611 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1268 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615 0.2601 0.1208 0.2615	MOL. bY. AG Alaf 28.97C 0.24909G 0.C 44.011 0.170765 0.0 28.911 0.241511 0.0 18.616 0.436062 0.0 32.000 0.246445 0.0 39.944 0.124345 0.0 2.016 3.2260C 0.0 AIR CO2 CO M20 0.2401 0.1268 0.2615 0.4301 0.2401 0.2401 0.1268 0.2615 0.4301 0.2401 0.1208 0.2615 0.4301 0.2401 0.1208 0.2615 0.4301 0.2401 0.1208 0.2615 0.4301 0.2401 0.1208 0.2615 0.4301 0.2401 0.1208 0.2615 0.4301 0.2401 0.1208 0.2615 0.4301	28.97C 0.249996 0.C 0.0 44.011 0.120765 0.0 0.0 28.911 0.241511 0.0 0.0 18.616 0.436962 0.0 0.0 32.000 0.746445 0.0 0.0 39.944 0.174345 0.0 0.0 0.0 A1R CO2 CO M2O O2 0.2491 0.1269 0.2615 0.4301 0.1905 0.2401 0.1268 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.2615 0.4301 0.1905 0.2401 0.1208 0.26	MOL. bY. AG	MOL. b7.	MOL. bT. AG

RANKINE	AIR	£02	cā	H20	07	N2	4		CPIBTU/LBMQLE-RI
0.0	6.9554	5.3150	7. 3257	7.74.0	6.0954	6.9005	4.9670	6.5636	ი. მ
10C.0	6.9554	5. 3150	7.3257	7.748C	6.0954	6.9005	4.9670	6.5036	100-6.
200-0	6.9554	5.3150	7.1257	7. 7430	6-0954	6-9075	4.9673	6.5036	207.0
360.5	6.9554	5.3150	7.3257	7.7480	6.0954	6.9005	4.9670	6.5036	300.0
400.0	6. 7554	5.2150	7. 3257	7.7486	6.0954	6.9005	4.5470	6.5036	400.0
500+0	6 4554	5. 1150	7.3257	7.7480	5.0954	6.4005	4.5672	6.5036	5co.0
600.0	6.9554	5.3150	7.7257	7. 74 EC	6-2954	6.9005	4,9670	6.5336	600.0
730.0	0.9554	5.3150	7-3257	7.7460	0.004	6.9005	4.9670	6.5036	700.0
800-0	6. 9554	5.3150	7.3257	7.7480	6. 2954	6.9035	4.9670	6.5036	600.0
900.0	6.9554	5.315C	7.3257	7.7480	6.0954	6.9005	4.9670	6.5036	900-0
1000.0	6.9554	3.2150	7. 3257	7.7480	6-0934	6.9005	4.9670	6.5026	1000.0
1100.0	6.9554	5. 3150	7.3257	7.7480	6.0954	6.9005	4.967C	4.5016	1100.0
1200.0	6. 9554	5.7150	7.3257	7.7483	6,0954	6.9205	4,9670	6.5036	1200.0
1300-0	6. 9554	5-3150	7.3257	7.7465	0.0954	6.9005	4.9573	6.5036	1303-0
1400.0	6.9554	5.315C	7.3257	7.7480	6. 0954	6.9CC5	4.9670	6.5036	1400.0
1500.C	6.9554	5.3150	7. 1257	7.7480	6.0954	6.9005			1500-0
							4.4670	6.5036	
1600.3	6.5554	5-3150 5-3150	7.3257	7. 748C	6.0054	6.9005	4 5673	6.5036	1500.0
1700.0	6,9554	5.315C	7. 2257	7.7480	6.0954	6.9005	4.9673	6.5036	1400.G
BANK INC	A 10	COS	·ro	HZO	07	4.9		M2	CD/CW CAMPA
PANKINE	AIR	_ cos	<u>co</u>	H20	02	N2	A	H2	CP/CV GAMMA
0.0	1.4000	1.5972	1.3723	1.3450	1.4837	1.4245	1.6660	1.4400	0.0
0.0	1.4000	1.5972	1.3723	1.3450	1.4837	1.4045	1.6669	1.4400	0.0
0.0 100.0 200.0	1.4000 1.4070 1.4030	1.5972 1.5572 1.5572	1.3723 1.3723 1.3723	1.3450 1.3450 1.3450	1.4837 1.4837 1.4837	1.4045 1.4045 1.4045	1.6669	1.4400 1.4400 1.4400	0.0 100.6 200.0
0.0 100.0 200.0 300.0	1.4000 1.4070 1.4030	1.5972 1.5572 1.5972 1.5972	1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4337	1.4045 1.4045 1.4045 1.4045	1.6669	1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0
0.0 100.0 200.0	1.4000 1.4070 1.4030	1.5972 1.5572 1.5572	1.3723 1.3723 1.3723	1.3450 1.3450 1.3450	1.4837 1.4837 1.4837	1.4045 1.4045 1.4045	1.6669	1.4400 1.4400 1.4400	0.0 100.6 200.0
0.0 100.0 200.0 300.0	1.4000 1.4070 1.4030	1.5972 1.5572 1.5972 1.5972	1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4337	1.4045 1.4045 1.4045 1.4045	1.6669	1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0
0.0 100.0 200.0 300.0 400.0	1.4000 1.4070 1.4030 1.4030 1.4030	1.5972 1.5572 1.5572 1.5572 1.5572	1.2723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4637 1.4637 1.4637	1.4045 1.4045 1.4045 1.4045 1.4045	1.6659 1.6659 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 400.0
0.0 100.0 200.0 300.0 400.0	1.4000 1.4070 1.4030 1.4030 1.4030	1.5972 1.5572 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4637 1.4637 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045	1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 200.0 400.0
0.0 100.0 200.0 300.0 400.0 500.0	1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837	1.4245 1.4045 1.4045 1.4045 1.4045	1.6659 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 400.0
100.0 200.0 300.0 400.0	1.4000 1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4245 1.4045 1.4045 1.4045 1.4045 1.4045	1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 400.0 500.0 500.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0	1.4000 1.4070 1.4030 1.4030 1.4030 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4637 1.4637 1.4637 1.4637 1.4637 1.4637 1.4637	1.4745 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 400.0 400.0 500.0 700.0 900.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 900.0	1.4000 1.4070 1.4030 1.4030 1.4030 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6659 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 400.0 500.0 700.0 900.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 100.0	1.4000 1.4070 1.4030 1.4030 1.4030 1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4745 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6659 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 400.0 400.0 500.0 500.0 900.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 100.0 1100.0	1.4000 1.4070 1.4030 1.4030 1.4030 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1,4400 1,4400 1,4400 1,4400 1,4400 1,4400 1,4400 1,4400 1,4400 1,4400 1,4400	0.0 100.0 200.0 300.0 400.0 400.0 700.0 700.0 900.0 1000.0 1100.0
0.0 100.0 200.0 300.0 400.0 500.0 400.0 700.0 100.0 100.0 1100.0 1200.0 1300.0	1.400c 1.4070 1.4030 1.4030 1.4090 1.4090 1.4090 1.4090 1.4090 1.4090 1.4090 1.4090	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4637 1.4637 1.4637 1.4637 1.4637 1.4637 1.4637 1.4637 1.4637	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4044 1.4045 1.4045	1.6659 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 300.0 300.0 400.0 500.0 700.0 900.0 100.0 1100.0 1100.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 100.0 1100.0	1.4000 1.4070 1.4030 1.4030 1.4030 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669 1.6669	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 200.0 300.0 400.0 500.0 500.0 900.0 100.0 1100.0 1200.0 1300.0 1400.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 100.0 1100.0 1200.0 1300.0 1500.0	1.4000 1.4070 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 200.0 300.0 400.0 500.0 500.0 100.0 1100.0 1200.0 1500.0 1500.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 100.0 1200.0 1300.0 1500.0	1.4000 1.4070 1.4030 1.4030 1.4030 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4070 1.4070 1.4070	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6650 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660 1.6660	1.0400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 200.0 300.0 400.0 500.0 500.0 900.0 100.0 1100.0 1200.0 1200.0 1400.0
0.0 100.0 200.0 300.0 400.0 500.0 600.0 700.0 800.0 100.0 1100.0 1200.0 1300.0 1500.0	1.4000 1.4070 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000 1.4000	1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972 1.5972	1.2723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723 1.3723	1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450 1.3450	1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837 1.4837	1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045 1.4045	1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600 1.6600	1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400 1.4400	0.0 100.0 200.0 200.0 300.0 400.0 500.0 500.0 100.0 1100.0 1200.0 1500.0 1500.0

GAS PROPERTIES

STAGNATION PARAMETERS NC. LAPUT POLNTS= 11

	TREAM FRA	CT.	TAGNATIO	N		RELATI	VE HASS O	FSPECIE			
		PSIA	T-A	ALR	COS	Co	H20	02	NZ	A	HZ
1	0.0	65,930	570.C	1.0000	0.0	2.9	0.0	0.0	3.9	0.0	C. 0
z	0.0556	66.250	57:-0	1.0000	0.0	0.0	Ç. 0	0.0	0.0	0.0	0.0
3	0-1674	71,490	57C.C	1.0000	0.0	0,0	0.C	0.0	C.9	C.O	0.0
4	0.2778	71.550	57C.C	1.0000	6.0	0.0	0.0	r.c	0.0	C.C	C. C
5	0.3855	71.350	473.C	1.3000	2.0	3.0	0.0	0.0	C.O	0.0	0.0
6	0.5073	71.470	57C.C	1.0000	C. O	C.0	0.0	C.O	C.n	c. 5	6.0
7	0.6119	71.420	57C.C	1.0010	0.0	3.0	0.0	0.0	2.0	0.0	0.0
	0.7205	7C. 4 30	570.0	1.0003	0.0	0.0	0.0	0.0			
9	0.6354	71.000	57C.C	1.0600	o, c	0.0	0.0	0.0	0.0	0.0	0.0
ιò¨	0.9426	70.420	:7C.2	1.000C	0.0	C+0	0.C	0.0	e. 5	6.6	. c. c
11	1.0000	70-140	573.C	1.0000	0,0	0.0	0.0	0.0	0.0	0.0	0.0

•••••	•	•	GAS PROPERTIES	

	PSFA		AIR	C 03	<u></u> Co	H20	07	M2	A	HZ
1 0.0	9525.510	479.C	1.0000	0.0	0.0	0.0	0.0	C.0	0.0	0.0
2 -0.0556	9879.438	5 70. C	1.0000	2.0	2.0	0.0	C-0	C.0	0.0	0.C
3 2.1674	10294.559	57C.C	1,CQ00	0, C	0,0	0.0	2.0	C.3	0.0	0.0
4 C.2776	10304-637	577.0	1.0000	0.0	3.0	C.n	0.0	C.0	0.0	0.0
5 0.3895	10274.398	570-C	1.6000	0.0	0.0	C.7	0.0	C.2	C.0	0.0
6 0.5003	10294-559	570.0	1.0000	0.0	6.0	C. 2	G.0	0.0	0.0	0.C
7 3.6119	10284-477	570.0	1-0200	0.0	5.0	0.0	0.0	C.C	0.0	C.0
8 0.7205	15222.559	570.0	1.0C00	0.0	0.0	0.)	C.G	0.¢	0.0	0.0
9 0.8354	10232.637	570.0	1.0700	0.0	_0.C		c.c	C.0	r.5	C-0
10 0.5426	10143.477	573.C	1.0000	0.0	2.0	C-7	C • C	0.0	C.3	0.0
11 1.0000	10100-156	570.G	1.0000	0.0	0∙≎	0. >	0.0	0.0	0.0	C.0
·	PSFA	T-R	A1R	CCS	<u>ço</u>	HZO	02 _	N2		.н2
1 0.0	9925.918	570.C	1.0000	0.0	0.0	0.0	0.0	C.2	0.0	0.0
2 0.0500	9837.146	5 7C. 0	1.0000	J. C	7.0	0.0	0.0	0.7	C. 0	C.0
3 0.1000	10014-152	57C.C	1.000	C.C	0.0	0_0	0.0	e.s	0.3	C. 0
. 0.15GC	102,5-104	2,70.0	1.0000	0.0	3.0	0.0	0.0	C.3	0.0	C.C
5 C. 20CC	16297.531	5 70. C	1.0090	0.0	0.0	0.0	C.C	0.C	0.7	0.0
6 0-2500	10302.096	57C.C	1.0000	C.C	5.0	C.0	0.0	C.0	0.7	0.0
7 0.30CC	10298.625	57c,C_	1.0000	0.c	<u></u>	0.0	0.0	0.0	0.0	C.0
6 0.3200	10245.C9C	57C.C	1.0500	0.0	0.0	0.0	0.0	0.3	0.0	0.0
9 0.4000	10276.305	570.C	1.0C00	C.G	0.7	3.0	C.G	0.0	2.0	0.0
10 004200	10295.402	" 570.C"	1.0000	3.0		c.o	0.0	C.0	C.O.	0.0
11 . 0.5000.	10294.500	\$70.0	1. 220C	0.0	D. 0	0.5	0.0	0.0	0.0	0.0
12 0.5500	10790-046	570.0	1.0036	C.C	0.0	C. 0	÷.6	6.7	0.0	C.0
13 C.63CO	10295.547	570.C	1.0000	0.0	C.0	0.0	0.0	0.0	0.0	0.0
14 0.65CC	10262.750	570.0	1.00CO	C-0	0.0	0.0	0.0	0.0	0.0	0.0
15 0.7GOC	10234.242	57C.O.	1.0000	0.0	0.0	0.0	C.O	C.0	C.0	0.0
16 0.7500	10725-141	57C.C	1.0000	0.0	0.0	0.0	C.0	0.0	0.0	0.0
17 0.80CG	16229.523	57C.C	1.0026	0.0		0.0	0.0	0.0	C.0	0.0
18 G. **CG	10223.082	570.C	1.0000	C. 0	0.C	0.5	C-0	0.0	0.0	0.0
19 0.9000	13177-094	570.C	1.0000	0.5	0.0	0.0	0.0	0.0	0.0	0.0
20 C-9500	10135.273	575.0	1.3660	C. C	C-0	0.0	0.0	C.3	0.0	0.0
21 1.0006	10100-156	570. C	1.0000	7.0	0.0	5.0	0.0	0.0	C. 0	0.0

MOL WT	GAS CON .		CP CCEFFICIENT	<u> </u>	CA	COEFFICIENT	<u> </u>
28.97	1716,	6007.	0 <u>. c</u>	0.0	4291.	<u>0.0</u>	٥.
ZA. 97	1716.	BCC7.	6-0	c.c	4291.	0.0	0.
28.57	<u>171</u> 6	<u> </u>	0.0	C.0	4201.	C.0	<u> </u>
26.57	171e.	60:7.	c.0	3.0	4291.	0.0	c.
26.97	1716.	6007.	0 <u>.0</u>		4291	0.0	0,
26.97 26.57	1716. 1716.	6007.	0.0	0.0	4201.	0.0	c.
28.57	1716	6007			4291.	····· <u>Š</u> *ä······	······
20.97	1716.	6CC7.	0.0	5.0	4291.	0.0	č.
	1716.	6CC7.	C. 0	0.C	~251a	2.3	- 6
28.97	171e.	6327.	0.2	0.0	4251.	0.0	č
26.57	171e.	6307	C. 6	0.0	42°1.	C. 0	
28.97	1716.	6067.	5. ò	č.š	4271.	0.0	č
78.57	1710.	6007	0.0		4291.	0.0	·č
25.07	1716.	£037.	0.0	0.0	42°1.	0.0	0.
26.67	1716.	6007.	C. 0	C.0	4241.	0.9	0,
26.97	1714.	egc7.	0.0	C.C	4251.	6.7	C.
23.97	17ie.	eC37.	G. 0	c.c	4291.	C.C	Ċ
28.57							0.
	1716.	£07.	C• C	r.c	4701.	C.C	
28.97 28.97	1716. 1716. 1716. 1716.	6007. e007.	C. G.	C. C C. C	4291. 4291.	G•C G•C	O.
28.97 28.97	1716. 1716.	6007. e007.	0.0	C. 0	4291. 4291.	C•€	0
28.97 28.97	1716. 1716. IJN EVALUATION	6007. e007.	0.0 C.7	C. O C. C	4291. 4291. SPEED O	G+C O+O	O.
28.97 28.97	1716. 1716. EM: EVALUATION GAMMA 1.4000	6007. e007.	0.0 C.7 CV 4250.75	C. O C. C ENTHAL	4291. 4291. 	G+C G+O	O.
28.97 28.97	1716- 1716-	6007, e007,	0.0 C.7 CV 4250.75 4290.75	ENTHAL 3.424023E 00 3.424023E 00	4291. 4291. SPEED C	G • C G • O • O	O.
28.97 28.97	1716- 1716-	6007. e007.	0.0 C.7 CV 4250.75 4290.75	C.O C.C ENTHAL 3.424023E 04 3.424023E 02 3.424023E 04	\$PEED C	G • C G • C	0,
28.97 28.97	1716- 1716-	6207. e007. CP 6027.C6 6037.C6 6037.C6	0.0 C.1 CV 4250.75 4290.75 4290.75 4290.75	ENTHAL 3.424023E 00 3.424023E 00	4291. 4291. SPEED C 1170. 1170. 1170.	0.0 0.0 F SDUND 30 20 30	O.
28.97 28.97	1716- 1716- 1716- 1716- 1716- 1716- 18400 1-4000 1-4000	6007, e007, CP 6077, C6 6077, C5 6077, C6 6077, C5	0.0 C.7 CV 4250.75 4290.75	0.0 0.0 ENTMAL 3.424073E 00 3.424013E 00 3.424013E 00 3.424013E 00	\$PEED C	0-0 0-0 IF SOUND 30 20 30 30	O.
28.97 28.97	1716- 1716-	6207. e007. CP 6027.C6 6037.C6 6037.C6	0.0 C.7 CV 4250.75 4290.75 4290.75 4290.75	ENTHAL 3.424073E 00 3.424013E 00 3.424013E 00 3.424012E 00 3.424014E 00	\$PEED C 5PEED C 5 1170 6 1170 6 1170 6 1170 6 1170	0-0 0-0 0-0 0F SDUND 30 30 30 30	O.
28.97 28.97	1716- 1716- 1716- 1716- 1716- 18400 18400 18400 18400 18400	6207. e007. CP 6077.C6 6077.C5 6077.C5 6077.C5 6077.05	0.0 C.7 CV 4250.75 4290.75 4290.75 4290.75 4290.75 4290.75	ENTHAL 3.424073E 06 3.424073E 06 3.424073E 06 3.424073E 06 3.424074E 06 3.424074E 06	\$PEED C 1170, b 1170, b 1170, b 1170, c 1170, c 1170, c 1170, c 1170,	0+0 0+0 F SOUND 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28-97 28-97 SIA(NAT	1716- 1716- 1716- 1716- 1716- 1716- 18400 18400 18400 18400 18400 18400 18400 18400	6007, e007, cp 6007, c6 6007, c6 6007, c6 6007, c5 6007, c5 6007, c5	0.0 Cen CV 4250.75 4290.75 4290.75 4290.75 4290.75 4290.75 4290.75	2.0 C.C ENTMAL 3.424073E 04 3.424073E 05 3.424073E 05 3.424073E 05 3.424076E 05 3.424076E 05 3.424076E 05 3.424076E 05	\$PEED C \$PEED C \$1770, \$1170, \$1170, \$1170, \$1170, \$1170, \$1170, \$1170, \$1170, \$1170, \$1170,	0-0 0-0 F Strumb 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28.97 28.97	171 c- 171 c- 17	6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007. 6007.	0.0 C.7 CV 4260.75 4290.75 4290.75 4200.75 4200.75 4200.75 4200.75 4200.75	ENTHAL 3.424073E 04 3.424017E 04 3.424017E 05 3.424017E 05 3.424017E 05 3.424017E 06 3.424017E 07 3.424017E 07 3.424017E 07 3.424017E 07 3.424017E 07	\$PEED C \$PEED C \$ 1170 \$ 1170	0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0	O.
28.97 28.07 SLACNAT	1716- 1716- 1716- 1716- 1716- 1-4000 1-4000 1-4000 1-4000 1-4000 1-4000 1-4000 1-4000 1-4000	6207. 6027. CP 6277.C6 6277.C5 6277.C5 6277.05 6277.05 6277.05 6277.05 6277.05 6277.05	0.0 Cv 4250.75 4290.75 4290.75 4290.75 4290.75 4290.75 4290.75 4200.75 4200.75	ENTHAL 3.424073E 06 3.424074E 07	\$PEED C \$PEED C 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170, 1170,	0+0 0+0 F SOUND 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28-97 28-97 28-97 SIA(NAT	1716- 1716- 1716- 1716- 1716- 1716- 1800 1-400 1-400 1-400 1-400 1-400 1-400 1-400 1-400 1-400 1-400	6207. 60	CV 4250-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75	ENTMAL 3.424073E 00 3.424013E 00 3.424013E 00 3.424013E 00 3.424013E 00 3.424014E 00	\$PEED C 1170 1170 1170 1170 1170 1170 1170 1170 1170 1170 1170 1170 1170 1170	0-0 0-0 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28-97 28-97 SIA(NAY 2 3 4 5 6 7 8 9	171 c- 17	607. 607.	CV 4250,75 4290,75 4290,75 4290,75 4290,75 4290,75 4200,75 4200,75 4200,75 4200,75 4200,75 4200,75 4200,75	ENTHAL 3.424073E 06 3.424073E 06 3.424073E 06 3.424078E 00	\$PEED C 1170, 1170	0+0 0+0 0+0 F \$0und 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28-97 28-97 28-97 SIA(NAT	171 c- 17	6007. 6007.	CV 4250,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75	ENTHAL 3.424073E 04 3.424073E 05 3.424074E 05	\$PEED C \$PEED C \$1170, \$117	0-0 0-0 0-0 F SOUND 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28-97 28-97 51ACNAT	1716- 1716-	6007. 6007.	CV 4250-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75 4290-75	C.O C.C ENTHAL 3.424073E Od 3.424013E Od 3.424013E Od 3.424013E Od 3.424014E Od	\$PEED C 1170	0-0 0-0 0-0 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28.97 28.97 SIACNAT 2 2 3 4 6 7 10 11 12 13 14 15	171 c. 17	6207. 6027. CP 6277. C6 6277. C5 6277. C5	CV 4250,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75	ENTHAL 3.424073E 04 3.424073E 04 3.424073E 04 3.424073E 05 3.424073E 05 3.424073E 06	\$PEED C \$PEED C \$1170, \$117	0-C 0-0 0-0 F SCRING 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28.97 28.07 SIA(NAT	1716- 1716-	6007. 6007.	CY 4250,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75	C.O C.C ENTMAL 3.424073E 04 3.424073E 05 3.424073E 05 3.424073E 05 3.424078E 05	\$PEED C 1170,	0-0 0-0 0-0 F Strumb 30 20 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28.97 28.97 SIA(NAY 2 3.46 5,67 8 9 10 11 12 13 14 15 16	171 c. 17	6077. 66 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05 6077. 05	CV 4250,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75	ENTHAL 3.424073E 06 3.424073E 06 3.424073E 07 3.424078E 07	\$PEED C 1170, 1170	0-0 0-0 0-0 F SOUND 30 22 30 30 30 30 30 30 30 30 30 30 30 30 30	O.
28.97 28.07 SIA(NAT	1716- 1716-	6007. 6007.	CY 4250,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75 4290,75	C.O C.C ENTMAL 3.424073E 04 3.424073E 05 3.424073E 05 3.424073E 05 3.424078E 05	\$PEED C \$PEED C \$1170, \$117	0 - C 0 - C 0 - C 0 - C 0 - C 20 30 30 30 30 30 30 30 30 30 30 30 30 30	0,

COMPUTER	R/RW	PRES. FACT.	
1	G.C	1.00000	
2	C. C5000	1.60003	
2	2.1000	1,0000	_
- 4	0.150G7	1.00007	
5	Ç. 20CQQ	1,0000	
6	3.25000	1.0000	
	C-3000C	1.0000	
•	0.35000	1.60000	
9	C.403P0	1.0000	
10	7.45CCC	1.00000	
11	0- \$6095	1-00000	
12	C. \$5008	1.0000	
13		1.0000	
14	2.65000	1.00000	
15	2.7C00C	1.0000	
16	C.75030	1.0000	
		1. 3C9C0	
16	C. ESOCC	1.0000	
19	22266	1.0000	
20	C.55000	1.0000	
21	1.00000	1.00002	

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											-
3	0.C	0.0025	0. 21C2 0. 4225			C. 9625	0.0000 C. 7225	0.1275 3.8103	0.1600		C.25CO
	0.3025	0.3503	0. 4223	C-4470	C. 7527	0.6433	C. 1223	30 0 1173	0.4025	1-0000	
·ź	C.C	C. 0025	C. C1 C2	C. 0225	0.0420	C.2025	0.0900	0.1225	0.1600	C-2025	0.2500
	0.3025	C+ 360C	C. 4225	0.4900	0.5625	C.6400	0. 72 25	0.6170	0.9725	1.0000	
3	C•C	0.0025	C. 01.00	C. 0225	C-0400	0.7625	0.0930	0-1225	0.1606		0.2500
	0.3025	0.3600	C. 4225	C. 490C	C. 5625	C.6400	0.7225	O. #100	C.9025	1.0000	
4	C.C	0.0025	0. C1C9	0. 7225	2.0400	0. ^525	C-C-OC	0.1725	0-1600	C-2075	0.2500
	0.3725	0,3600	0, 4275	Q-490C	0.5625	3,6477	C. 7225	0.1100	G. 9025	1.0000	
5	Ç•Ç	0-0025		C. 0225	5-0400	C-9625	0.2902	0.1225	0.1696	7. 2025	C. 2500
	0.3025	0.350C	C. 4225	0-4900	C. 5625	C-6400	0.7225	C. F10C	0.9325	1.0000	
<u>. </u>	C.C	0.0025	C. CICC	C-0225	C-C-0:	0.0625	3.3900	0.1225	0.1600	0.2075	0.2500
	C-3025	3.3600	G. 4225	0.4900	0.56?5	C-6433	0.7225	0-5100	0.9025	1.0000	
7	C.0	0.0025		C. C225	7.0407	0.0625	0.000	C-1225	0-1400	0.2025	0-2500
	C. 3025	C- 3603	C • 4225	C. +400	C.5625	0.6400	5.7225		0.9625	1.0000	•
8	C.C	9-0025	0. C1 CC	C. 9225	C.C400	(.0625).C900	0.1225	0.1600	0.2025	0.2500
	C. 3C25	C+363C	0. 4225	C-4900	2.5425		7725	0.4133	C. 9025	1.0000	•
9	C.O	C-0025	C-0:10	0. C 2 2 5	5.0400	0.2625	0.0900	0.1225	C-1650	C. 2025	C.2500
	G. 3025	3.36CO	C. 4225	G-4900	0.5625	0.4400	0. 7225	0.5100	0.9325	1	
10	C.3	0.C025	C. C1 ?9	C. 0225	C.C40C	0.0625	00000	0.1225	C-1600	0, 2025	0.2500
	0.3025	0,3600	0. 4225	C-4900	0.5625	0.6400	2.7225	0.8130	0.9025	1.0000	
11	c_o	C.0025	C. Cl Co	C. 0225	0.04C0	0.0625	0.0500	0.1225	0.1600	0.2075	0.2500
	0.3025	C. 3600	0. 4225	C. 4900	G. 5625	0.6400	3.7225	0.6130	0.9025	1.0000	
12	£.C	0.0025	6.0160	0.7225	C. 240C	0.0525	0- 3500	0.1225	C-16C0	0.2025	0.2500
	0_3025	3. 36OC	0, 4275	C. 490C	C.5625	0.6400	0.7225	C- 6 1 0 0	0.4054	1.0000	**********
1.2	0.0	(.0025	0. 01 00	0.0225	0.2400	0.0625	0.0900	0-1225	C-16CC	0.2025	C. 25CD
	C. 3C25	C.3600	0.4225	0.4900	C.5675	0.6400	3.7225	C. +170	C. 6452	1.0000	
1 	C.0	0.0325	C. CICO	0.0225	2.0400	0.0625	0.090	C-1225	0.1600	0.2025	0.7500
	ų. 3025	C+ 3600	C. 4225	C. 4 900	5625	C.6400	7.7225	0.8100	0.9025	1.0000	
15	c.e	0.0025	0.0100	0.0225	C.040C	C+0625	0.5700	0.1225	C-1670	C. 2025	0.2500
	C. 3025	C.3503	0.4225	C. 4900	* • 5625	2.6400	G. 7225	0.1100	0.9025	1.0000	•• • • • • • • • • • • • • • • • • • • •
16	C.O	C.C325	C. (1C)	C. C225	0.0400	C.C 525	0.0000	0.1275	0.1670	0.2025	C. 25CO
	G• 3025	C+3600	Ç. 4225	0-4900	0.5625	0. 6400	0.7725	C. 120	0.9025	1.0000	
17	6.C	0.0025	C. CLCO	0.0225	9-0400	0.7625	7.7900	0.1225	0.1500	0.2625	0.2500
	0.3025	0.3600	U. 4225	G- 4900	" C.5425"	0.6400	0.7225	0.4170	0. 4025	1.0000	
16	C.0	0.3025	C. C1 CO	0. 1275	C.C473	C. 7625	0.7976	0.1225	0.1500	C-2C25	C. 2520
- DII	C.3625	2.3600	0,4225	C. 4900	0.5625	C. 6400	0.7225	0.8100	0.9025	1.0000	
19	0.0	0.0025	C.0100	C. 0225	0.0470	6.2625	0.0922	0.1225	7.1600	0.2075	0.2503
,	0.3025	3.3620	0. 4225	0.4900	0.5525	0.6400	0.7225	0.0100	0.5025	1.0000	

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0,3025 0,3600 0,4225 0.4900 0,5625 0.6400 0,7225 0,8100 0.902 21 0.C 0,0025 0.0100 C,0225 0.940C C.3625 0.9900 7.1225 0.164 0.3025 0.3600 0.4225 0.4900 0.5625 0.6400 0.7225 0.8100 0.902 22 C.0 0.0025 C.0103 0.6225 0.0400 0.7625 0.0900 0.1275 0.164 0,3025 0.3600 0.4225 0.4900 0.4625 0.6400 0.7725 0.8120 0.902 23 C.0 0.0025 C.010C C.0225 0.7400 0.0625 C.0900 0.1225 0.164 0.3025 0.3000 0.4225 0.4900 7.5625 0.6400 0.7225 7.8170 0.902 24 C.C 0.0025 0.6100 C.0225 0.6400 0.0025 0.0900 0.1225 7.144 0.3025 0.3600 0.4225 0.4900 0.5625 0.6400 0.7225 0.8170 0.902	00 0-2075 0-25 25 1-0000 00 0-2725 0-25 25 1-0000
0_3325	25 1.0000 00 0.2723 0.25 25 1.0000 00 0.2C25 0.25
C, 3025 0.3630 0.4225 0.4930 0.425 0.6430 0.7725 0.8130 0.90 23	25 1.0000 00 0.2C25 0.25
0.3025 0.3900 0.4225 0.4900 0.5625 0.6400 0.7225 0.8100 0.900 24 0.0 0.0025 0.0100 0.0225 0.0400 0.0025 0.6400 0.1225 0.14 0.3025 0.3630 0.4225 0.4900 0.5625 0.6400 0.7225 0.8100 0.900	
24	75 1.000.0
• • • • • • • • • • • • • • • • • • • •	
25 C.O 0.0025 C.CICO C.0225 C.G-00 0.C-25 0.0900 0.1225 0.16	00 0.2025 0.25
0.3025 3.360C 0.4225 C.4900 0.5625 0.649C 0.7225 0.8100 0.90	100 - 00000
26	
27	
28 0.9 0.0725 C.CLC9 0.0225 C.C4C0 0.0625 G.C909 C.1225 0.16 C. 025 0.360C C.4225 C.4990 0.4625 3.6400 C.7225 3.8100 0.99	
29 0.0 0.0225 C.CICO C.2225 0.040C 0.3625 0.0400 0.1225 3.15 0.3025 C.3600 0.4228 C.440C 0.3623 0.6400 0.7225 0.6210 0.90	
30 C.9 0.0025 C.01C? 0.0225 0.0400 C.3625 C.3400 3.1725 0.16 C.3C25 C.3600 C.4225 C.9900 C.5525 C.64CC C.7225 0.21CO 0.9C	
31 C.C 9.0025 C_CIC9 G_0225 0.0400 0.0625 C_06909 0.1275 0.15 C_3025 0.3600 G_4225 G_4960 C_5625 C_6400 0.7225 G_8100 0.90	
32 C-3 0.0027 C-C1C3 0.0225 G-04C3 0.7425 0.09CC C-1225 G-16 C-2025 0.3600 0.4225 0.49GG 0.5625 0.6400 0.7725 C-61C0 0.90	oc c.2025 0.25
33 C.C 9.0025 C.C1C0 0.0225 0.0407 C.C425 0.0900 0.1225 0.16	ro 0.2025 0.25
C.3025 0.367C 0.4225 0.4909 0.5625 0.6400 C.7225 C.5100 0.90 34 C.3 0.0025 C.01C9 0.0725 0.0400 0.0625 0.0500 0.1225 0.16	00 C.2025 0.2
. G.3025 0.360C 0.4725 C.499C C.5625 C.6400 C.7225 0.8100 C.90	25 1.0000
35 C.C 0.0325 C.CICO 3.0225 C.9400 0.0625 0.3900 0.1225 0.16 C.3025 0.363C 0.4225 0.4400 C.5625 0.6400 0.7225 0.8100 0.90	00 0.2025 0.20 025 1.0000
36 C.C 0.CC25 C.OLC9 G.0223 0.040C C.C625 0.0900 0.1223 C.16 C.3025 C.360C Q.4225 Q.4900 G.5625 0.640C 0.7225 0.#100 C.9C	
37 C.C C.0025 C.CICO G.0225 C.0400 0.025 C.0900 0.1225 0.1 0.3025 0.3500 0.4725 0.4900 0.5625 0.4400 0.7225 0.8100 0.90	
38	
39 C.O 0.0025 C.C1C0 C.0225 0.0400 0.0425 C.090C 0.1225 0.16	on 0.2025 0.2
40 0.0 0.0025 0.0100 3.0225 0.0403 0.0625 0.0900 0.1225 0.14	00 0.2025 0.2
0,3025 0,3600 0,4225 0,4907 0,5625 0,6490 0,7225 0,7100 0,41 41 0.0 2,0025 0,0100 0,6225 0,0400 0,0225 0,1000 0,1225 0,10	
0.3025 0.3600 0.4725 0.4900 0.5625 0.6400 6.7225 0.4100 0.90	

	»ElGHT=	781.817	PTH	.01=******539	2.36	PANIC=	9639.15	·			
50	0.0 0.3025	0.0025	C+01C0 C+4225	C. 9775 0.4900	0.0497 C.5625	C.7625 0.6400	0.0°00 0.7225	0.1225 0.0100	0.9C25	0.2025	0.2500
	6.3025	0.3636	0.4225	0.4900	0.5625	0.6400	C. 72 25	0.8100"	C.9025	1.0000	
49	C.O	0.0725	C. 01CO	0.0225	C.0400	0.0625	0.0930	C-1225	0-1600	C. 2025	0.2500
48	C.O O. 3025	0.0025 0.3600	0. C1 CC	C. 0225 C. 4900	0.0400 0.5425	0.7625	0.3900 0.7225	0.1225	7.1609 0.9025	0.2025	C.25C0
ו•••	G. 3025	0.3400	C. 4225	C. 4906	C. 5625	C.6400	0.7225	2.F100	0. 9025	1.0000	03.2.300
47	0.0	0.0025	C. 51C5	0.0225	0-0-20	C.0625	0.2900	0.1223	0.1600	0.2025	0.2500
46	0.3025	0.0025 C.3600	C. C1C2 0. 4225	0. 4900	0.0400 0.5625	C.0425	3.29C0 0.7225	0.1225	0.1600	0.2723 1.0000	0.2500
	0.3025	C. 3600	G. 422 5	C. 4900	0.5625	2.6470	C.7225	0.e100	0.9025	1.0000	
5	0.0	0.0025	C. C1 00	0. 0225	0.6400	0.0625	0.0900	0.1225	0.1600	. 0.2025	0.2500
•	0. 3025	C+3600	0.4225	0.4903	0,5425	0.6400		0.6103	0.9025	1.0000	
.4	C.0	0.0025	C. CICO	C. 0552	7.0420	0.7625	0.09CC	0.1225	0.1620	0.2075	0.2500
	C.3025	C.3600	0.4225	C. 4900	0.5625	C.6400	0.7225	C. P1 CO	0.9025	1.0000	
3	0.0	0.9025	0.0100	C. 0225	0.0400	0.0625	0.0900	C-1225	0.1600	0.2025	0.2500
·	0.3025	0.3600	0.4225	0.4900	0,5625	0.6400	0.7225	0.1107	0,9025	1.0000	
5	C.C	C. ^025	O. 01 C3	0.0225	0.0400	0.6625	3.0406	G-1245	0.1600	C.2725	C. 2500

5	TREAML INE &	H1 DENSITY	₩2 U	Ee V	FLOW ANGIOL	P-STAT P-STAG	TEMP(R) T-STAG	WACH NO
	C+0	9.60294E-67	3.44851F-04	0-0	4. 3857	9297.2	559.44	0- 3771 9
	1.4000	9.66284E-03	35e.15	0.0	0.0	9925.9	57C.00	356.15
	0.23	1.29342E-03	0-45700	-1.039#15-02	31 * 0 . 6	9297.2	559,51	0.30614
	1.4002	4,69163E-Q2	354, 88	-7. ac73	-1.2ec3	9921,6	570+C0	354,64
	1.00	2.584891-03	G-9F743	-3.362716-02	6367.5	9297.2	559,72	0. 30300
	1.4000	5.676COF-03	251.05	-3.35273E-0?	-2.5194	9906-5	£70.07	351.39
		3-674431-23	1, 3251	-6. t 11 75t -02	0541.8	9297-2		C. 29769
	₹•25 1•4000	9.67195E-03	344.40	-22.743	-3.7760	9886.5	540.07 570.00	345.35
	4.05	5-161C4E-07	1.7309	-0-15232	12 706. -5.0 291	€ 207. Z 98° 6. 5	560.57	C. 5900
	1.4000	4-65344E-03	335-37	-29-513	-3.0241	40-6-3	570.00	336,67
	6-25	6.456CLE-23	2-2001	-C. 743CC	15699.	9247.2	540-14	C. 29673
	1.4000	9-570858-03	242-18	-37,640	-6,2773	9682.9	570.70	344.24
	5.00	7.768495-07	2.8519	-0.37645	19162.	9797.2-	55=.59	C. 31962
	1.400	9.657676-02	367.11	-48.458	-7-4196	9974.2	57C.00	37C-29
				2007-00		1000000		
	12-25	9.09631E-03 9.73322E-03	3, 6143 397, 34	-C.:5661 -61.191	22457. -a. 7548	9297.2	556.55 570.00	C. 34765
	16.CC	1.04775F-02	4,4303	-0.77973	25705.	9257.2	554.53	^. 37251
	1.4000	9.708665-03	424.62	-74,734	-9.9818	10237.	577.00	431.1
	20.25	1.17574E-02	5-12C3	-1.0138	29076.	9297.2	553.59	C. 39493
	1.4000	9.78514F-03	435,20	-86, 229	-11,200	1C29P.	570.00	443,0
	25.00	1-30c52E-02	5.6764	-1.2448	32723.	9297.2	553.53	0.34573
	1.4000	9.78631F-03	474,46	-95.582	-12.407	10302.	£70,00	444.8
							727 22	
1	30-25 1-400	1.43659E-02 9.75518E-03	6-2012 471-5-	-1.5007 -104.43	35 5 5 C . -1 3 . 604	9297.7 10298.	553, 59 570- 22	C. 3549
• • • • •								
}	36.0C	1.56559E-D2	6.6896	-1.7637	38 759.	9207.2	553.87	C- 3877
	1.4000	7.7a1216-03	426.33	-112-55	-14.759	10763.	570.00	440.9
	42.25	1.657426-02	7.1861	-2.0552	41984.	9297.2	557.46	C. 3816
	1.4000	4.78342E-03	423.35	-121-08	-15.961	10240.	570,00	440.3
.	49.00	1.428616-02	7. 7401	-2.3539	45235.	4297.2	*51.67	0.3939
٠	1.4300	9.743761-23	423.28	-130,37	-17.119	10243.	F70.00	442.9
•	56-25 1-4CUJ	1.55901F-02 7.78274E-03	8. 224 B 41 5. 85	-2.7142 -138.45	46459. -1*.263	9297.2 102#9.	551.73 570.00	0.3432 442.1
		101 101 101 03						
t	64-00	2.068356-02	R. 6195	-3.3341	51647.	9797.9	554.06	0. 3792
	1.4000	9.776858-03	417.74	-145.28	-1<.352	12267.	570.00	437.5
	72.25	2.21657E-CZ	6.9192	-3-335R	54 796. -20. 50a	4247.7 10230.	534-64	0.3721
	1.400n	9.76674E-03	472-39	-150-49	-20 • 50 <u>•</u>	Instant	570-00	429.6
	61.CC	2.34679F-02	9, 361 9	-3.7073	59013.	9 297 • 2	554.68	C-3716
	1.4000	9. 76605E-03	398.03	-157.97	-21.604	10228.	570.00	429.0
<u>. </u>	90-25	2.47351F-02	5. 5265	-3.0822	61111.	¢ 297. 2	555.49	C. 3613
- 	1.4000	9.75166E-03	395-16	-161.00	-22,685	15175,	570.00	417.4
	100.55	3 541105 65	0.6170	-4-1879	44130	0307.3		
l l	10C+CO	7.5982CF-02 9.73110E-03	9.5179 356-33	-161.18	64139. -23.740	9297.2	556.67 570.00	0.3460 400.2

STREAMLINE & CP/CV	M1 DENSITY	h2 U	h3 Y	FLCW ANGEOT	F-STAT P-STAG	TEMP(R) T-STAG	MACH NI VFLOCIT
1.4000	9.57255E-07	3.79981E-04	0.0	2. 3627	9149.3	556.89 573.00	0.34315
1.4000	A* 2/522F-C3	346.42	C. O	0.0	772767	211000	340.42
0.25	1.23643E-03	0-48935	-1.076636-02	3051.7	4149.3	556.95	C-34222
1.4000	9+57136E-03	395,80	-4.7075	-1.2603	9921.5	572.00	395.89
1-00	2.47C97E-03	C. 96 94 4	-4-26552E-C2	6097.8	9149.3	557.16	0.33941
1.4000	9.567778-03	392.33	-17.263	-2.5194	9908.5	572.00	392.71
2.25	3-7C360E-C3	1.4314	-c_44745E-02	9137.5	9149-3	457-51	0-33465
1.4000	5-56178E-33	394.49	-25.508	-3.7760	9886.8	570.00	387.31
4 00	/ CANEER 02		-0.14410	12168.	0140.7	55 R. OC	
4-3C	4.53355E-73 9.55337E-03	1. P658 376.19	-0.16419 -32.281	-5. 2291	9856.4	570.00	0.32781 379.65
		mar Berney	1 = 1110000				
6.25 1.400G	6.171436-03	2,3701	-0.26371	15275.	9149.3	557.5E	0.23379
1. 4000	9.5507CE-03	354.04	-42.244	-6.2773	9852.9	570.00	386.35
5,00	7.4 26C6E-03	3, C158	-C.39678	1034C.	9140.3	556.03	0-35439
1.4000	9.507216-03	406.11	-53-606	-7.5196	9979.2	570.0¢	409.6
12.25	9.695338-02	3.7676	-C.58021	21505.	9149.3	554.00	0.3799
1.4070	9-622366-03	453-29	-66.727	-8.7548	10104.	572.00	438,49
16.00	9.973598-03	4.5688	-0.80411	24701.	9149.3	551.99	0-4938
1.4000	9.6 5741£-03	45 e. 09	-60.624	-9.9418	10237.	570.00	465.1
2C. 25	1-12391E-02	5.2586	-1.0412	27955.	9140.3	551.06	0.4145
1.4000	9.67368E-03	467.89	-92,642	-11.200	10298.	570.00	476.9
25 60	1.244925-02	5. e2e0	-1.2522	30957.	9149.3		0 4171
25.CQ	9.674845-03	406.65	-102.66	-12.457	10302.	551.00 579.00	0.41 52 477.8
		110-110-1					
30.25 1.4000	1.37365E-02 9.67373E-03	6.2696 467.62	-1.5412 -112.20	34042. -13.504	10296.	551.06 572.00	0.4145 477.0
36.00	1,457916-02	6.6675	-1.8139	37116.	9149.3	551.28	0-4120
1.4300	9.66980F-03	450.47	-121.04	-1787	10263.	570.00	474.1
42.25	1.62259F-02	7.3886	-2.1131	47204.	9140.3	551.33	0.4114
1,4000	4.669021-03	455,36	-130 <u>-23</u>	-15.961	10540*	570-00	4.73.6
49.00	1.748301-02	7,9517	-2.4401	43317.	9149.3	551.14	C.4136
1.4050	9.672316-03	444.91	-14C-11	-17.119	10263.	577-00	475.9
56.25	1.87265E-C2	9-4518	-2.7891	40494-	0140.3	551.20	0.4129
3.4000	9.671316-03	451,33	-148.04	-18,763	10289.	570.00	474.2
64.00	1.954296-02	8, 2702	-3-1223	49457.	9149.3	551.53	C-4091
1.4000	9.665506-03	444.34	-156.41	14. 792	10267	570.00	471.7
72.25	2.11866-72	5.2026	-3,4418	32474.	9149.3	557.10	0-4076
1.4000	9,655491-03	434.33	-162,44	-27.506	10230.	570.00	463,7
81.00	2-243335-02	9. 661 4	-2.825 °	55555.	9149.1	552.14	0.4021
1.4000	9.654816-03	430.67	-1 70.55	-21.404	10228.	570.00	463.2
90.25	2.36447E-02 9.64059E-03	5.8720 417.51	-4.1265 -174.52	5F520. -22.685	°149.3 10175.	557.96 570.00	0.3925 452.5
		71 '• ZL	» 170 74			2: 3*3!9	7.24.4.7.
100.00	2.4236cF-C2	5. 9288	-4, 3687	61420-	9149.3	554-12	0.3785
1.4000	9-623261-03	399.76	-175.90	-23.749	16100.	57C.OC	436.7

STREAMLINE & CP/CV	#1 DENSITY	₩2	, <u>, , , , , , , , , , , , , , , , , , </u>	FLOW ANGLO)	P-STAY P-STAG	TEMPIRI 7-S7AG	MACH NO VELOCITY
0.C 1.4CCO	9.43457F-07 9.43457E-03	4.18C18E-04	0.0	2.3339 C.3	8965.2 9925.9	553.66 575.00	0. 29414 443. C7
0.25	1.17591E-C3	C. 52C22	-1.14449E-GZ	2911.3	6965.2	553.73	0.3633C
1.4900	9,433395-03	442.C2	-9.7245	-1.2603	9921.5	470.00	442.13
1.0¢	2.35199F-73 9.42985t-03	1.0322 436.67	-4.54174E-02 -19.310	-2.5194	9951,2	55% 94 570.00	0.38077 437.30
2.25	3.52532F-C3	1.5235	-0.1 00e8	8717.0	6065.2	554.28	0.37652
1.4000	9.42395t-03		-28.617	-1.7760	9886.8	573.00	434.52
4.00 1.40C0	4.69597E-73 9.41567E-03	2. CCC9	-0.1760F	1160E. -5.0291	8965.7 9856.5	554.77 573.00	0.37C47 427.73
1.40(0	5. 87422L-03	2.5321	-0.27954	14525 .	8945.2	554.35	0.27575
	9. 42 289E-03	411.40	-47.416	-6. 2773	9852.9	570.00	437.66
9.00	7.06843E-02	3.1843	-0.42713	17496.	#965.2	552.51	0.39427
1.400G	4.44902E-03	45C.49	-59.405	-7.5196	979.2	570.00	454.40
12.25	8.27657F-03	3. 52 03	-0.60512	20515.	6°65.2	550.79	C. 41 754
1.4000	9,45366E-93	474. 75	-73.112	-8.7548	10108.	570.00	482.35
14.90	9,49376E-03	4.7190	-0.f3054	23563.	8965.2	548.80	0.43953
1.4000	9,51821E-03	497.09	-47.4*9.	-9.9318	10237.	570.00	
2C.25	1.06578E-02	5.4107	-1.9713	26570 .	F965.2	547.87	C. 44936
	9.53424F-03	505.78	-100.14	-11.200	10298.	=70.00	515.60
25.0C	1.10075E-C2	5. 9951	-1.2189	29527.	8965. Z	547.81 .	0.4500°
1.4000	7.53538E-03	504. 31	-110.95	-12.407		570.00 .	516.3
30.25	1.30747F-02	6.5527	-1.5357	32474.	8905.7	547.87	0.4494
1.4003	9.53428E-03	577.16	-121.28	-13.604	10298.	572.00	515.6
76.00	1.42577E-02	7.0723	-1.0671	35476.	10263.	549.09	0.4470
1.4000	4.53041E-03	496.34	-130.95	-14.789		570.00	513.0
1,4000	1.54445E-02	7.6103	-2.17e6	36353.	8965.2	548.14	C. 4465
	4.52764E-03	492.75	-140.93	-15.961	107?0.	577.00	512.5
49.00	1.66391F-02.		-2.5207 -151.50	4:3?2. -17.119	8965.2 10293.	547.95 570.00	n. 4485 51 4. 7
56.25	1.70246L-32	P.7C39	-2.6713	44267.	8965.?	54 %. C1	C.4479
1.+000	9.53193E-03	486.14	-161.09	-18.263	10289.	570.00	514.0
64.00	1.90015E-02	5. 1439	-3.7187	47179.	8965.2	548.34	0.4446
1.4000	9.52617E-03	481.22	-169.39	-19.362	10267.	570.00	
72.25	3.01-91E-03	9,5098	-3.5567	50056.	8945.2	548.90	0.43836
1.4000	5.01-91E-03	471,53	-176.35	-20,506	10230,	57C.00	503.4
1.4007	2.13579E-02 9.51564E-03	9, 5854 457, 64	-3.4542 -185.18	-21.604	8965.2 10228.	548.94 570.00	0.43794 502.91
90.25	2.25C59[-C2	10.241	-4,2808	55825.	8965.2	54°, 75	0.4291
1.4000	9.50162F-0]	455.05	-190.21	-27.585	10175.	570, 00	493.20
100.00 1.400	2.364055-02 9.46157E-33	10.362	-4.5592 -192.85	59593. -23.749	8965.2 10100.	550.91 570.00	0.4167

	CP/CV	DENS 17Y	U					
			 	V	FLOW 4NG(01	P-STAG	T-STAG	AET OC! A
	0.0	9.258556-07	4.55427E-C4	0. n	2. 2976	5731.9	549.50	0.43184
	1.4000	5.25255E-03	496.22	0.0	0.0	9925.9	570.CO	496.22
	0.25	1.1140ai-03	6.55177	-1.21348E-02	2743.5	8731.9	549.57	0.43109
	1.4900	9.257396-02	495,27	-1 (-, 696	-1.2603	9921.5	570,00	495.31
	1.00	2.2264FE-03	1.0963	-4. AZ366E-02	5522.4 -2.5194	8731.9	549.78 570.00	0.42883
	1.4000	9.253931-93	497.40	-21.666	-2.5194	9908.5	570.00	492.80
	2.25	3.337C5E-33	1.4272	-0.10739	4275.3	8731.9	557.12	C. 425C
	1-4000	0, 24813F-03	497.60	-32-162	-3.7762	9886.8	570.00	486.66
-	4.CD	9.24COGE-03	2.1273	-C.18809 -42.312	1102C. -5.02C1	2731.9 9856.4	552.61	C. 4196
	1.4000	9.24005-03	49G-02	-42.312	38 8			482.6
	6.25	5.562516-03	7.6957	-C. 2 9664	13709.	E721.9	550-19	C. 4243
.	1.4005	9.24739E-03	454, 57	-53.347	-6.2773	992.9	570.00	447.9
	9.00	6,690932-03	3.3564	-0.44321	16409.	P731.9	548.66	F. 4409
	1.4000	9.272736-03	501.93	-66.255	-7.5196	9979.2	570.00	596.2
	12.25	7. 834 545-33	4-1003	-0.63144	19475.	8731.9	546.66	2.4620
	7°+0c6	9, 1267st-03	527.36	-ac • • • 7	-3.7544	10176,	572.00	529,5
	16.00	8.966226-03	4, 8815	-C.85915	22358.	8731.9	544.68	0.4871
	1.4000	9.340626-03	543.22	-95.607	-9.4818	10237.	572.00	551. 9
	ZC. 25	1.01264F-02	5.5773	-1.1743	25222.	P731.9	543.76	0.4413
	1.4000	9.35e3eE-03	55C, 77	-1C % 05	-11.200	10298.	57c.00	561.4
	25.00	1.12528E-C2	6.1782	-1.3592	28029.	6731.9	543. 70	0.4918
	1.4003	9.3574bE-03	549.03	-12c.79	-12.407	10302.	570.00	568.1
	30.25	1.23766E-02	6.7544	-1.6346	3:827.	8731.9	542.76	C.4912
	1.4000	9.35647E-03	\$45.74	-132,07	-13-604	10268.	570.00	561.4
	36.0C	1.34962E-02	7. 2951 54C.60	-1.9262	37511. -14.789	5717.9	543,98	C. 4890
	1.4000	9.35261E-03	540.60	-142.72	-14.789	19283.	570.00	559.1
	42.25	161966-92	7. 2524	-2.2458	36437.	6731.9	544.02	0.4886
	1.4000	<u>9-351</u> 85 <u>6-03</u>	537,12	-151-61	-15.961	10280.	577.70	558.6
	49.00	1.574956-02	2.4366	-2,5001	39 226.	6731.9	543, 84	C. 4904
	1.4000	9.35504E-03	535.80	-165.03	-17.119	iczej.	570.00	560.6
	50.25	1.657266-02	b. 4733	-2.9612	42522.	2737.0	547.89	G. 489
	1.4000	9.35406F-03	531.83	-175.50	-18.261	10219.	570.00	560.0
	64.00	1.79966F-02	9.4419	-1.3236	44 786.	6731.9	544.22	0.486
	1.4000	9.3484-6-03	524.44	-144.76	-14.307	16257.	570.00	556.5
	72.25 1.4000	1.5040+1-02	9.6417	-3.6879 -1.72,80	47517.	8731.9	54 % 78	0.4610
·		9,33816t-03	515.52		-20 •50 <u>•</u>	10230,	570,00	550.3
	1.400	2.021246-02	10, 335	-4.0928	50 30 7.	8731.9	544.82	0.480
		9.338116-03	511.34	-202.49	-21.604	10228.	570.00	549.
	90.25	2.13039E-02	10.636	-4.4460	52995.	8731.9	544.63	0.472
	1.4000	9.334755-03	499.20	-204.69	-22.685	10175.	570.00	541.1
	100.00 1.4000	2.23778E-C7	17.819	-4,7697 -212,72	55622. -23,749	6731.9 10100.	546.78 570.00	C.460

	STREAMLINE & CP/CV	DEMSITA	u 2	h3 V	FLOW ANGEOL	P-STAT P-STAG	TEMP(R) 7-5TAG	VELOCITY
	C.D	9.0267CE-07	5.04905E-04	0.0	2.2400		*** **	12741170
	1.4000	9-226708-03	559.35	C. 0	2. 2480 0.3	9925.9	543.96 579.00	559.35
	C.25 1.4*^^0	1.04m33E-03 9.02 57E-03	C. 56436 258,48	-1.28555E-02 -12.287	2605.7 -1.2603	8427-3 9971-6	544.C3 570,00	C.45859 556.61
	1.00	2.04398E-03 9.02218E-03	1.1623 555.87	-5-11421E-02 -24-458	5206.4 -2.5194	6427.3 9908.5	544.23 570.00	0.48657 556.41
	2.75 1.4000	3.13436E-03 9.31654E-03	1.7285 551.52	-0-11476 -35-400	7AC1.8 -3.7763	8427.3 9866.8	544.57 570.00	0.48319 552.72
	4.30	·.174775-03	2.2768	-0.22036	15386-	8427.3	545.05	0.47841
2	1.4005	9-00961E-03	545.38	-47.994	10359. -5.0291	9856.4	570.00	54 7.49
,	t.25	5-232348-03	2. E657	-C. 31522	1330C.	E427.3	544.63	0.48758
	1,4909	9-015528-02	544.74	-67-362	-6,2773	9682-9	579.00	552.D5
,	9.00	6-28358E-03	3-5298	-0.46726 -74.358	15655.	6427.3	543.13	0.49739
	1.4006	5.C4052E-03	*63.32	-14.358	-7.5156	9975.Z	570.00	568.71
3	12-25	7.357-2E-03 9.0/3-45-03	4, 2819 591, 94	-0.65941 -89.619	1636C. -8.7548	8427.3 1C108.	541.14 572.00	C. 51 636 58 8. 80
2	16-00	5.4395*E-03 9.10e71E-03	5. C578	-0. 49017 -105.45	21067. -9.9818	10237.	539-18 579-00	0. 53461 608-51
)	20.25	9.510386-04	5. 7598	-1.1404	23778.	8427.3	528.27	0.54281
	1,4000	9,122065-03	675.64	-119.92	-11 -200	10298.	570.00	617.39
١	25-00	1.05602E-C2.	6.3785 603.59	-1.4034 -132.79	-12-407	A427.3 10302.	538.21 570.00	0.54346
	1-4000	V.12317E-03	673.34	-132.14	-1207			018.02
2	30.25	1.16236E-C2	6, 5753	-1.6500	79261.	8427.3	527.27	0.54290
	1-1200	9-12210E-03	67C-10	-1-5-22	-13.604	10206.	<u> </u>	617.45
3		1,25751E-02 9,11,40E-03	7.5406 594.91	-1.9707 -157.04	31 6 5.	8427.3 10283.	530.49 570.00	C.5409
_	1.400	•						
4	1.4000	1.37302F-32 9.11765E-33	1103 -71,1:	-2.3214 5.5	34322. -15.961	8427.3 10280.	52 F • 53 570 • 00	0,5405 614.8
_	49-G0	1.47=138-32	e. 7171	-2.6849	J779.	8427.3	#10 >#	C. 5421
5	1.4000	9.1:1778-03	584.34	-181.52		10293.	570.00	616.60
4	56.25	1.525 E-7 9.11042E-4	2712	-3.0595	34615.	9427.3	570.00	C.5416
	1.4000	401: 126-6	585.08	-193.07	-1: • 263		516.06	616.1
J.,	64.CQ	9-1143 -03	7. 7057 278-17	-3,4379 -203,52	-19.392	10267.	570-00	0.5387
6:	72.25	1.7429 -02	ineici	-3.8157	4776.	642743	529.29	0.53363
	3.4000	9.1046 03	568.96	-212,79	-20,506	10230,	577, 20	607,45
₹	#1.00	1.89827E-02	17,714	-4.7479 -223.51	47426. -21.604	10229.	539,37	0.53321 607.01
	-	1,111			****			17/2 1.3
0	90.25 1.4000	2.00074E-02 9.09085E-03	11.C60 :52.80	-4.6232 -231.07	49960 <u>-</u> -22-685	#427.3 10172.	540-12 570-00	C. 5259 599.1
-					- 1111111111111111111111111111111111111			
ı	1,4000	7.10164E-02	11.304 537.84	-4. 9715 -236.65	52437e -23e749	6427.3 10100.	541.26 573.00	9.5152 587.4

S	TREAMLINE &	#1 DENSITY	112 U	, w3	FLOW ANGEOD	P-STAT P-STAG	TEMP(F) 7-STAG	MACH NO VELOCITY
	0,0	8,70569E-07 8,70569F-03	5,55284E-C4 637,84	0.0 0.0	2. 1799 C. O	8910.7 9925.9	534,14 570.00	0.56197
	C.25	9.75694F-04 8.70460E-03	C.61838 637, 25	-1.36044E-22 -14.015	2439.4 -1.2693	8010.7 9921.6	536.20 570.00	C. 56138 637,21
	1-00 1-400	1.93979E-03 8.70134E-03	1.2312	-5.41715F-12 -27.926	4a56.C -2.5194	#010 ₀ 7	534.40 57C.00	0,5596C 635.31
	2.25	2.977436-03	1.8339 63C.75	-0.12103 -41.629	7276.7 -3.7760	801C.7	536-74 570-00	0.55662
	1-4690 4-90	4,65589E-Q3 3,87287F-Q3	2. 4213	-0.21308	9689.9	9886.8 F010.7	537.21	632 <u>.12</u> 0.55241
	1.4000	6.68825E-03	625.20 3.0412	-55.018 -C.32454	-5.C291 12125.	9856.4 8C10.7	571-00	627.62
	1.4000	8.65451E-03	627.76	-09.053	-6,2773	9965.9	571.00	631.55
••••	7. QC 1.4000	5.82945E-03 8.71902E-03	2, 7326 63 9, 96	-C. 49244 -84.475	-7.5196	9979.2	535.32 570.00	0.56916 645.51
	12.25 1.4000	6.62582E-03 8.75097E-03	4.4759 653,73	-C.68929 -100.98	17123. -8.7548	8010.7 10108.	533.36 570.00	0,58606 663.46
	16-00	7.82922F-03 8.78246E-03	5.2491 67C.45	-0.92384 -118.00	19666. -9,9618	8010.7 10237.	521.42 570400	0. 60247 680.76
	20.25 1.4000	8.82259E-03 8.79766E-03	5. 9595 679.48	-1.1870 -132.75	22175. -11.200	8010.7 10298.	530.53 570.00	0.60986
	25.00 1.400C	9.8C395E-03 8.79871E-03	6.5926 673.06	-1.4517 -148.07	24643. -12.407	8C10.7	520.47 570.00	0.61041 689.19
	3G-25 1-4CC0	1.0783CE-02 8.79770E-03	7-2171 669-30	-1.7465 -161.97	27103. -13.664	801C.7 10298.	520.52 570.00	C.60991
	36.0C	1.17564E-02 8.79413E-03	7, 1075	-2.0612 -175.29	2455C. -14.789	#010.7 10283.	530.74 570.00	0.6G81
	42.25	1. 27372F-G2	8.4053	-2,4039	32709.	401C-7	520.79 \$70.00	0.6077
·	49.00	8.79341E-03_ 1.37216E-C2_	9.0215	-188.73 -2.7786	-15.961 36487.	8010-7	530-61	0.6092
_	1.4000	6.79642E-03	657.47 5.5968	-202.50 -3.1669	-17-119	10203.	570.00	0-6263
	1.400G	8.7955CL-G3	652,84	-215,44	-18,263	19289.	570-00	687,4
	1.4000 72.25	1.567C7E-02 8.79021E-03 1.5632tE-C2	10-121	-3. 5624 -227.35 -3. 9610	39376. -14.392 -61777.	5010.7 10267. 5210.7	530.98 570.00	0.6061 684.6 0.6015
	1.4000	8.781128-03	636, 75	-238,14	-20-506	10,230.	\$70,00	679.8
	#1,00 1,4000	1.76099E-07 8.78049E-03	631.76	-4.4056 -250.18	-21.604	#010.7 10228.	570.00	679.4
	9C.25 1.4000	1.856CEE-02 2.7675eE-03	11.517 620,50	-4. 9141 -259.37	46594. -22.689	8016.7 10175.	532.35 470.00	0.5946 672.5
	100.00	1.94964E-02	11 .821	-5. 201 2 -266. 78	49905. -21.749	6010.7	573.48	0.585C

SIREAMLI CP/C		#1 DENSITY	h2 U	h3	FLOW ANGLOS	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VELOCITY
1.40	00	8.21459E-C7 8.21459E-03	6-11817E-C4 744.79	C.O	2.0742 0.0	7285.3 9625. 9	523.83 570.00	0.66387 744.79
	.25	8.796326-04	0.65452	-1.43994E-02	2220.9	7385.3	523.09	C. 66335
1,40	000	0.21356E-93	744, 69	-16,370	-1. 2603	9921.6	573.00	744.26
1.40	00	1.7577AE-C3	1.3042	-5.73847E-02	4437.6 -2.5194	7365.3	524.09 570.00	742.67
- 70	2. 25	2.63401F-03	1.5454	-0-12940	6649.7	7355.3	524,42	0.65923
1,40		#.20535F-03	736,41	-46.735	-3 - 1760	9826.6	570.00	740.01
	00	3.50946F-03	2.5739 733.43	-0.22651 -64.541	8854.9 -5.0251	7305.3	524.86 579.00	C. 65560 736.26
				777 61	11280-	7365-3	524-4 B	C. 55 977
1.45	25	4.28993E-G3 -38993E-G3	3.2:71 735.10	-C.35498 -87.867	11780. -6.2773	9882.9	57C-00	739,54
	9. <u>CO</u>	5.282425-03	3.9342	-0.51931	13345.	7345.3	523.03	C. 67011
1.44	oco	8.227176-03	744.77	-98.309	-7.5196	9979.2	£70.00	751.23
	2.25	6.10520F-03 8.2°T34F-03	4.6848 757.42	-0.72147 -136.64	15646. -8. 7548	7355.3 10108,	521.12 570-00	0.68485 766.35
1.4	5.03	7.C5452F-03 8.20741L-03	5.4572 769.21	-0.96046 -135.38	17969. -9.9815	7385.3 10237.	51 %, 23 570, 00	C. 69924
	0.25 0GC	7.95468E-03	6-1776 772.72	-1.2232 -153.00	20261. -11.200	7385.3 10298.	51 9. 35 570.00	0.70582 787.72
	5.00	0.00394E-03 0.30237E-03	6.8307	-1, 5045 -169, 35	22516. -12.407	7185.3 10302.	518.29 570.00	0.70621
	0.25	9-771126-03	7,4611	-1.0104	24764.	7305.3	510.35	C. 70584
1,4	000	0,30141E-03	765,64	-185428	-13,604	10298.	570.00	787.74
	909 6•0 <u>6</u>	1.06550F-02_ 8.295046-03	8, CORB 764, 09	-2.1361 -200.66	27C00.	7385.3 10283.	513.56 572.00	0.70426 786.13
	2.25	1.15419F-02	6.7201	-2.4940	29247.	7385.3	51 0. 60	C. 7039
	9C <u>2</u>	8.29737E-03	755.52	-216.08	-13.961	10260.	570,00	745.9
	9.00 000	1.24739F-02 0.20020E-03	752.29	-2. #810 -231.70	-17.119	7385.3 10293.	570.00	0.70524 787.10
	6.25	1.33206E-02 8.29934E-03	9.9521 747.12	-3.2842 -244.55	33757. -18.263	7385.3 10289.	518-49 570-00	0. 7048 786.7
	4.C0	1.42901E-02	10,506	-1.69A2	35978.	7 30 5 . 3	510.79	C. 7025
1.4	000	8.294356-03	739.87	-260.43	-19.392	10267.	570.00	784.3
1.4	2.2: QCQ	1.50719E-02 8.28576E-03	11.015 73C, 80	-4.1194 -273.32	36173. -29,506	7365.3 1023C.	51 % 33 570,00	C.6984 780.2
	1.00	1.59573F-C2	11.572	-4.5874 -287.17	40414.	7305.3	51 9, 37 570, 00	0. 6981
	C-25	1.661906-32	12.011	-5.0207	42574.	7305.3	520-13	0.6923
	6 00	5.272958-03	714,15	-296.52	-22.685	10175,	570,00	774,0
	000 0.00	1.76669F-07 8.25554E-03	17,378	-5.4464 -378.26	44687. -23.749	7365.3 10100.	521.23 570.00	<u>C. 6639</u>

S	TREAMLINE & CP/CV	DENSITY	u 2 U	v 13	FLOW ARGEON	P-STAT P-STAG	TEHP(R) T-STAG	MACH NO VELOCITY

L	0.0	7,1C743E-C7	6. 77561E-04	0.2	1,8306	6030.4	494,39	0,87470
	1.4000	7.137406-03	953.32	0.0	0.0	9925.9	570.00	953.32
1	0.25	7.296976-04	C.64516	-1.529398-02	1079.3	6C30-4	404.42	0.87428
	1.400 <u>6</u>		952,70	-2c.959	-1.26Q3	9921.6	57C.00	952,93
<u> </u>	1-00	1.45814E-C3	1.3864	-6-10036E-02	3754.9 -2.5194	6030.4	494.60	9. 87304
	1.4000	7.10305F-03	950, 83	~41.837	-2.5194	9905.5	570.00	751.75
	2.25	2.16549E-03	2.0713	-0.1357C	5626.7	5030.4	454.51	0.87098
	1,4600	7,099408-03	947,74	<u>-62.551</u> .	-3, 7760	9885.5	57C.00	949.80
	4-00	2.911186-03	2.7464	-0.2414	7492.9	4C30-4	495.35	0. 86 807
	1.4066	7.093176-03	943.40	-83.019	-5.0291	9856.5	570.00	947.04
,	6.25	3.64159E-C3	3.4368	-C. 37804	9175.3	6730.4	494.57	C- 67060
	1-4000	7.039616-03	943, 75	-1 23 . 81	-6.2773	9502.9	:76.00	949,45
<u> </u>	9,00	4.381886-03	4. 1620	-0,54739	11 291.	6030.4	493.60	0. 97973
	1.4000	7.118298-03	949.83	-125.38	-7.5196	9979.2	£70.00	958.07
	12.22	5.13081E-C3	4. 9154	-C. 75697	13237.	403C.4	491.40	0.89168
	<u> </u>	7,14439F-03	55 8 , 01	-147,53	-8.7544	rctos*	570.00	969,31
	16-09	5,855C4F-03	5.6410	-0.99999	15201.	6010.4	490.01	0.90343
	1.4000	7.17041E-03	965.46	-159.92	-9.9518	19237.	570.00	960-30
,	20.25	6.631738-93	6-4101	-1.2692	17139.	6030.4	487.19	0.90884
	1,4000	7,142496-03	966,57	-191.38	-11.200	.10208.	570.00	985.34
l	25,00	7.369396-03	7.0043	-1.5608	19046.	6030.4	489.13	0. 90922
	1.4000	7. 1b335E-03	902.48	-211.79	-12.407	10302.	570.00	985.70
2	3C. 25	6.105328-03	7.7625	-1.8785	20948.	6030.4	489.18	0. 90 886
	1.4000		957,71	<u>-2:1.77</u>	-13-604	10298.	5,7c•0 <u>0</u>	985.35
3	36.00 L-4000	8.834536-92	6.4102	-2.2203	22840. -14.789	603C.4	489.34	0.90755
	1.4000	7.17961E-03	951.54	-251.21	-14.789	10563.	570.00	984.14
4	42.25	9.57423E-03	9.0569	-2.5903	24740.	6030.4	489.42	0- 90729
	1-4000	7,17903E-03	945.97	-270-55	-15-961	10260.	570.CD	983,90
5	49.00	1.031426-02	5,7086	-2, 9902	26655.	6030.4	489.25	0. 90839
	1.4000	7.16148E-03	\$41.28	-269.92	-17.119	10293.	370.00	984.92
	50.25	1.10497F-G2	10.332	-3.4094	28555.	503C.4	-489.31	C. 90FO
	1,4000	7-180736-03	935.01	-378,55	-16-263	10269.	570-00	984.61
₹	64.00	1.17792E-02	10.920	-7. 8438	30434.	6032.4	489.60	0.9061
	1.4000	7.1764LE-03	927.06		-14.592	10267.	373.00	982.01
	72.25 1.4000	1.25324E-C2 7.16098E-03	11.473 917.63	-4.2907 -343.19	32292. -20.506	6030.4 10230,	490.11 570.00	0.90279 979.70
-				- ,		705		
9	1.4000	1.32369E-C2 7.16540E-03	12,055	-4.7736 -360.63	3418% -21.604		490 <u>-14</u> 573-00	979.45
	_		F2 -5-14141	1000	100	3837	5.4019/5550	
0	90.25	1.395146-02	12.551	-5. 2464 -376.04	36017. -22.685	6030.4 10175.	490.87 570.00	0.8978 975.0
	1-4000	7. 1579ZE-03					25 46	
1	10C.OC	1.46549F-0Z 7.14283E-03	12.993	-5 <u>, 71 79</u> -390, 11	37806.	6030.4	491.90 570.00	0.6909°

			-STATION MO. = 1			III yayay		757 1025
	TREAMLINE \$	%1 OENSITY	#2 U	N)	FLOW ANGED)	P-STAT P-STAG	TEMPIR) 7-STAG	MACH NO VELOCITY
	0-0	5.664526-07	6. 909798-64	0. 0	1.5473	46^7.6	457.77	1-1072
	1.4000	5.06452E-03	1161.2	0.0	0.0	4925.9	570.00	1161.2
	0.25	5.6921E-04	C.40483	9-1-502E-04	1556.4	4607.6	457.A3 570.00	1.1068
	1-4-000	5,66379E-03	1160.9	1.5502	7,55110E-02	9921-5		1140.9
	1.4003	1.178#1E-C? 5.60159E-C3	1.3674 1160.0	3.652092-03 3.0780	?109.7 C.15302	4607.6 4928.5	458.77 570.00	1.1058
	7.25	1.702625-03	2. C469	6-19993E-03	4657.9	4607.6	453,79	1.1045
	1.4000	5.25792E-23	1150.5	4,6411	0.22953	9884,8	57C.00	1158,5
	4.00	2.35350E-G3 5.85278E-G3	2,7216	1.45373E-02	6205-6 C-30604	4637.6 9856.4	458.69 576.00	1.1015
	1.4000		1156.4					
	6.25 1.4000	2.941985-03 5.857276-03	7.4C98 1158.2	2.27665E-02 7,7332	7764.4 0.38255	4627.6 9882.9	458.34 570.00	1.1037 1158-2
	9.0C	3.54245E-G3	4-1261	3.305936-02	9350.5	4607.6	457.07	1.1115
	1-4000	5.8735[E-03	1164.8	9. 3321	0.45906	9976.2	570-00	1164.6
	12.25	4.14792E-33	4. Et 65	4.54933E-C2	10961.	4607.5	455.40	1.1217
	1.4000	5,59564t-33	1171-3	10.966	C.53556	10178.	579.00	1173.4
••••	16-00	4, 75765E-C3	5.6223 1181.7	6.00628E-02	12585. C. 61207	4607.6 10237.	453,79 579,00	1,1316
	20.25	5-3-1316-33	6-3563	7.63924E-02	14169.	4607.6	452.98	1,1305
	1-4000	5.92648E-03	1185.4	14,749	2.68857	10298.	570.00	1185.7
 -	25-00	5-957656-03	7. 0649	9.434276-02	15768.	4607.6	452,93	1,1360
	1.4000	5.92719F-03	1185.8	15.875	0.76506	10302.	577.00	1186.0
	30.25 1.4000	6.55260E-03 5.92651E-03	7.7685 1185.6	0.11411 17,415	17342. 0.64154	4607.6 10298.	452.98 £73.00	1.1365 1105.7
	36.03	7.14533E-03	8.4644	0.13564	18938.	4607.6	453.17	1.1354
	1.4000	5.92410E-03	1164.6	18. 983	0.91605	10283.	970.00	1184.8
	42.25	7.74010E-93	5.1673	0.15914	20482.	407.6	453.20	1.1351
•	1.4000	5.92362E-03	1194.4	20.561	0-99454	10280.	570,00	1184,4
	1.4000	6.11825F-03 5.92564E-03	9.8821 1185.1	0.1 0.75 22.157	22967. 1.9719	10293.		1,1361
		1000 Family 1000 Co.						
Ŷ	56.25 1.400C	8.9?271E-03 5.92503E-03	10.584 1184.9	0.21701 23.774	236=0+ 1-1475	4607.6 10289.	453.10 570.00	1,1359 1185,1
	64.00	9.52268E-03	11.270	0.24079	25196.	4607-4	453.37	1-1341
•••••	1.4000	5.92:46E-03	11 83.3	25.296	7.5540	16247.	570.00	1103.7
	72.25 1.4000	1.61073E-52 5.91534E-03	11.937	0.27099 26.811	26 735. 1. 3005	4607.6 10230.	453.84 573,00	1.1313 1101.3
	81.00	1.07C11E-02	12,636	2.30374	28 305.	4407-4	453.87	1.1911
•	1.4000	5.91492E-03	1140-8	25.344	1.3769	10228.	\$70.00	1101.2
	90.25	1-127898-02	13.28C	0.33693	29825.	4607.5	454.54	1.1270
	1,4000	5,90521F-03	1177.4	29- 973	1.4534	10175	570.00	1177.0
	100.00	1.184756-02 5.89375E-03	13.691	0.37098	31 304.	4607.6	455.50	1.1211

STREAMLINE &	DENZITA #1	₩2 U	#3 V	FLUM ANGEOD	P-STAT P-STAG	TEMPIRI T-STAG	VELOCITY
1.4000	5,732215-07 5,732206-03	6.774365-04 1162.5	0.0	1.5164	4452.7 5925.9	45%-61 570-00	1.1327 1182.5
C.25 1.4000	5.76147F-04 5.731495-07	C.58349 11*7.2	9.1271°5-04 1.5787	1529.4 7.65113E-02	4462.7 5921.5	453.67 570.00	1.1323 1182.2
1.00	1.15529F-03 5.72934E-03	1.3648	3.64501F-03 3.1551	3055.8 0.15302	9906.5	453.34 570.00	1161.3
2.25 1.4C00	1.73154E-03 5.72576F-03	7.0431 1179.9	8.1E477E-03 4.7269	4579.1 C.22953	4462.7 9986.8	454.12 572.00	1.1295 1179.9
4.00 1.4200	2.30653F-03 5.72073E-03	2.7158	1.45115E-02 6.2915	6099.3		454.52 570.00	1.127 <u>1</u> 1177.9
6.25 1.4000	2.86523F-C3 5.72512E-03	3.4035 1179.6	2.27245E-02 7.8761	7630.0 0.35255	4452.7	454.17 577.00	1.1292
1.4000	3.471765-33 5.740955-33	4.1175 1:46.0	3,79800 E=92 9,5024	0148.6 0.45066	4462.7	452.92 570.00	1.1369
12.25	4.05514E-03 5.76203E-03	4, 5551 11 °4,3	4.53832E-02 11.164	10771. 0.53556	4462.7 10136.	451.26 570.00	1.1470
16.00	4.ac271E-C3	5.6C70 12G2.5	5.98999F-02 12.846	12367.	10237.	449.62 575.00	1.157
20.25 1.4000	5.25431E+32 5.75277E-03	6, 3381 12C6, 3	7.617215-02 14.497	13943. C.68857	4467.7 10298.	445.87 570.00	1.1616
25.CC	5.83476E-C3 5.79345E-03	7. 0445 1206.5	9.40704E-02 16.111	15494. C. 76566	4462.7 16202.	445.81 570.00	1.1614
30.2	6.42184F-C3 5.75280E-03	7.7462 1206.2	0.11378 17.718	1704). 0.84156	4467.7 10298.	442.87 570.00	1.161 1206.
36.0¢	7.00 274E - 33 5.79344E-03	8,4404 1205.3	0.13525 19.314	1858:. 0.91805	4467.7 10283.	449.05 570.00	1.169
42.25	7.56-64E-03 5.78-97E-03	9.1614 1205.1	C.15869 20.920	20127. 3.99454	4467.7 10259.	449.09 570.00	1.16C 3205.
49.00 1.4000	#.17190E-03 5.79195E-03	9. £539 1205. 8	0.18422 22.543	21564.	4462.7 10293.	448.93 570.00	1.161
56.25 1.4000	P. 75464E-03 5. 79135E-03	12.554 1205.6	0.71141 24.148	23230. 1.1475	44e2.7 10289.	44 9. 98 573.00	1.160 1205.
	9. 2276eE - 03 5. 7e7s7E-03	11.238	5.24011 25.728	24759. 1.2240	4462.7 10767.	449.25 570.00	1.159 1204.
72.25 1.4000	4.96564E-03 5,781876-03	11.905 1201.5	6•27025 27•283	26771. 1.3005	10230.	449.71 570.00	1.156 1202,
P1.0C	1.24875E-02 5.78146E-03	12.602	C. 30291	27814. 1. 3769	4467.7 10228.	570.00	1.156
90.25 1.4000	1.13539E-02 5.77295E-03	19-245 1198-3	0.13607 30.403	25 3C4. 1. 4534	4462.7 19175.	450.41 570.00	1-152 1198•
100.00	1.16111E-72 5.76278E-03	13.857	0.37209 31.874	30 762. 1. 5299	10100	451,36 570,05	1.146

OUTPUT NO. =

1203.2

10110.

1.5259

577. 20

17684710N NO. 0 X-STATION NO. 21 Y-INNER = C.0001 Y-007 64 = 2.0182

130.GC

1.4000

...21.....

1.150706-02

5.771581-03

: 3.840

1202.0

	CP/CV	W1 DENSITY	W2	y h3	FLUM ANG(C)	P-STAT P-STAG	T-STAG	MACH NO
1	0-0	5.619055-07	6. 746335-04	0.0	1.4898	4336.8	449,98	1. 1549
	1.4063	5.6:805E-03	1200.8	0.0	0.0	9925.9	570.00	12CC.
2	C. 25	5-691396-04	C.5#208	9-1:3765-74	1500.5	4338.8	45C.03	1.1545
- -).400C	5.01.7356-23	1200.5	1-6035	7-65113F-02	9921.5	577.00	1200.5
	1.400	1.17529E-03 5.61524E-03	1.3620	3.62796E-03	3010.0	433P.8		1.1535
4	2.25	1.701598-03	2. C390	F.16837E-03	4512.7	4337.6	450.48	1.1518
	1.4000	5-61173E-03	1198.3	4.8004	0.22953	4886.8	570.00	1198-3
. 5	4-0C	2.266e7-03	2.7115	1.448346-02	600009	4337.8	457.88	1.1493
	1.4000	5.696808-03	1196.3	6. 3899	0.30664	9856.5	572.00	1196.3
6	£.25	2.83520E-C3	3.3967	2.267725-CZ	7515.7	4338.8	457.53	1.1515
	1,4600	5,61110E-03	1; 04.0	7, 9289	0,38255	9.5850	570.00	1190.C
	9.20	311. 7E-03	4.1084	3. 291 765-02	9050.8	4338.8	449.29	1.1590
	1.4000	5.6266F-0?	1204.2	9.6485	C-45706	9979.2	570.00	1204.3
- 8	12.25	3.95477F-03	4.8432	4.52718E-02	10609.	4278.8	447.65	1.1690
	1,4000	5.64728E-03	1217.4	11-333	0.53556	10106.	570.00	1212.4
. 9	16.0C	4. 9 92 CCE - 03	5. 591 6	5.973665-02	12161.	4338.8	440.02	1.1789
707	1 • 4090	5.00785E-03	1220.4	13.037	C. 61206	10237.	570,00	1220.4
10	20.25	5.16337E-03	6. 3232	7.595615-02		4336.8	445.27	1.1025
	1,4609	5,67740E-03	1224.0	14.711	0,68857	19294.	570,00	1224-1
11	25.0Ç	5, 73770E-G3	7. C246	9.380416-02	15 26 2 ₀ 0 • 7 5 5 0 6	4338.8	445.22	1.1878
	1.4000	5.67808E-03	1224.3	16.349	0.75506	10302.	570.00	1224.4
12	30.25	6. 11C66E-03	7. 7243	C-11346	16725.	4326.6	445.27	1.1 235
	1.4000	5.677436-03	1224.0	17. 9AC	0.44156	10298-	577.00	1224,1
. 13	36.00	6.80154E-03	E-4168	0.134#7	15 301.	4330.8	445.45	1.1824
	1.4000	5.67513F-03	1221.1	19.599	0.91805	10283.	570.06	1223.3
14	42.25	7.49434E-03	5.1159	C.15925	19824.	4117.4	445,49	1.1022
	1.4COQ	5, e 74e6E-03	1227.9	21-229	0.09454	10770.	579-00	
15	49.0C	4. 03C46E-03	9.8262	0.1 8370	21 359.	4339.8	445.33	1.1931
	1.4000	5. 67660E-03	1 ? 23. 6	22.876	1.0710	10293.	570.00	1 22 3. 8
16	56.25	8. 60 412E-03	10.525	0.210=1	22981.	4336.5	. 445.30	T.1826
	1.4000	5.6760LE-03	1223.4	24.504	1.1475	16249.	570.00	1 223.6
17	64.00	9.171116-03	11.207	0.23945	24387. 1. 2240	4334.0	445.65	1.1812
	1.4000	5.6726CE-03	12 22.0	26.109		10257.	57C.00	1222.3
16	72.25 1.4C00	4.73414E-C3 5.66673E-03	11.673 1219.7	0.24953 27.689	25577. 1.3205	4736.6 10230,	444.11 570.00	1.1784 1220.0
•				••••				XELVIV
19	61.0C	1.03760F-02 5.66633F-33	12.560 1219.5	0.30210 29.313	27397.	10228.	579.00	1.1742
20	90.25 1.4000	1.056250-02	13.211 1716.2	0.33520 30.656	2*864. 1.4534	4338.0 10175.	446.8C 570-90	1.1742 1216.6
				0.7790.003	100 11			
21	10C.30	1.14101E-C7_	13.623 1211.5	32.356	3C 30C. 1.5299	473E.B	447.74 570.GO	

	CP/CV	DENSI74	h2 U	43	FLOW ANG(O)	P-STAG	TEMP(R) 7-STAG	VEL O
. 1	1.4003	5.515C5E-07 5.51605E-03	6.71390E-94 1217.2	C-G C-3	1.5658	422849	446.69 570.00	1.1 121
2	0.25 1.4000	5.59205E-04 5.51536E-03	C.68C61 1216.9	9. C5662E-C4 1.6253	1486.2 7.65109E-02	4226.9 9921.6	446.74 570.00	1.1 121
	1.00	1.11764E-03 5.01329E-03	1.35 <u>91</u> 1216.0	3.62941F-03	2969.5 C.15 302	4728.9	446.91 570-00	1:1
4	2.25 1.40C0	1.e7513E-33 5.50964E-03	2.0247 1214.7	6.15127E-03 6.8660	445c.0 0.22953	4228.9 9886.8	447.19 570.00	1.1 121
5	4.00	2.23136E-03	2.7060	1.44543E-02	5926.1 0.30664	4228.9 9856.4	447.59 570.00	
	1.40C0 6.22	5.5050E-03 2.79121E-03	1212.7	2.263205-02	7414.6	4278.9	447.24	1-1
•	1 <u>.40</u> 00	5,5C922E-03 3,35963E-03	1214.4 4. 0991	3-1783	0.38755	4228.9	577-00 446-01	121
	1.4000	5.5245CE-03	122C.5	3,284335-02 9,77%	0.45906	9975.2	57C - 00	122
	12.25	3.53767E-03 5,54475E-03	4. e311 122*.5	4.51594E-02 11.483	10466. 0.53536	422*.9 10108.	444.38 57C.00	1.1
	16.CD 1.4C30	4.51077t-05 5.56495f-03	5.5767 1236.3	5.95754E-02 13.267	12017. 0.512C6	4229.9 10237.	442.76 570.00	1.1 123
10	2G. 25 1.4000	5.08309E-03 5.57432F-03	6, 3025 1239, 9	7.57455E-02 14.901	13548. 0.68857	4228.9 15298.	442.02 \$70.00	1.2
	25.00 1.4000	5.64849F-03 5.57499F-03	7, 0049 1240, 1	9.35411F-02 16.560	15056 0,76506	4228.9 10302.	449.47 570.00	1.2
12	3C. 25	6.21257E-C3 5.574356-03	7. 7027 1239. 9	C.11315	16554. 0.84156	427F.9 10298.	442.97 570,93	1.2 124
.12	36.00	6.77455E-C3	0.3935 1279.0	C.13450 19.854	1895%	4226.9		
14	42.25	7.33945f-03 5.5716X-03	9.0906 1238.8	C.157#1 21.505	19457. 0.94454	4275.9 10280.	442.23 570,00	1.2
15	49.00	7,505616-03 5,273546-03	9. 7987 1234.5	0.16319 23.172	21371 <u>.</u> 1.0710	10293.	4.42, 79 577, 00	123
16	54.75 1.4000	9.46937E-09 5.57296E-03	17.495 1239.2	0.21C23 24.822	225 ⁷ 2. 1,1475	4224.9 10289.	447.13 577.00	1. 12:
	64.00	9.02854F-C3	11.174		24059. 1.2240	4228.9 10267.	442.39 570.00	1.2
18	72.25	5.55384E-03	71.841 1235,6	0.268e0 20.050	25 526. 1. 3005	42284 9 10230,	442.85 570.00	151
.19	81.0C	L.C1456F+Q2 5.26345t-03	12.535 1235.4	0.3012 <u>9</u> 29.696	27027. 1.3769	4728.9 10778.	442.88 570.00	121
20	90-25 1-4000	1.06936E-72 5,55525E-03	13.177 1232.2	0.33432 31.264	28475. 1.4534	4228.9 10175.	443.56 573.00	1.1
.21	106.00	1.12127E-02 5.54354E-03	13.789 1227.6	0.36629	29892a 1.5299	4228.9	444,47 570.00	1.1

1.4000

2	TREAMLINE & CP/CV	UENSITY UENSITY	#2 U	v 3	FLOM ANGIOS	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VELOCITY
		VEN 37 LV	· · · · · · · · · · · · · · · · · · ·		1204			VELOCITY
	0,0	5.42341E-07	6.68138E-04	0.0	1.4440	4129.8	443.67	1.1932
	1.4000	5.42341E-01	1232.0	0-0	0.0	9925.9	570.00	1232.0
	0.25	5.513658-04	0.67910	9.06855E-04	1468.C	4129.8	447.73	1-1920
	1.4500	5,42274E-03	1271.7	1,0447	7.651696-02	9921,5	570,00	1231.7
	1.30	1.1C178E-C3	1,2561 123C. 9	3. 6 21 88E-03	2933.1 0.15302	4129.8	443.90	1-1918
	1.4000	5.42071E-03	123C. 9	3,2873	0.15302	9906.5	577.00	1230.9
	2.25	1.651366-03	2. C2O3	8.13376 E-03	4395.4	4129.8	444.17	1.1901
	1.4000	5-41731E-03	1229,5	4.9255	0.22553	9876.8	570,00	1229,5
	4-00	2,199696-03	2.7503	1.44236E-92	5E53.4	4120.8	444.56	1.1878
	1.400C	5.41255E-03	1227.4	6, 5571	0.30404	9856.5	570.00	1227.6
	6.25	2.751596-02	3.3824	2.25835E-02	7323.6	4129.8	464.72	1.1798
	1-4000	5.41671E-03	1229-2	6.2074	C.38255	9882.9	570.C0	1229-3
	9.00	3.31096E-03	4. C897	3. 27 6795-02	8819.4	4125.8	447.99	1.1973
	1.4000	3,43172E-03	1235.2	9. 2568	C-45906	6979.2	579.00	123523
	12.25	3.87685E-03	4,6151	4. 90469E-C2	10338.	4129.8	441.38	1,2071
	1.4000	5,45),446-03	1243.0	1119	0.53554	10108.	570,00	1543-1
	16.CC	4.44674[-03	5.5617 1250.7	5.941576-02	11869.	4129.8	499,77	1.2168
	1.4000	5.471496-03	1250.7	13.362	0.61206	10237.	57C.00	1250.8
	20.25	5.01095E-03	6,2751	7.55361E-02	13342.	4129.8	430.04	1.2213
	1,4000	5,46C71E-03	1254.3	15,074	0.68857	10298.	570,00	1254,4
	25.00	5,56633E-03	6. 9455	9. 32 21 96-02	14871.	4129.8	439.98	1294.6
	1.4000	5.48137E-03	1254.5	16.752	0.76506	10302.	570-C0	1254.6
	3C.25	6.12439F-03	7.6814	0.11763	16355.	4129.8	439.03	1.2213
•	1.4000	5. 460 74E - Q3	1254,2	10.424	0.84156	10290.	470,00	1254,4
	36.00	6,67843E-03	8, 3704	0.13413	17833.	4129.8	439.21	1.7202
	1.4000	5.474516-03	1253.4	20.084	0.91605	10593.	570,00	1253.5
_	42.25	7.2343CE-03	9.0657	0.15738	19317.	4129.8	479.25	1.2200
-	1.4000	5,478078-03	17:3-2	21 • 755	0.50454	10540*	570,00	1253-1
	49.00	7.793416-03	9.7717	0-1 626 8	2011.	4124.8	429.10	1.2209
•	1.4000	5.47994E-03	12:3.8	23.441	1.0710	10293.	57C.00	1254.1
	56.25	8.34916E-03	10.446	0.20465	22205.	4179.8	439.14	1.2200
	1,4000	5.47937E-03	1253.6	25.110	1.1475	10289.	57C.00	1253.0
	64.00	0.50C39E-03	11.146	0.23814	23763.	4129.8	430.41	1.2190
	1.4000	5.47607E-03	1252.3	26.756	1. 2240	10267.	572.00	1252.
•	72.25	9.44684E-03	11.409	0.26908	252144	4129.8	439.96	1.7163
	1.4000	5,47041E-03	1250-1	20,379	1.3005	10230.	570,00	1750.4
	81.00	1.0001 0E-02	12,561	0.10048	26695.	4129.8	439.89	1 - 21 61
	1.4000	5.47CC2E-03	1249.9	30,043	1.3769	10228.	570.00	1250.
	90. 25	1.05-19E-C2	13,143	0.33346	20125.	4129.8	440.54	1.712
	1,4000	5.46196E-Q3_	1246.7	31 - 632	1, 4534	10175	570.CO	1,24.7-1
		1.107336-02	13.755	0.36736	29525.	4129.8	441.47	1.2065

STREAMLINE &	OENSITY	n n	v 3	FLOW ANGIDS	P-STAT P-STAG	TEMP(P) T-STAG	MACH NO VFLOCITY
	5.337681-07	6-64880E-04	0.0	1.4238 0.0	4038.9	440.86	1.2102
1.4000	5.33788E-03	1245.6	0. 5	0.0	9925.9	570.00	1245.6
C.25	5.440975-04	0.47750	9. C481 8E -04	1451.3	4038.9	440.52	1.2099
<u>_</u>	5•33722 <u>E-</u> 03	3 745.3	1-0630	7.65110F-02	9921.5	57C.CO	1245.3
1.00	1. (67266-03	1.3511	3-61341E-03	2099.7	4638.9	441.18	1.2089
1.4000	5.335716-03	1244.5	3, 37 38	0.15302	9908.5	570.00	1244.5
2.25	1.02 9006-03	7. C259	8.1159CE-03	4345.3	4038.9	441.36	1.2072
1.4000	5.33187E-33	1743.2	4.9903	0-22953	9856.8	570.00	1243.2
4-00	2,170716-03	2.6945	1.43925E-02	5786.8	4038.9	441.75	1.2048
1.4000	5.327196-03	1 241.3	6.6303	G.30604	9E56.4	579.00	1241.3
6.25	2.715346-03	3.3750	2.253436-02		4038.9	441.41	1.2069
1-4000	5,33127E-Q3	1242.9	5.2988	C.38255	9382.9	577.00	1242.9
9.00	3.26734E-03	4. C90Z	3.26917E-02	8719.5	4038.9	440.14	1.2143
1.4000	5.34e06E-03	1246.8	10.006	C.45906	9970.2	570.00	1248.8
12.25	3-625796-03	4.6071	4.49343E-GZ	10556*	4238.9	438.58	1.2240
1.4000	5, 365666-03	1256.5	11.745	0.53556	fcics.	570,00	1256.5
16.00	4.78816F-03	5.5469	5.92.71 E-02	11734.	4038.9	436, 99	1.2337
1-4000	5.365276-03	1264.1	13.504	0.61207	10237.	570.00	1264.1
20.25	4.544936-03	6-2678	7.53297E-02		4038.9	436,25	1.2361
1,4900	5.39+276-03	1267,5	15.234	0.68857	10298.	570.00	1267.6
25.00	5.45456E-03	6. 96 63	9. 30252E-02	14701. 0.76506	4630.9	436,20	1.2764
1.4000	5.39.92E-03	1267.8	16.929	0.76506	13302.	570-00	1267.9
30.25	6. C437[E-C3	7. e6C3	0-11252	16169.	4070.9	436.25	1.7301
1,4000	5-35430F-03	1267.3	18,618	C,84156	10298.	5 70. 30	1267.6
36.00	6.55041E-03	F. 3476	C,13377	17629.	4038-9	430,43	1.2370
1.4009	5.39211E-03	1264.6	20.297	0.91805	10283.	570.00	1246.8
42.25	7-13899E-03	5.C410	C.1:695	19396.	4038.9	436.46	1.2368
1.400·G	5, 39167E-09	1266.4	21 - 945	0.59454	10260.	570,00	1 266.4
49.0C	7.69C73E-C3	9.7450	0.18218	20 57 4.	4038.9	434,91	1.2377
1.4000	5.39351E-03	1267.1	22,689	1.0710	10293.	570.00	1267.3
56.25	8.2391et-03	10-438	C.20904	22041.	4/38.9	436.36	1.2375
1.4000	5.392956-03,	1266.9	25.376	1.1475	16584	570-00	1267-1
64.00	0. 7031 3E -03.	11.116	0.23750	23492.	4938.9	436.67	1.2359
1,4000	5.38971E-03	1265.6	27.040	1.2240	10267.	570.60	1245. 6
72.25	a-35, arr-03	11.776	0.26737	24927. 1.3005	4038.9	437.07 570.00	1.2331 1263.7
1,400C	5.384136-03	1243-4	28,681		· · · · · · · · · · · · · · · · · · ·		
81.00	- 9. 870C4E-03	12.466	C. 29969	26391.	10228-	437-10 570-50	1.2330
1.4700	5.38375E-03	1263.2					
90.25	1.040306-02	13.109	C.33260	27804.	4038.9	437.75	1.2290
1,4000	5,37582E-03	1260,1	31.971	1.4534	19175	570.00	1 546.5
100.00	1.69774E-02	13.721	0.36645	29186.	4038.9	419.67	1.2235
1.4000	5.364496-03	1255-6	33.535	1.5299	10105.	570.00	127601

5	TREAMLINE &	41	PS.	W 3	u4	P-STAT	TEMPIR)	MACH NO
	CP/CY	DENSITY	<u>V</u>	Y	FLOW ANGION	P-STAG	T-STAG	VELOCITY
	0. 0	5.25010E-07	6.61622F-04	0.0	1. 4049	3954.7	437.21	1.2262
	1.4000	3.236106-03	1238.3	0.0	0.0	9925.	372.00	1250.3
	0.25	5. 373776-04	0-67604	9. C275 8E-04	1435.8	1954.7	438.27	1.2259
••••	1,4000	5,257456-03	1238-0	1,6799	7.65110E-02	9921.6	570.00	1256.0
	1.00	1.07=836-03	1.3501	3.403646-03	2868.4	3954.7	434.43	1.2249
	1.4000	5.255480-93	1257.2	3.3574	C-15302	9926-5	570.00	1257.2
	2,25	1.63947E-C3	2.C714	6.09779F-03	4299.0	1954.7	43 9. 71	1.2233
	1-4000	5.252196-03	1255.9	5.031?	0. 22953	9886.8	570.00	1233.9
	4.00	2.14390F-G3	2.6886	1.43610E-CZ	3725.1	1954.7	439,09	1.2209
	1.4000	5.24757E-03	1254.1	6.6986	C.30604	9956.4	570.00	1254.1
	6.23	2. 661 80E-C3	3, 3674	2.24834E-02	7163.0	3954.7	439.76	1.223C
	1,4000	5,251605-03	1233.7	9, 3829	C.38755	9892.9	570.00	1255.7
	9.00	3.226976-03	4- C707	3-261498-02	8525.9	3954.7	437.54	1-2303
	1.4000	3, 266166-03	1261.4	10.107	C-4390b	9979.2	570.00	1261.5
	12.23	3-778326-03	4-7950	4-48217E-02	10111.	3954.7	435.95	1.2400
	1.4000	5.28547E-03	1269.0	11.862	0.33456	10108.	370.00	1269.1
	10.00	4.37795E-03	5-5321	3.90996E-02	11609.	3954.7	434.36	1.2495
•••••	1.4000	4, 33395E-03 5, 30472E-03	5.5321 1276.5	13.636	0.61296	10237.	570.00	1276.5
	20.25	4. 26354E-03	6.2507	7-512336-02	13046.	3954.7	437.63	1.2539
	1.4000	5-31363E-03	1279.9	15.382	0.68837	10298.	570-00	12 30 - 0
	25.00	4.427086-03	6.5472	9.277116-02	14544	3954.7	433.58	1.2549
	1.4000	5-314298-03	158C-1	17.094	0.76506	10305	370.00	1280-2
	30.25	5. 969056-03	7.6394	0.11222	15996.	3954.7	433.63	1.2540
	1.4000	5.31368E-03	1279.6	18,800	0.84156	10298.	570,00	1280.0
	36-00	6.5C9CCE-93	P. 3230	0-13340	17441.	1934.7	477.81	1.2529
-	1.4000	5.31132F-03	1279.0	20.493	C.91803	10283.	570.70	1279.2
	42.23	7.05C8CE-C3	5. C1 65	0.15653	18692.	3954.7	437.84	1.7527
	1.4009	5.31109E-03	1278.8	22.200	0.99434	10280.	570.00	1279.0
	49.0C	7.59577E-03	9. 7184	0.18169	20 354.	3954.7	477-69	1.2534
	1.4000	3.3129GE-03	1279.5	23.920	1.0710	10293.	570.00	1279.1
	36.25	4.13739E-03	17.409	0.70851	21903.	3954,7	421.74	1,2533
	1.4000	5-312336-03	1279.2	25.623	1.1475	10244	570,00	1279,5
	64.00	8.674696-03	11.006	0.23686	23241.	3954.7	494.00	1.2517
	1.4900	5.30916E-03	1276.0	27.305	1.2240	10257.	57G-00	1278.2
	72.25	9.2C721E-03	11.747	0-16665	24660.	3934.7	434.43	1.749
- 	1,4000	3,30366€ <u>-</u> Ç3	,1273.6	78,962	1.3903	10230,	570,00	1276,1
	81.00	9.74810F-03	12.435	0.29889	26109.	3954.7	434.48	1.240
	1.4000	5.30329E-03	1273-6	37.662	1.3769	1027#-	570.00	1276.
	90.25	1.C2745E-02	13.973	0.33174	27507.	3934.7	41:-12	1.244
•••••	3-4000	3-293498-03	1272-6	32,287	1x4534	10175,	570.00	1273.
- -	100.00	1.079246-02	13.687	C. 36551	26677.	3934.7	436.04	1.239
	1.4000	5.28431E-03	1265.2	33.870	1.5299	10100-	570400	1268-

-	TREAMLINE &				44	P-STAT	TEMPIPS	MACH NO
	CP/CV_	DENSITY	V	Y	FLOW ANGIDS	P-STAG	T-SYAG	VFLOC17Y
	0.0	5.18313E-07	6.56371E-04	0.0	1. 3871	3875.9	435.70	1.2414
	1.4000	5.18313E-03	1276.2	0.0	0.0	9925.9	570.00	1270.2
	0.25	5-31103E-04	C. 67448	9.006806-04	1+21.3	3875.9	435.76	1.2411
	1.4000	5,18249E-03	1270-0	1,6959	7,651105-92	9921,6	570.00	1 2 7 0 , 0
	1.400	1.C6129F-03	1.3470	3.59740E-03	2139.9 0.15302	3875.9	435. 92 570. 00	1 . 2401
	1.4000	5.18054E-03	1269.2	3.3896		9908-5	370.00	1264.2
	2.25	1.59063[-03	2.0168	8.0795CE-03 5.0793	4255.7	3975.9	435.19 570.00	1.2365
	1.4000	5,17730E-03	1267.9		0.22953			1267.9
·	4.00	2,11897E-03 9,17275E-03	2. 6F25 1266-1	1.43291E-02	5(67.4 0.30694	3879.9	416.58 573.00	1.2361
				- Markonson	Company Comment			1970
	6.25	2.69C49E-03	3.3598	€. 24332 E-02	7090.8	3875.9	435.24	1.2302
	1,4003	9-176726-03	1267.6	8.4638	0.35255	7002.7	570.00	1247.7
	9.06	3-19031E-03	4.0610	3,25378E-02	2538.9	3975.9	435.04	1.2455
	1.4000	5.19107E-03	1273.3	10-202	0.45906	9979.2	570.00	1273.4
	12.25	3-73441E-03	4. 763C	4.47092F-02	10739.	3675.9	437.45	1.2551
	1. 509.9	5,21010E-03	12424	11-972	C.53556	10108.	570. 20	1580-8
	16,00	4, 2833ef -C3 5, 22908E-03	5.5175 1288.1	5.87431E-02	11491.	3875.9	431,88	1.2646
	1.4000	5. 729C8E-93	1288-1	13.761	0.61206	10237.	570-00	1286.2
	20.25	4.82684E-03	6.2338	7.49195E-02	12955.	3875.9	431.15	1.2690
	1,4000	5.23769E-03	1291.5	19,921	0.69857	10256.	570.00	1291.6
	25.00	5,363746-03	4 - 52 84	9,251916-02	14 397,	3675.9	431,10	1,2693
	1.4000	5. 23852E-03	1291.7	17,249	0.76506	10302.	570- 00	1291.8
	30.2:	5.899385-03	7.6187	0.11101	15634.	3975.9	421.15	1.2690
	1,4000	5+23791E-03	1291.4	18.970	0.44156	10298.	570.00	1.291,8
	34.00	6.43303E-03	8, 3025	0.13304	17265.	2975.9	431.32	1.2679
	1.4000	5.23579E-03	1290.6	20.681	0.91805	10203.	370. CO	1290.8
	42.25	4.90850E-03	0.9923	0.15610	16701.	7975.9	431.36	1.2677
	1,4000	5.23536F-03	1290-4	27.401	0.99454	102504	572,00	1290, 4.
	49.00	7,527C7E-03	9.6521	0-16120	20146.	3875.9	431,21	1.2666
	1.40CC	5.23715E-03	1291.1	24.137	1.0710	10293.	570.00	1291.3
	56. 25	6.C4241E-03	10.361	0.20794	21505.	3875.9	431.75	1.2683
	1.4000	5. 2 3660F-03	1290.8	25. 856	1,1475	10289.	570.CO	1291,1
,	64.00	4.57338F-03	11.056	0.23622	23006.	3875.9	431.51	1.2667
	1.4900	5.23346E-03	1289.6	27.553	7.5540	19767.	570.00	12 99.9
)	72.25	9.099756-03	11.716	0.76596	24411.	1875.9	431.96	1.2640
- -	la4Q0Q	5,220C4E-03		214227	1.3075	10230.	<u>\$</u> 7,0,00	1287, 8
	\$1.00	9.634336-03	12.402	0.29810	25845.	3075.9	431,99	1.2639
	1.4000	5.22767E-C3	1287,3	30.942	1. 3769	10220.	570.00	1207.7
0	90.25	1.015466-32	13.041	0.33356	27229.	3675.9	432.63	1.7600
115	1,4000	5.21997E-03	1204,3	32 - 584	1.4534	10175,	570.00	1284,7

STREAMLINE &	WI	h2	N3	W4	P-STAY	TEMP(R)	MACH NO
CP/ <u>C</u> Y	DENSITY	<u>V</u>		FLOW ANGION	P-STAG	Y-S7AG	VELOCITY
c.o	5,14770E-C7	6-56747E-C4	n.0	1.3766 0.0	383F.4	434,49	1,2487
1.4000	5.147276-03	1279.9	0.0	0.0	9025.9	57C+00	1275.9
C. 25	5-281116-04	G-6737C	8.99625E-04	1414.4	3839.4	434-55	1.2484
1.4000	5.14676E-03	1275.7	1.7035	7,65109E-02	9921-5	570,00	1274,7
1.00	1.055316-03	1, 3454	3.59326E-03	2826.0	3636.4	434.71	1,2474
1-4000	5.14463E-03	1274.9	3_4049	0.15302	9908.5	570.00	1274.9
2. 25	1-5 (1726-03	2. C145	8.07027E-03	4235.0	3636.4	434.98	1.2456
1.4000	5,14141E-C3	1273.9		0.22953	\$896.0	570-00	1273.4
4,00	2-10694E-03	2.6796	1.47170E-02	5639.9	3838.4	435.34	1-2435
1.4000	2-1308aE-G3	1271.6	6,7933	0.39604	9856.5	579.00	1271.6
6,25	2.03556E-C3	3.3%6C	2.74C77E-02	7056.4	383*.4	435.33	1.2455
1,4000	5,14083E-C?	1273.4	e. 5020	C. 36.255	9882.9	57C- 90	1273.4
9-00	3-171346-03	4,0562	3,24991E-C2	8497.4	3838.4	433.43	1.2528
1.4000	5.155C7E-03	1279-0	1C-246	0. 45 976	9979.2	570- 30	1270.1
12.25	3.71337E-03	4.7770	4.46530E-02	9959.9	3639,4	432.24	1.2623
3,4000	5,17398E-03.	1286.4	12,C25	C.5.3554	10108.	577-00	1286.5
16.00	4,259246-03	5.5102	5. 48651 E-02	11435,	3838.4	430.68	1.2714
1.4000	5.1 9283E-C3	1293.7	13.021	0.61206	1C237.	570.00	1293.0
20.25	4.75965E-03	t. 2253	7.4#182E-02	12692.	3838.4	429.95	1.2762
1,4000	5.20157E-03	12.97.C	15.568	0.68857	10798	570.00	1297.1
25,00	5,33353E-03	6.9190	9.23924E-02	19327.	3937.4	479. 90	1.2765
2.4000	5-202206-03	1297.3	17.329	0.76506	10362.	570-00	1 297.4
30.25	5.0015E-03	7.6084	C-11176	15737.	3838.4	479.95	1.276
1,4000	5-201606-03	1297,0	19,052	C-04154	10296	570,00	1297,1
36.00	6-15679E-C3	8. 2913	0.13266	17180.	3837.4	437-17	1.275
1.4000	5.19949E-03	1296.2	20.770	0.91805	10203.	570.00	1296.
42.25	6.929266-03	9, 9802	0.15569	18610.	3838.4	430,14	1.274
1,4000	5,19907E-03	1296.0	22.498	0.99454	10260	577-00	1296,
49.00	7,464 795-63	5.6791	0.16095	20050-	3838.4	430.C1	1.275
1.4000	5.20084E-03	1296.6	24.241	1.0710	10203.	57C.00	1294.
56.25	7.99711F-03	17.367	0-20746	21483.	3834.4	430.06	1.275
1,4000	5 . 20030E - 03	1296.4	22.967	1.1475	10289.	570-00	1296.
64.00	8.525096-03	11.641	C-23591	22894.	3828.4	430.32	1.274
1.4060	5.19717E-03	1295.2	27.672	1.2240	10267.	570.00	1295.
72.25	9.04826-63	11.750	0.26561	24293.	3538-4	433.76	1.271
1.4000	5,19169E-03	1293.0	29,354	1,3005	10530*	577,00	1293.
	9,500C6E-03	12.384	0.29771	25719.	3530.4	437.79	1.271
1.4000	5.141436-03	1292.9	31.076	1.3749	10228.	577.00	1 293.
90.25	1.00974E-02	13.C24	0.12045	27097.	3838.4	431.43	1.247
1. 600C	5.16379E-03	1584.9	32,727	1.4574	10175.	570-00	1290
100.00_	1,06C64E-02	13.435	0.36416	28 446.	3538.4	432.34	1. 241
1.4700	5-17285E-03	1285.6	34.334	1.5299	10100.	579.00	1286.

		F1555, A	X-STATION NO 3		0.0501 V-0U1		DUTPUT NO.	
	TREAMLINE &	DENSTA NJ	P.S	, N3	FLOW ANGIOS	P-STAG	TEMP(A) T-STAG	AETUCITA AVCH MO
	1-4000	5.11224E-07 5.11224E-03	6.55127E-04 1201.5	0.0	1. 3762 0.0	3861.9 9925.9	432, 31 570.00	1.2559
	0-25 1-4000	5.25205E-34 5.11163E-03	C-67292	8.78591E-C4 1,7109	1-07-7 7-65110E-02	3801.9 9921.5	433-36 570,90	1.2556
	1.4000	1,04951E-03 5,10968E-03	1.3459	3.58912E-05 3.4198	2612.7 0.15302	3801.9 9908.5	433.53 370.00	1.2546
	2-25 1-4000	1.573C3E-03 5.1C649E-05	2. C122 1279. Z	8.061C7E-03 5-1245	4214.9 0.22353	5801.9	45% 80 570.00	1.7529
	4-90	2.95536E-03 5.10200F-05	2.6766 1277.4	1.42969E-02	5615-1 0-50e04	3801.9 9856.4	434.18 579.00	1.2500
	1.4000	2.621C8F-05 5.10591E-05	5.7522 1279.9	2.23871F-02 8.5393	70 22.9 0.38255	3801.9 9852.9	423.55 570.00	1.2526
		3.15392F-05 5.12007E-05	4. C51 4 1284. 5	3.24604E-02 10.292	8457.1 0.45906	3861.9 9979.2	452-45 570-00	1.2549
	17-25 1-4000	3.69297E-03 2.13884E-03	4.7710 1291.9	4.45969E-CZ	200000	3801.9 10108.	421.07 570,00	1.2694 1292.0
	16.00	4.2°584E-05	5.5029 1299.1	5.67676E-02	11381.	3601.9 10237.	429.50 570.00	1.2799
	2C-25	4.77328E-05 5.16625E-03	6-2170 1302-5	7,47175E-02 15,653	(A) (C) (C)	3801.9 10298.	425.78 570.00	1.2853
	25.00 1.4000	5.3C422E~03	6, 9096 1502, 7	9,22692E-02	14259. 0.76506	3801.9 10502.	428.73 570.00	1.2836
	30.22	5.03392E-03 5.10627E-03	7.5982 1502.4	0-11161	15602. 0.84156	3831.9 19298	424. V8 570.00	1.2033
	36.60	6,36165E-03	8,2802 1301.4	C.15257	17099.	5801.9 10263.	478.95 575.60	1.2022
	42.25 1,4000	6.89118F-03 5.16576E-03	8.9682 1391 ₉ 4	0.1 5569	18522.	3071-9	428.99 570,09	1.2826
	49.00	7.47377E-03 5.14552E-03	\$.666C	0,18071 24,342	19955	5801. 9	42F.R4 577.00	3.2029 1502-3
	50.25	7.553178-03	10-353 1301-8	0.20736 26.076	21 977.	3801.9 10259.	427.09	1.2826
	1.4000 64.60	5.16458E+03 8.47825E-03 5.16187E-05		0.23559	22785. 1. 2240	5801.+ 10267.	570-30 429-14 570-00	1 502 - 1
	72.25	e. 59879E-05	11.005	0.26526	24177.	3401-9	429.59 570.00	1 300.9 1.2784 1298,8
	81.00	5, 15659 <u>t - 27</u> 7, 5 2 7 4 3 F - 03	1298,5		1.5705 25597. 1.5769	19250+ 5801.9 10228.	429.62 570.00	1.27#2 129#,7
_	1.4000	5-15617E-C5	17.007	0.33003	26968.	7001.9	437-25	1.2744
	1,4900	1.05481E-02	13.618	37, 965 0.56371	1•4 <u>554</u> 20 311•	10175,	579-00 431-16	1295,7 1,2689

	I ERA7	Transcript of the second	K-STATION NO 3		4.4		Vivola	
	STREAMLINE & CP/CV	DENSITY	W2	. <u> </u>	FLOW ANGLOS	P-STAT P-STAG	TEMPIRI T-ST4G	MACH N
١	C.0 1.4000	5.04486E-07 5.04486E-03	6.51893F-04 1292.2	0.0	1. 3542 0.0	373 Z. 0 9925. 9	431.02 570.00	1.2698 1292.2
2	0.25 1.4000	5.15640E-04 5.04424E-03	C. 67134 1291.9	8.76492E-04 1,7252	1794.8 7.65110E-02	3732.0 9921.5	431.07 570.00	1.2494
	1.00	1.03839F-03 5.04234E-03	1.3407 1291.2	3.58078E-03 3.4484	2756.9 0.15302	3732.0 990a.5	431 . 23 570. 00	1.2654 1291.2
	2.25 1.4000	1. 5 c 2 5 f - 03 5 . 03 9 1 9 E - 03	2. CC76 1289. 9	8.04255E-03 5.1676	4176.4 0.22953	3732.G 9886.9	431.50 570.00	1.2668
٠	4.00	2.07315F-03 5.03476E-03	2.67C5 1286.1	1.4264*E-0Z	5561.8 C.30604	3732.0 9856.4	431.88 570.90	1.2645
b	6.25 1.4000	2.59329E-03 5.07802E-03	2.3445 1289.7	2.233CAE-02 8.6110	6958.7 0.39255	3732.0 4862.9	431.55 573.00	1.2665 1289.7
7	9.00 1.4000	3.12049F-03 5.05260t-03	4. C417 1295.2	3,23825E-02 13,378	8379 <u>.7</u> 0.45906	3732.0 9979.2	439.3e 579.30	1 . 2737 1 2 • 5 • 3
0	12.25 1.4000	3.65382F-03 5,07112E-03	4.7590 1302.5	4.44849E-02 12.175	9621.8 0.53556	1732.0 10108.	426.79 570.00	1.2832 1302.5
۹	16.00	4,15097E-03 5.08959E-03	5,4485 1369,6	5.86329E-02	11277. 0.61206	3732.0 10237.	477, 23 570, 00	1 . 2 924 1 309. 7
0	20 • 25 1 • 4000	4.72268E-03 5.09816E-03	6.2003 1312.9	7.45170E-02 15.779	12713. 0,68857	3752.0 10298.	426.51 570.09	1.2970 1313.0
1	25.00 1.4000	5.24798E-03 5.09678E-03	4-4911 1313-1	9.20211E-02 17.535	14128 <u>.</u> 0.76506	3732.0 10302.	426.48 579.00	1.2975
2	30.25 1.4000	5.772C6E-03 5.05819E-03	7.5776 1312.8	0.11131	15538. C.841fe	3732.0 1029e.	426.51 570.00	1.2970
3	36.00 1.4000	6 • 29 • 20E - 93 5 • 09 61 2E - 93	E.2581 1312.0	0.13233 21.074		3737.0 10283.	426,58 577,00	1,295
4	42.25).4000	6.81812F-03 5.09970E-03	6.9442 1311.8	0.15527 22.773	18352. 0,99454	3732.0 10280.	426.72 570,00	1.2951 1312.0
5	1.4000	7,345C6E-33 5.09744E-93	9.6401 1312.5	0.18022 24.537	19772.	3732 <u>.0</u> 102 03.	425.57 570.00	1.2966 1312.1
6	56.25 1.4000	7.4c285E-33 5.09691E-03	10.326 1312.2	0.2C683 26.2A5	21161. 1-1475	3732.0 10289.	426.62 570.00	1.796 1312.
1 <u>7</u>	1.4000	6.38837E-03 5.09385E-73	10.997	0.23497 29.011	22576. 1.2240	3732.0 10267.	426.87 570.00	1.2946
	72.25 1.4000	8.90338E-03 5.088 <u>59E-0</u> 3	11.654 13.69.0	0.26456	23956. 1.3005	3732.0 10230,	427.31 570,90	1.292 1309,
١٩	1.4000	9,42641E-03 5.G8821E-73	12.337 1308.4	C.29654 31.458	25 362e 1 • 3 769	3732.0 1022 6.	427.34 570.00	1 309.
20	90.25 1,4000	9.93542E-03 5.08072E-03	12.974 1305.8	0.32918 33,132	26721. 1.4534	3737.0 10175.	427.98 570.00	1.288 1306.
ž1	1c0.00 1.4c00	1.04363E-02 5.07001E-03	130584	C. 36280	28052. 1.5259	3737.0 10100.	428.68 570.00	1.282

	CA TELE	DENSTLA mj	₩2 U	W3 V	H4 FLOW ANGID)	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VFLOCITY
				•••	•			
·····i.		5.01225E-07 5.01225E-03	6-90277E-C4		1. 3464	3698 <u>.2</u> 9925.9	429,90 570,00	1,2765
• 1	0_25 4000	5.16954E-94 5.0]163f-93	C. 67(55 1297.1	8. 95436E-04	1388.6 7.05110E-07	3698.2 9921.5	429. 95 570. 20	1.2762
A	744%							
	1.CO	1.033C2E-C? 5.0C974E-03	1.3397	3.57659E-03	2774.5 0.15302	3698-2	430-12 572-00	1.2752
1.	~000	3.067746-03		3027	cor . en.	777067	377600	127004
	2.25	1.546'1E-C3	2.0052	0. 23320E-23	4157.7	3699.2	432.38	1.2736
J	4000	5.006614-03	1295.1	.5-1874	0 - 2 2953	9874.8	570.00	1295-1
	_ 4+ CÇ	2.062435-03	2. c 675	1.42481 E-C2	5537.0 C.33604	3456.2	432.76	1.2713
1,	4CC 0	5.002216-03	1293.4	6.9084	C. 33604	9856.4	5 70. 00	1293.4
	e-25	2. : 7489E-C3	3-340-	2. 2 304 98 -02	6927.7	3698.2	437.43	1.2733
1	4000	5,000056-03	1294.9	8.6457	0.78255	9882.9	577-09	1294,9
	9.90	3,104368-09	4. C368	3.22439E-92	F342.4	3670.2	429.24	1.2805
1.	4000	5.019936-03	1300.4	10.419	C. 45906	9979.2	572.00	1300.4
	12.25	3-674546-03	4.753C	4.442888-02	9778.0	3494.2	427.67	1.2099
J	-c00	5,03833E-03	1307.6	12,223	C. 53556	10104.	570.30	1307.6
	16.00	4.165276-03	5-4412	5.855*68-02	11226.	3644.2	426.12	1.2993
	4000	5.056686-03	5.4812 1314.7	14.045	0.61207	10737.	570.00	1314.7
	20.25	4.03827E-03	6-1919	7.44169E-02	12657.	3697.2	425.41	1,3030
1	4000	5.3652CE-03	1317.9	15,839	0.68857	10548	570.00	1318.0
	25.00	5.220876-03	6- 881 8	9.18973E-02	14045.	3699.2	425,35	1, 3039
······i	4000	5.065818-03	1316.1	17.6CZ	0.76506	10302	570.00	1318.2
	10.25 4000	5.74224E-03 5.C6523E-03	7.5676 1317.9	0-11116 19-358	15469.	3698.2 10298.	425.40 577.00	1.3037
····· · .	36.00	4.26168E-03 5.06317E-03	8. 2471 1317-1	0.13215 21.175	15966	. 3698.2 19283e	42ª.58 570.00	1.3024
	721.00				okas s		Was a second	110.00
	42.25	6. 782 891-03	8.9323	0.15506	14270.	3498.2	425.61 577.00	1.3024
1	4000	5.062766-07	331669	27.841	0.99454	J. 540'•		1317,1
	49.00	7.367116-03	9.6272	0.17998	19684.	3698.2	475.47	1. 3033
1	.4000	5.76449E-03	1317.5	24.631	1.3710	10293.	577.00	1317.7
	56.25	7.828198-03	10.312	0.20655	21987.	3698.2	475.51	1.3030
1	-40C0	5.063968-03	1317.3	24.356	1.1475	TOSWA*	570.00	1 317.5
	64.00	8.345C2E-03	10.983	0.23465	22475.	3694.2	425.77	1.3015
· ··· · ·	4000	5.060911-03	1316.1	28.119	1.2240	19267.	577.00	1316.4
	72.25	4. d57 * 72 - G3	11.039	C. 20421	23849.	3699.2	426.21	1.2988
	-4000	5,255688-03	1314,0	29,830	1, 3005	17230,	570.CO	1,314,4
	81.00	9.37771E-03	12.321	0.29615	25249.	3498.2	476.24	1.2986
	.4CC0	5.055326-0	1313.	31.580	1.3769	10228.	577.00	1314.7
	90.25	9.954C9E-03	12-957	0.32475	256024	3098.2	426.87	
	40C0	5.047885-03	1310.9	33.261	1.4534	10175.	577.00	1.2948
				2-4-20		APPRIL D		0.00
	100.00	1.038236-02	13.567	0. 36234	27927 . 1.5299	3698.2 10103e	477. 77 570. 00	1307-2

STA	EAMLINE & CP/CY	#1 0EN517Y	h2 V	¥3	FLOW ANGLOS	P-STAT P-STAG	TEMP(#)	MACH NO VELUCITY
		4.56047E-07	6.4P667E-04	0.0		3665.4	475.81	
A	1.4000	4.98047E-03	1 302.4	0.0	1. 3366 0.0	9925.9	570.00	1 302.4
2	9.25	5.14343E-04	0.66576	8.94383E-?4	1302.5	3645.4	474.86	1.2828
•••••	<u>l. 40</u> 00	4.97985E-93	130242	1.7389	7,6511CE-02	9921.5	570,00	1302,2
3	1.400	1.02790F-C3 4.97798E-02	1.3376 1301.4	3.57241E-03 3.4758	2762.4 0.15302	3665.4 9908.5	429.02 57C.DO	1.2818
•	2.25 1.400C	1.545491-03 4.97486F-C3	2. CC29 13CC-2	8.023°(E-C3 5.2387	41 30.6 0.2 2 95 \$	3665.4 9896.8	420.29 570.00	1.2802 1300.2
a	4_CC	2-052C2E-03	7. 6644	1.42315E-02	5517.9	3665.4	429.67	1.2779
?	1.4000	4.97349E-03	1298.4	6. 9355	0.30604	9856.4	570.CO	1298.4
<u> </u>	6.25	2.56687E-03	30.3348	2-227916-02	6897-5	3665.4	479.34	1.2799
-	1.4000	4,97430[-03	1259.9	8. 6795	0.30255	9882.9	577.00	1390.0
7	9.00	3.C8868E-C3	4. C320	3.23050E-02	8306.0	3665.4	426.15	1.2071
	1.4000	4.98210E-03	1305-4	10.459	C-45906	9979.2	577.0C	1305.4
8	12.25	3.61659E-C3	4.747G	4.417298-02	9735.4	3665.4	426.59	1.2965
	1.4000	5,00638E-Q)	1312-6	17.4769	0.53556	10100,	5 7 % 00	1312.4
•	16.00	4-148225-03	5,4740	5.84788E-02	11177. C.61207	3605.4	425-04	1,3059
	1.4000	5.02462E-03	13:9.6	14.097	C. 6 1 207	19237.	570.00	1319.1
0	20.23	4.674556-03	6.1037	7.431736-02	12401.	166 5.4	424.32	1.310
	3-4000	5,03308E-03	1322.9	15,898	Q,68857	10298.	570-00	1322.5
A	25.00	5,19451E-C3	6, 7726	9-177436-02	14904	3665.4	424.27 570.00	1 - 310
	1.4000	5.03369E-03	1323.0	17.668		10302.		1323.7
Z	3C-25	5.71325E-03 5.03311E-03	7, 5575 1322, 0	0.11101 19.431	1:402. G.84150	3665.4 10298.	424,32 570,00	1.210
				0.701 2.02410				
13	1.4000	6. 230 C7E - 03 5.0 31 0 7E - 03	6. 22.61 1 322.0	0,13193	16793.	10283.	424, 49 579, 00	1322
	1000							100 100 100
14	42.25	6.74865E-03 5.03266E-03	2.9204 1321.8	0.15486 22.946	18190.	3665.4 10280.	424.53 570,00	1.308
				0.17974		3665.4		
15	1.4000	7.27C21E-03 5.03237E-03	4.6144 1322.4	24.723	19598.	10293	424.39	1322
16	56.25	7.789475-03	17.200	0.2062#	20 795.	36654	424, 43	1.309
10	1.4000	5.03185E-03	1322.2	26.474	1.1475	10209.	570.00	1322
17	64.70	6.3C289E-03	10.965	0.23434	22377.	3465-4	474.68	1.308
• •	1.4600	5-0 200 3E - 23	1321.6	28.224	1.2240	19267.	573.00	1 321.
18	72.25	8.812656-03	11.624	0.2638T	- 23745.	3005.4	425-12	1.305
	1.4000	5,023626-03	1319,0	79,942	1.3005	10230,	570-00	1319,
19	81.00	9.33037E-03	12.305	0.29576	25139.	3465.4	425-15	1.305
	1.4000	5.023276-03	1318.0	31.699	1.3769	10228.	570.00	1.305
20	90.25	9. 83419E-03	12.941	0.72833	26486.	3665.4	423.78	1.301
•••••	1.4000	5.01507E-Q3	A335a9	23.367	1.4534	10175.	572,00	1316,
21	100.00	1.03299E-02	13.550	0,36129	27805.	3665.4	426.60	1.295
	1.4000	5.00529E-03	1311.7	35.033	1.5299	10100.	572.00	1312

	STREAMLINE & CP/CV	DENSITY	45	A3	FLOW 4NG(0)	P-STAT P-STAG	TEMP(R) 7-STAG	WACH NO
	0.G 1.4000	4,91497E-07 4,91897E-03	4.43463E-04 1312-2	0-0 0-0	1,3240 0,0	3607.2 4923.4	476.68 577.00	1.2999 1312.2
-	C.23	5.09317E-04 4.91635E-03	C. 66619 1311. 9	6.92277E-04 1.7319	1377.0 7.63109E-02	3602.2 9921.5	476.74 570,00	1.2956
<u></u> .	1.00	1.01775E-C3 4.91631E-03		7.59404E-03 3.5019	2739.1 0.15302	3602.2 9908.3	426.90 570.00	1.7946
, -	2.23 1.4000	1.52342E-03 4.91343E-33	1.5543 1310.0	6.05265-03 5.2479	41 04.7 0.2 2953	3602.2 9666.8	427.14 570.00	1.2930
<u> </u>	4.00	2,03194E-03 4,90911E-03	2. 6583 1308.2	1.41931E-02 6.9860	3456.4 C. 30604	3602.2	427,54 570.00	1.2906
•	4.23 1.4000	2.34175E-03 4.912695-03	3.3290 1309.7	2.22274E-02 . 8.7449	6634°3	3602.2	427.21 570.00	1.2927
	9.00	3.05845E-03 4.9263CE-03	4.0223	3.22274E-02 10.337	6233-9	3672.2 9979.2	426.03 570.00	1.2999
,	12.23	3.3612DE-03	4.7331 1322.2	4.42616E-02 12.359	9653.L 0.33556	3602. 2 10108.	424.47 579.00	1.3093
2	16.00	4-10764E-03	3.4397	3,63260E-02	11063.	3602.2 10237.	422.93 57%.00	1.3186
,	20-23	4.62861E-03 4.97093E-03	6.1672 1332.4	7.41197E-02 16.013	12495. C.66857	3602.2	422.22 570.00	1.3220
L	23.00	5.14349F-03 4.97133E-03	6.0543 1332.4	9.133006-02 17.795	13885.	3602.2 10302.	422.17 570-00	13232
2	30, 23 1,4000	9.63733E-03	7,5374 1332,3	0.11072 19.570	15271. 0.84156	3632.2 10298.	422.22 379.00	1.3224
3	36.00	6,10911E-03 4,96494E-03		0.13163 21.337	16631. C-91603	3602.2 10743.	422,39 370.00	
•	42.25	6,68262E-03 4,96834E-03	4.6968 1731.3	0.13445	18036.	3602.2	422.42 370,00	1.3216
۶	49.00	7.19909E-03 4.97323E-03	9.5888 1332-0	0.17927 24.901	19432. 1.0710	3402.2	422.28 570.00	1.3229
•	34.23	7.712476-03 4.96971E-03	15.271	0.20573 26.673	20 617.	3602.2	422. 12 372. 00	1.3223 1332.0
7	1.4000	8.22166E-03 4.76673E-03	10.939	0.23373	22168. 1.2240	3602.2 10267.	472.58 376.00	1.3207
	72.25 1.4000	8.726446-03 4.96179E-03	11.353	0.24316	23544. 1,3003	3602.2 10230.	423.02 570.00	1.3101
9	01.00	9.23966E-03 4.94124E-03	17.273	C.29499 31.929	24927. 1.3769	3602.2	423.05 370.00	1,3179
20	90.23 1.4000	9.73797E-C2 4.93393E-23	12.907	0.12749 33.620	24262. 1.4334	3652.2 10173.	423.47 570.90	1.3141 1323.9
	190.00	1.02269E-02 4.9434dE-03	13.516	0.36098 35.290	27 970.	3602.2	424.57 570.00	1.3087

STREAMLINE &	#1 0ENS17Y	h2 U	tr3	FLOW ANG(O)	P-STAT P-STAG	TEMPIRI T-STAG	WACH NO
0.0	4.18914F-07	6.42665E-04	C. 0	1.3149	3571.7		
1.4000	4.889136-03	1316. 9	0.0	0.0	9925.9	475.44 573,30	1316.9
0,25	3-C6876E-C4	0.66740	8.91221E-04	1365.2	3571.7	425,70	1.3019
1.4000	4,864521-03	131647	1,7543	7.65110E-02	921,5	579490	1310,7
1.00	1.012886-03	1. 3329	3,55985E-C3	2727.0	7571.7	425.86	1.3009
1.4000	4.88669E-03	1316.0	3, 5146	0.15302	9909.5	572.00	1314.0
2,25	1.518136-03	1. 5959	7.9959CE-03	4087.8	3571.7	*26.12	1.2995
1,4000	4.88363E-03	1314.7	5, 2669	0.22953	9366.8	573.00	1314.7
4.00	2.022235-03	2.6552 1313.0	1.41827E-02	5443.9	3571.7	42 6, 50	1,2970
1.4300	4.87934E-03	1313.0	7.0134	0. 30 50 4	9856. 6	570.00	
1.4000	2,52961E-C3	3. 3251	2.22015E-02 5.7767	4811.2	3571.7	424,17 570,00	1.2990
	4,8830#E-03	1314,5		0, 30255	9882.9		1314-5
9.00	3.043P5E-03	4,0174	3,21884E-02	8202.0 0.45906	3571.7 9979.2	424. 99 370. 00	1,3061
7-71			401000000000000000000000000000000000000	marial (I)	- 10	A 22	
12.25	3.564C9E-73 4,91457E-03	4, 7291 1326, 9	4.42767E-02 12.403	9613.3 0.53556	3571.7 10100.	423.44 570.00	1.3155 1326.9
	4. CBBC1E-03	5.4526	5.82496E-02	11037,	3571.7		1.3240
16-00	4. 93247E-03	1 3 33 . 0	14.249	0.61206	10237.	421.90 573.00	
20. 25	4-60670F-03	6,1590	7-40212F-02	12443.	3571.7	421.20	1.3291
1.4000	4.940796-03	1337.0	16.068	0.68856	10298.	570,00	1337.1
25.00	5.11911E-03	6.8452	9.14083E-02	13828.	3571.7	421.14	1.1294
1.4000	4.94136E-03	1337.2	17.056	0.76506	16305	570.00	1337.3
3C.25	5.630338-03	7. 5274	0,11057	15200.	3571.7	421.19	1.3291
1.4000	4.94081E-03	1334,9	19,638	9.84156	10298.	570-03	1337,1
36.CC	6.13564E-03	e. 2034	0,13146	16582.	3571.7	421.34	1,3201
1.4000	4.938406-03	1336.1	21.4)1	0.51803	10283.	570.00	1336.3
42.25	6.65069E-03	8. 8850	0.15424	17962.	3571.7	421.40	1.327
la4000	4,93840E-03	1336-0	23.192	0.99454	10260	570, 00	1336-3
	7.16469F-23	9,5761 1320.6	0.17903	19352.	3571.7	421,25 570,00	1.3207
	and the second second second second	To 17 order 1		-			
56.25 1.4000	7.67562E-03 4.93957E-03	10.257	0.20544	20731. 1.1475	3571.7 20289.	421.30 570.00	1.3289 1336.0
			0.23342	22397.	3571.7	421. 55	
1,4000	0.18238E-03 4.93661E-03	10,925	20.527		10267		1.7269
72.25	8-68475F-03	11.578	0.26284	23447.	3571.7	421.99	1.3243
1.4000	4.931496-03	1333.2	30. 264	1.3005	10230,	570.00	1333.5
81-00	9. 19494E-03	12-257	0.29461	24824.	3571.7	422.02	1.3241
1.4000	4.931156-03	1333.0	32.040	1, 3769	10226.	570.00	1333.4
90.25	9.69145E-03	12.691	0.32707	201540	3571.7	422.44	1.3201
1,4000	4,92384E-03	1310-1	32,740	1.4534	10179,	570,00	1330.4
100.00	1.01600E-02	13.499	0.36053	27457.	3571.7	423.53	1.3150
1.4000	4. 91350E-03	1 126. 1	35.415	1.5299	10100.	\$70.00	1326.

	ITERAT	10M NO. 0 3	-STATICH NO 4	2 Y-IKNER .	0.0001 Y-0	JTER - 2.0745	OUTPUT NO. •	1
	STREAMLINE & CP/CV	DENSITY ME	b2 U	¥3 Y	FLOW ANGED)	P-57A7 P-57AG	TEMP (P) T-STAG	HACH NO
1	0.0 1.4000	4.85990E-07 4.85989E-03	6.42272E-04 1 321.6	0.0	1. 3099 C. 0	3541.8 9925.9	424,62 570.00	1.3084
2	0.25 1.4090	5.04496E-74 4.85929E-03	0.44461	8.90167E-06 1,7645	1359.7 7,65110E-02	3541.8 9921,5	424.68 570,00	1.3080 1321.3
ì	1.00	1.00813E-03	1,3313 1320,6	3.55565E-03 3.5270	2716.0 0.15302	9541.2 9402.5	424.84 570.00	1.3071
	2.25 1.4000	1.51100E-03 4.4544JE-03	1.9936 1319.6	7.98656E-03 5.2856	4671.3 0.22953	3541. 8 9836. 8	425.10 570.00	1.3055
	4.00	2.01274E-73 4.65716E-03	2. 6521 1317, 7	1.41663E-02	5421.9 C. 30606	3541.8 9856.6	425.48 570.00	1.3032
,	6.25	2.51773E-C3 4.85385E-03	3. 3213 1319.1	2,21756E-02 8,8078	6743.4 C. 38255	3541.8 9882.9	425.13 570.00	1,3032
	9.00	3,02956E-03 4,56734E-03	4. C176	3.21497E-02	8168.8 C. 45906	3541.8	423.98 570.00	1.3123
_	12-25	3.54736E-03 4.88519E-03	4, 7232 1331,5	4,41506E-02 12,446	9574.4 C. 53510	3541.8 10104.	422.43 570.00	1.3214 1331.5
)	16-00	4.04862E-03	5. 4455 1330.3	5.81747E-02	10992.	3541.8	420.89	1.3309
,	·2C-25	4.585C8E-03 4.91174E-03	6-1509 1341-5	7,392926-02	12393.	3541.8 10298.	420.19 570.00	1.3352
 L	25.00 1.4000	9,095C8E-03	6.8361 1341.7	9-12871E-02	13772. C.76506	3541.8 10302.	470.16 570.00	1341.4 1.3353 1341.0
2	30.29	5.603896-03	7.5174	0,11047	151476	3541.0	420.18	1.9352
))	3t.00	4.91126E-03 6.11082E-03 4.90927E-03	1941 A.5 8. 1924 1340. 7	19.705	0.8815e 16515. 0.91805	10290. 3541.0 16283.	570,00 420,35	1341.4. 13342
•	1.4000	6.61947E-03	8.8733	0.15404	17889.	2541.6	420.39	1340.8
	3.4000 49.60 1.4600	7.13106E-03 4.91354E-03	1340.5 9.5634 1341.1	23,27 <u>1</u> 0,17679 24,072	0x99454 19273. 1.0716	102674 3541.9 10293.	572.00 620.29 570.00	1340,7 1.3348 1341.3
-	54.29	7.639596-03	10.244	0.20519	29647.	3541.6	420.29	1.3346
··	1.4000	4.91003E-03 0.14396E-03	1340.9	26.550 0.23311	22007. 1.2240	10289. 3541.8	577.00 420.56 573.00	1.3330
8	1.4000 72.25	4.907CBE-03	1339.7	26.624	23 352 .	3541.8	420.98	1340.0
9		4.902015-07. 9.151786-03 4.901646-03	1227A7 12.241 1337.5	30,368 0.29423 32.150	24773. 1,3769	10230, 1541.8	\$70,00 421.61 570.00	1,330,0 1,330,2 1,337,9
0	90.25	9.445958-03	12.474	0.32665	26048.	3541.8	421.63	1.3265
	100.00 1.4000	4.89444E-03 1.01322E-02 4.86412E-03	1334,7 13,462 1330.4	0.36,075 35.53 0	1.4534 27345. 1.5299	10175. 3541.8 16160.	570.00 422.52 570.00	1335.1 1.3211 1331.Y

STREAML 1		61 0ENS17V	u b2	v 3	FLOW ANGEDS	P-STAT P-STAG	TEMP(R) 7-STAG	MACH NO VELOCITY
	.0	4.83121E-07	6.40e 52E-04	0.0	1.3030	3512.6	423.62	1.3144
1.40		4.831216-03	1326.1	0.0	1.3030 0.0	9925.	57C-00	1324.1
	.25	5.C2166E-04	C. 66582	8.89112E-94	1354.3	3512.6	423.67	1.3141
	00		132249	1,7704	7.651136-02	9921,5	570,00	1.325,9
	-00	1.03347E-03	1-3298	3,55146E-03	2706.C	3512.6	423.83	1.3131
1.40	60	4.82480E-93	132.05	3, 53 92	0.15302	9938.5	570.00	1323.2
	.25	1. 124C3E-03	1.9913	7.97720E-03	4355.1	3512.6	474-10	1.3115
1.40	юс	4.82577E-03	1324.0	5-3039	0.22953	9886-8		1324.0
1.40	.00	2,00 345E-03	2. 64 91	1.41499E-02	9400.3	3512.4	424.47 570.00	1322.3
		4.82154E-03	1 322.3				570.00	-
1.49	.25	2.5C611E-C3	3. 3174 1323. 7	2.21497E-02 6,8383	6756.6 0.38255	3512.6 9882.9	474-15 573-00	1.3119
		4.823246-03						
1.40	00	?,C1557E-03 4.53861E-03	1325.0	3.211106-02		3512.6	422. 97 570. 00	1.3183
		400000000000000000000000000000000000000		The state of the s	D-9110			
1.40	2.25	3.53098E-J3 4.65635E-J3	4. 71 73 1336. 0	4.40951E-C2	9° 36.7 0.53556	3512.6 10108.	421.43 570.00	1. 1277 1336, 0
						3512.6		
1.40	00	4,050C4E-03		5.83983E-02 14.345	10949. 0.61207	10237	419.90 570.00	1,3769
	0.25	4.56391E-03	6.1427	7.382556-02	12343.	3512.6	419,19	1.7412
3.40		4.882256-03	1245, 9	16-176	0.68857	10200.	570,00	1346,0
	3.0C	5.C7155E-03	r. 627C	9.11662E-02	13717.	3512.6	417-14	1.3415
1.40		4.882846-03	1346.1	17.976	0.76506	10:02.	570.00	1346.3
	0.25	5-57402E-03	7.5075	0.11728	15086.	3512.6	419.19	1,3412
3, 4	00	4. 682288-03	1345.9	19.770	0.84156	10298.	577-00	1344,0
34	. 00	6. C3 263E-93	8.1218	0.13111	16440.	351 2. 6	419,36	1.3402
1.40	300	4,143296-03	1345-1	21.555	C.919C5	10283.	572.00	1345.3
	2.25	6.58891E-03	4. 6614	0.15384	17816-	3512.6	419.39	1.3400
	000	4,87990E-03	1344.9	23.345	0.99454	10280.	570,00	1345-1
	. co		9.5508	0,17055	19197.	3512.6	419.25	1.3428
1.40	970	4.44156E-03	1345.5	25.155	1.0710	10293.	570.00	1345.6
	0.29	7. 60431E-03	10-230	26.947	20565.	3512.6 10289.	410.20	1.3406
1,40		4.881056-03	1345.3		1.3475		572.00	1345.4
1.4	00	9.1C637E-03 87612E-03	10.896	0.23281 28.719	2191°. 1. 2240	351 2. 6 1026 7.	419.55 570.00	1.3390
								-
1.4	2.25	8.674C6E-03	11.548 1342.2	0.26216	23259. 1.3025	3512.6 10230.	419.98 570,00	1.3364
1.4	1,00	9-10952E- <u>C3</u> 4-87273E-03	12.225	32.257	24624.	3512. <u>6</u>	420.01 970.00	1. 1362
	Control of the Control		UN 100	North Control				
	0.25 000	9.60141E-03 4.26555E-03	12.850 1339.2	0.32623 33.477	25944. 1. 4534	3512.6 10175.	420.63 570.00	1,3225
10	6.00	1 • COE54E-C2 4 • 25529E-03	13.4 <u>65</u> 1335.1	0.15963 35.658	2723e. 1.5299	3512.6	421.52 570.00	1.3271

51	CP/CV	#1 DENSITY	n =5	, n)	FLOW ANGIOS	P-STAT P-57AG	TEMPIR } T-STAG	MACH NO
J	0.0 1.4000	4.8C297E-07	6.39092E-04 1330.4	0.0	1.2962	348 % 9 992 5 9	422.63 570.00	1.3204
2	C+25	4.558761-04	C- 05 505	8-88054E-04	1340.5	3483.9	422.66	1.3201
		4-802376-03	133944	1,7765	7.651135-02	9921.5	570,00	1330.4
3	1.4600	9.98593E-04 4.83037E-03	1-32 <u>82</u> 1329-7	3.54726E-03 3.5512	25 95.3 0.15392	3483.9 7908.5	570.CÓ	1,3191
•	2.23	1.44717E-03	1.5009	7. 467828-03	4039.1	3453.9	423,10	1.3175
	1.4000	4.79756E-03	1325-5	3.3219	C-22953	9886.8	₹70.00	1220.5
5	4.00 1.4CCO	1.554315-03	2. 6460	1,41334E-02 7,0869	5379.1 C.326C4	3493.9	423.48	1326.8
			1150.00521		CO. T. C.			
• 	6.23 1.4000	2.4 9468E-33 4.79702E-03	3.3135	2.71735E-02 8.85°3	673C.1 0.39255	3483.9 9882.9	423.15 570.00	1.3173 1328.2
7	9.00	3- CO1 + SE - O3	4. CC2 9	3-20771E-CZ	6104-2	3483.4	421.98	1.3243
	1.4000	4.410338-03	1333.5	10.684	0.43906	979.2	570.00	1333.5
5	12.23	3-3140dE-03 4-02796E-03	4.7113 1340.4	4.40397E-02	9498.7 C.33556	3483.0 10100.	425.44 570.00	1.3336
•		4.03157E-C3	5.4313	5. 80226E-02		3402.9	41 0. 91	
,	16.0 <u>c</u> 1.4000	4.94534E-03	1347.2	14.392	10906.	10237.	570.00	1.3429
0	20.25 1.4000	4.34310F-03 4.85371E-03	6.1344 1330.3	7.37273E-02 16.229	12295.	3483.9 10298.	410.21 570.00	1.3471
1	25.00	5.04843E-03	6, 81 80	9,10454E-02	13663.	3483.9	410-16	1,3474
14	1.4000	4.854295-03	1350.5	18.034	0.74506	10302.	570.00	1350.6
ž	30.29 1.4000	5.55259E-03 4.85373E-03	7. 4975 1350.3	0.11013 19.834	15027. C-84154	3483. 9 10298.	418.21 570.00	1.3471
3	3e.00	6.C5487E-C3	0.1710	0-13094	16384.	3483.9	410,38	1,3441
	1-4600	4. 631 76E-03"	1349.5	21.425	0.41 805	16203.	577.00	1344.7
4	42.25	6.53847E-03 4.85137E-03	8. 5300 1349. 3	0.15363 23,424	17748.	3483.9 10280.	41A.41 57C,00	1.3459
			9. 3382	0.17832	19121.	3482.9	410-27	
ž	1.4000	7.04577E-C3 4.85393E-03	1349.9	25.237	1.0710	10293	576.00	1350-2
6	56.23	7.5e964E-C3	10.217	0.20465	25484.	3485.9	410.31	1.3465
	1.4000	4.95252E-07	1349.7	27.035	1,1475	16564.	577-00	1350.0
Z	1.4000	8.06941E-03	17.882	0.23230 20.875	21833. 1.2240	3483.9	418.56 579.00	1.3450
	72.25	8.:6483E-C3	(1.51)	0.26141	23167.	3483.9	419.00	1.3424
	1.4C0Q	4,844396-03	1346,6	30,569	1, 3005	10535	570,00	1346,9
9	1.4000	4.64424E-03	12-209	0.29344	24527 <u>.</u> 1.3769	3493.9 10228.	419.03	1,3422
	1 00 00	the state of the s	187	000491955	ATT ATT			
0	90.25 1.4000	9.55763E-03 4.837[16-03	12.341 1343.6	0.32581 34.088	25842. 1.4574	3403.9 10175,	419.45 \$70,00	1.3384 1344.0
	100-00	1.003946-02	13.449	C-35918	27129.	3483.8	420.53	
	1.4000	4-82490E-03	1339.4	35.776	1.5299	10100	57C.CO	1,333 <u>1</u>

			-STATION NO 40				OUTPUT NO	1
	STREAMLINE &	DEMSITY	52 U	w3 	FLOW SAGERS	P-STAT P-STAG	TEMP(R) T-STAG	AFFOCIAN
1	0,C	4.74815E-07 4.74815E-03	6.35735E-C4 1739.3	0.0		3428.3 9925.9	570.00	1.3321
2	0.25 3,4000	4.95443E-04 4.74756E-03	0.66344 1339.1	8.85544E-04 1.7882	1330.6 7,45113E-92	3428.3 9921.5	470.74 570.00	13314
₹	1.00 1.400C	4.74578E-03	1.3251 1338.4	3.538866-03. 3.5745	2674.7 0.15302	3428.3 9908.5	420.90 579.00	1.3308 1336.4
4	2.25 3.4000 /	1.48 38 4E -03 4.742806-03	1. 99 42 1337. 2	7.94911F-03 5.3569	4008.2 C. 22953	3477.3 9846.8	421.17 570.00	1.3293 1337.2
ž	4.00 1.400	1.97663E-03	2,6398 1335.5	1.41706E-02 7.1336	5338.0 C. 30604	342°.3	421.54 570.00	. 1.327¢ 1335.5
•	6.25 1.4000	2.47256E-03 4.74227E-03	3.3057 1337.0	2.2071 7E-02 8.9267	6675.6 C.38255	3426.3 9892.9	421-21 570-00	1.3290
7	9.CO 1.4000	2.57521E-03 4.75543E-03	7.5932 1342.2	3.19947E-02 10.754	8042.3 C.45906	3428.3	420.05 570.00	1.3360
•	12.25	3.40372E-03 4.77286E-03	4.6995 1349.0	4.39294E-02 12.610	94 26.5 0. £ 3556	3478.3 10108.	418-51 570-00	1.3453 1349.1
 .	16.00	3.55583E-C3 4.790256-03	5.4173 1355.7	5.787?4E-02 14.483	10827 . 0.41207	342 9, 9 1023 9,	417.00 570.00	1. 1545 1355. 8
0	25.2 2 1.4000	4.50252E-03 4.79831E-03	6-11-05 1358-0	7.35338E-02 16.331	12 201. 0. 6 8 8 5 7	3428.3 10298.	416.29 570.50	1.3587 1356.9
l	25.0Q 1.4000	5.00368E-03 4.75889E-03	6.8000 1359.0	9.0805 9E-02	13558.	3428.3 10302.	415-24 570-00	1.3590 1359.1
2	30.22 1,4060	5.50336F-73 4.79833E-03	7,4778 1358.8	0.10984 19.959	14912. 0.84156	342P.3 10298.	416.29 570.00	1.3507
3 .	36.00	6.C2119F-03 4.79639E-03	8.1496 1356.0	0.13059 21.761	1625 9. C.91805	3426.3 10283.	416.46 573.00	1.3577
4	42.25 1.4000	6.5C072E-03 4.7960CE-03	8,8268 1357.8	0.15323 23.911	17612. 0.99454	3428.3 10280.	416.50 570.00	1.3575 1350,0
	49.00 1.4000	7.00313E-03 4.79763E-03	9.5131 1356.4	0-17755 25-396	18974.	342A.3 10293.	416.35 570.00	1.3584 1358,6
16	56.25 1.4000	7.5C2545-03 4.79714E-03	17.190 1358.2	0-20411 27-205	20327. 1.1475	3426.9 10264.	416.40 579.00	1.3501 1358.5
17	1.4000	7,55747E-03 4.79425E-03	19.653 1357.0	0.23189 28.994	21666. 1.2240	3429.3 19267.	416.65 470.00	1.3566 1357.4
8	72.25 3.4000	6.46851E-03 4.78429E-03	11.503 1355.1	0.26114 20,762	2299C• 1,37C5	3426.3 10230,	41 / • 0A 570 • 00	1.3540 1355.4
2	1.4000	8.55760E-03 4.78895E-03	12.177 1354.9	32.548	24340 <u>.</u> 1.3769	9428.3 10228.	417,11 576,60	3.353 <u>0</u> 1355.3
0	90.25	9.47290E-03 4,79190E-03	12.809 1352,1	0.32498 34.307	25644. 1.4534	3428.3 10175,	417.72 970.00	1.3501
31	100,60	9.95043E-03 4.77181E-03	13.415	0.35828 36.006	26922.	3420.3	418.41 570.00	1.3447

111	ERATION NO 0	A-STATION NO	48 Y-1 NNER =	0.0001 Y-00	TER = 2.09%	OUTPUT NO. =	i
STREAMLINE I	DENSITY	W2 U	A 2	FLCW ANGEOD	P-STAT P-STAG	TEMP(R) 7-STAG	MACH NO
0,0 1.4000	4.69521E-0		0.0	1,2702 0,0	9925 , 9	418,81 570.00	1.3429 1347.7
0.25	4. 51176E-04 4. 6946ZE-0		0,63837E-C4 1,7994	1326.7 7,65110E-02	3374.9 9921.5	418.86 570,00	1,3432 1347,5
1.00	9,81517E-04		3.53049E-03 3.5970	2654.9 0.15302	3374.9 9908.5	41 % 07 570,00	1.3422 1346.6
2.25 1.4000	1.47112E-0		7.53^41E-03 5.3907	3976.5 0.22953	3374.9 9886.8	419.28 570.00	1.3406 1345.6
4.20	1,95961E-0	3 2.6337 3 1344.0	1.40677E-02 7.1785	5298.3 0.39604	3374.4 9856.4	419.65 570.00	1.3384 1344.0
6.25 1.400C	2.451 ZBE-0 4, 68 940E-0		2.2C199E-02 6.9430	6629.1 C.38255	1374.9 9882.4	419.33 270.00	1.3404 1345.4
1,4000	2,94960E-0	3.5836 3 1350.6	3,19174E-C2 10.621	7982.5 0.45906	3374.9 9979.2	410-17 570-00	1.3474
17.25 1.4000	3.45373f-3 4.71964E-0		4.35197E-02 12.458	9355.9 0.53556	3374.9 10108,	416.64 577.00	1.3566 1357,4
14,00	3,96143E-0	3 • • • • • • • • • • • • • • • • • • •	5.77229E-02 14.571	10742. 0.6126*	3374.9 10237.	415.13	1.3658 1364.0
20.23 1,4000	4.464C6F-0		7.33413E-02 16.429	12110. C.68857	3374.9 10298.	414.43 570.00	1.3700 1367.1
25,60 1,4000	4, 46349F-0	3 6. 7422 3 1367.2	9.05676E-02 18.257	13457. 0.76506	3374.9 10302.	41 4. 38 570, 00	1.3703
30.25 1.4000	5.45591E-3 4.7440张-0		0.10955 20,080	148Cl. 0.84156	3374. 9 10298.	414.43 570.00	1.3700 1367.1
36,00 1,4000	5, 94953E-0 4, 74291E-0	3 0,1203 3 1366-2	C.1 3025 21.693	16178.	3374. 9 10283.	414,60 570.00	1.3690
42,25 1,4900	6.44475E-0 4,74252E-0		0.15283 23.714	17481. 0,99454	3374.9 1070c.	414-83 570-00	1.3666
1,4000	6,94284E-0	3 7.4863 3 1366.6	0-17738 25-549	10833. 1.0710	3374.9 10293.	414.49 570.00	1.3696
56.25 1,4900	7,43795E-0 4,74365E-0		0.2C337 27.370	20176. 1-1475	3374.9 10289.	414.53 57c.00	1.3694 1366,7
1,4000	7.92992E-0 4.74079E-0		0.27129 29.170	21 504. 1 . 2249	3274.9 10267.	41 4. 78 470.00	1.3679
72.25 1.4009			C. 26046 30. 949	1,3005	3374.9 10230,	415-21 579-00	1.3653 1363,7
1.4000	4.73556E-	1363.2	0.29195 32.766	24159. 1.3769	3374.9 10228.	415.24 570.00	1363.6
- 1.4000	4.72650E-		0.32416 34,517	25453. 1.4534	3374.9 10175.	415.85 570.00	1.3614 1360.4
1.4000	9,86477E-0		0.35738 36.228	26 722. 1.5299	3374.9 10100.	416.73 570.00	1.3561

	AMLINE &	DEMSITA	w2	v 3	FLOW ANGIOS	P-STAT P-STAG	TEMP(R1 T-STAG	WACH N
	-						135	
·	1.4000	4.64355E-07 4.64395E-03	6.29674E-04 1355.9	0.0	1. 2578	9925.9	41 6. 97 570. 00	1355.9
	C. 25	4.87059E-04 4.64337E-93	0.66C29 1355.7	0.81733E-04 1,8103	1319.1 7.65110E-02	3373.5 9921.5	417.03 570.00	1.3541
	1.00	9.71289E-C4	1355.0	3.522116-03 3.6188	26 35.7 0.15322	3323.5	417.18 570.00	1.7533
.	2.23	1.45879E-03	1. 5745 1353. 8	7.91172E-03 5.4235	3549.8 D. 22953	3?23.5 9886.6	417.44 570.00	1.251 (135?.)
	4.00	1.943196-03	2.6275	1.403486-02	5260-1	3323.5	417.61	1-3499
	1.4000	4.63465E-03	1352.2	7. 2224	0.30604	9656.4	570.00	1332.
	6.25	2.430738-03	3-2902	2.19691F-02	4581-1	3373.5	417,49	1.351
	1.4000	4,47829E-03	1353.4	9,0176	0.38255	9802,9	570,00	1353.
	9-00	Z.52487E-03	2. 9740	3,184C3E-02	7924.8	3323.5	415-34	1.350
	1.40C0	4.651C6E-03	1330-7	19.866	C.45906	9979.2	\$70 . 50	1350.
	12.25	3.42478E-C3	4,6761	4-37102E-02	9288-2	3327.5	414.82 -	1.367
	1,40CC	4-811E-03	1345.4	17, 763	0.53556	10124.	\$7C-00	1365.
	16.00	3-42022E-03	5.7894	5.75742E-02	10664.	3323.5	413-31	1.376
	1.4000	4.68512E-03	1372.0	14,657	C.61206	10237.	376.00	1377-
	20-25	4.426648-03	6. 0065	7. 11497E-02	12022.	3323.5	412.62	1.361
	1.4009	4,493C1E-03	1375.0	16.525	0.68857	10298.	570-00	1375.
	25.00	4.919CZE-03	6-7645	9.09309E-0Z	13300.	3323,5	412.57	
	1.4000	4.69357E-03	1375.2	18.364	C.76506	lesez.	570.00	1975.
	30.25	5.41C25E-03	7.4388	0.10927	14693.	3323.5	412-61	1,301
	1.4000	4-69303E-03	137449	70,197	0.64156	10299.	573,00	1375,
	36.00.	5-89966F-03	8,1072 1374-2	0.12091	16021. C.91805	3323.5	41 2, 78 570, 00	1.380
	1.4000				107 100 1	190		
	42.25	6.39074E-03 4.49075E-03	8.78C9 1374.0	0.15243 23.052	17354. C. 79454	3323.5 10280.	412.61 570.00	1.374
	.1.499¢							
	1.4000	6.85466E-03 4.69235E-03	9.4635		1.0710	3323.5 16293.	41 Z . 67 570 . CO	<u>1.790</u>
			100			3.2		
	56.25 1.4000	7.37561E-C3 4.69186E-03	10-137 1374-4	0.20304 27.529	2003C. 1.1475	3323.5 10249.	412.72 570.00	1.300
·					,			
	1.4000	7.86255E-C3	10.797	0.23069 29.340	21349. 1.2240	3323,5	412.97 570.00	1373
	72-23 1-4000	4.34329E-03	11.444 1371,3	0-25985	22653. 1.3005	3323.5 10230.	413.39 570.00	1.374 1371.
	1.4000	6,63554E-C3	12.119 1371.2	6.29120 37.958	23984	3323 <u>-5</u> 10226	413,42 570-00	1.376
	100000					2023117	9103	177
	90-25	9.31.264F-03 4.67696E-03	12.744 1368,4	0.37333 34.720	25269. 1.4534	332 % 5 101 75.	414.03 570.00	1.372 3360.
	10C-00	9.782CBE-03	13,348	9.35649	2632 8. 1.52 9 9	3323.5	414.91 579.00	1365.

	5	112	b3	¥4	P-STAT	TEMPTRE	MACH NO
CP/CV_	DENS 174	<u>u</u>	Y	FLOW ANGEDS	P-57AG	7-STAG	AETUCIAA
0.0	9.772858-07	3-119946-04	0.0	2.4044	9418.4	561.52	0.27484
1.4000	9.772855-C3	319.25	0.0	0.0	9925.9	570.00	319.25
0.21	1.327046-03	C. 42207	-9.28544E-C3	3204.8	9418.4	561.58 .	0.27386
1.40CQ	9-771926-03	31.6,95	<u>-</u> -5, 9971	-1 • 26 <u>03</u>	9923-5	570+00	218-13
C. 89	2,552276-03	0.93405	-3.46983E-02	-2.5194	9418.4	561.75	0.27093
1.4000	9.764758-03	314.47	-13, 837	-2.5194	9911.3	370.00	314.77
1.87			-6.295Z6E-02	9778.2	9418.4	567.C4	C. 26694
1.4000	9.75370E-03	328.50	-30-361	-3,7760	9893.4	570-00	309.17
3. 29	5.297078-03		-0.13992	13024.	941 8.4	562,44	0.25921
1.4000	9.75678E-03	300.18	-26.415	-9.0291	9868.9	570 . 00	301.34
5.05			-C. 21125	16261.	941*.4	562.90	0.23111
1-4000	9,749926-03	\$9C-29	-31.932	-6.2773	9940-7	577-07	292.04
7.26			-0.32398	19573.	9418.4	561.64	0.27281
1.4000	9.770718-03	314.19	-41.473	-7.5106	9918.3	570.00	314.92
10.11			-0.49050	22927.	9618.6	56C.C3	0.29842
144000	9.798886-03	342.14	-52.690	-8. 7548	10019.	570-co	346-18
13.74	1.06844E-02		-0.71375	26 358.	941 7.4	557.64	C. 33294
1.4000	9.8 4 G 86E - 03	379.56	-65.823	-7.9818	10170.	57C-00	385,40
18.20			-0.95774	29768.	9418.4	556. C7	0,35390
1,4000	9.86853E-G3	401,29	-79.456	-11,200	10270,	570,00	409408
23,39		5,4444	-1.1978	33114.	9418.4	555.60	0.35994
1.4000	9. 476878-03	406.17	-89.357	-32.407	10:01.	\$70.00	415,66
29.04			-1.4412	36423.	9418.4	555.62	0.35968
1,4000	9. 676516-03	473.93	-97.75 <u>)</u>	-13,604	10299,	5 7 9, 00	
35.24	1.6G777E-02	6.4094	-1.6921	39717.	9418.4	555.85	0,35676
1.4000	9. 872498-03	397.65	-105.24	-14.789	10295.	570.00	412.31
41.92			-1.9692	43013.	9418.4	555.92	0,35580
1.4000	9+87117E-Q	395,37	-113.68	-15.961	10260.	572-20	
49.10	1.87614E-02 9.47475E-03		-2.2672	-17.119	9418.4 10243.	595.72 575.00	0.35841
1.4000	4.074755-03	395.61	-151.01	-17-114	105.4.34	577.00	414-16
46.7			-2.6024	49647,	9418.4	555.79	0, 35 753
1.4000	9-87355E-Q	392,36	-129.48	-18.263	Tusua.	575.00	413-17
64.80		8,2350	-2.8987	52905.	941 8.4	556-14	0,35250
1.4000	9.966676-03	314.38	-1 35. 30	-19.392	10263.	570.00	407.50
73.25			-3.1616	56136.	9418.4	556.72	0.34532
	9+3702E-03	374-09	-139491	-20,596	10228	570.09	799,40
			-3,5353	59432.	9418-4	556,74	0,34479
1.4000	9.85632E-03	370,78	-146.83	-51.604	102200	570,00	398. 80
90.90			-3.7694	62595.	9418.4	557.69	0.3*276
1.4600	9-84043E-C	355,39	-148.55	-22-685	10169+	570.00	3 45 . 1 9

STREAMLINE & CP/CY	DENSITY	VŽ U	₩3 V	FLOW ANGEDS	P-57A7 P-57AG	TEMP(P) 7-STAG	MACH NO VELOCITY
0.0	9.65765F-07	3.53210E-C4	0-0	2. 3805	9263.8	555.97	C. 31560
1.4000	9.657956-03	365.73	0. 0	0.0	9925.9	572.CO	365.73
0.30	1.256055-03	C-56782	-8, C1833E-03	3108.7	4923.5	557.99	0.39223
144000	9,4C2131-03	657,06	-6, 2036	-0.80904	9921,9	572-00	452-10
1.25	2.473626-03	1.2139	-1.58663E-02	6134.9	8741.6	549,95	0-42695
3.400C	9.26137E-03	490.76	-6.4142	-C.74682	9908-8	570.00	490.80
2.69	3.64C12E-03	1.8612	-3-466 CE-02	9135.6	16:2.2	546.71	0.44050
1,4002	9.18739E-03_		-9-4195	-1-0671	9885.5	570,00	505.79
5.21	4.87553E-C3	2.5016	-0.10889	12108.	8586-9	349.06	0.44743
1.4000	9.12585E-03	512.96	-22.334	-2.4931	9851.6	572.00	513.45
8.32	6. C20C1E-G3	3.3398	-0.27025	1490.	F422.7	544.20	0.4664
1,4,000	9.017748-03	554.70	-46.386	-4.7793		570-00	556.71
	7.1e3906-03 8.94295E-03	4.2792 597.33	-0.54779 -76.465	17892.	AZE5.5	539.A3 577.00	602-21
17.46 1.4000	8.37407E-03 8.96044E-03	5.2344 625.07	-0.17456 -104.45	20961. -9.4664	8251.9 13196.	536.57 570.00	0.55013 633.74
	30				434 77		
23.43	9.7C351E-03	5. 9335	-1.1727 -126.85	24272. -11.160	8384.1 10286.	537 <u>.66</u>	0. 54837 623, 29
29,98		6.4071	-1, 3736	21712-	8581.4	541.01	0-51763
1.4000	1.11347E-02 9.24194E-03	576, 97	-124.14	-12.143	19302.	572.00	590-18
36.97	1 - 25 76 2E - GZ	6.7046	-1.4510	31 29 3.	8815.2	545.24	0.47655
1.4000	9.42006-03	533.11	-115,36	-12.711	102-8.	570.00	545.46
44.10	1-41974E-C2	6, 6793	-1-4357	35096.	e110.5	550-62	0.41953
1.4000	9.64045E-03	471,79	-101,41	-12,131	10253.	573.00	457,56
51.13	1.575216-02	6.5077	-1.4884	38970.	9356.9	5 45 - 05	0.36697
1.4000	9.832546-03	413.13	-94.427	-12.08Z	102 90.	570.00	423.80
50.01	1.729526-02	6.4110	-1.6749	42667.	9418.4	550.67	0.33307
1.4000	9.965356-03	370.68	-96. 844	-14.642		567, 99	383,32
64.58	1.86951E-02	4. 9290	-1.0015	46503.	9416.4	547.81	C-28716
1.4000	1. C1 097E -C2	313.76	-95.142	-16.901	9973.3	551,76	327,95
70.37	2. C 5 31 dE -02	4.9257	-1.7354	5C404.	9412.4	535.22	0.22378
1.4000	1-02530E-02	219,50	-#3, 112	-19-108	9753.0	£40.59	253.89
75.12	2.20372F-G2	3. 98 97	-1.5244	54015. -23.911	0418.4	531,90	C.37143
1.4000	1.031706-02	131.04	-69, 175	-53.411	9413.6	535.03	193.81
79.72	2-3:2736-62	4.6527	-1.8918	57 2C 7a	9418-4	531.09	0.19610
1.4000	. 1,027deE-Q2	199045	61,799	-22,127	965 8. B.	\$3.79.75	217,31
81.42 1.4900	2,44456E-02 1,01729E-02		-2,5496 -194,30	-22,795	9418.4	539,43 545,47	269.20
92.35 1.4000	2.5:141E-02 1.0058sE-02	6. 5069 270, 71	-2.9573 -1:5.91	67716. -23,379	9410.4	545.56 557.77	0-25720 294-48
1:0-00	2-56 136E-C2	7.4574	-3, 2013	45495.	9418-4	550.13	C.26607

	PACA PALINE &	MI DENSITY	H2 U	W3 V	FLOW ANGIDS	P-STAT P-STAG	TEMPER 1 T-STAG	MACH NO VELOCITY
	0,0	9,073286-07	5.05500E-04	c. o	2, 2473	8422.8	547.88	0_49004
1	4000	9.02328E-03	560.23	C. 0	0.0	9925.9	570-00	367.23
	0.34	1.185578-03	0.06203	-2.05028E-02	2952.5	8425,4	544-02	C. 48866
1	4QQQ	9,023656-03	556.43	-17.204	-1,7736	9919-8	570,00	550-69
	1.35	2.369758-03	1. 3219	-6. *1281 £-92	5989.4	8404.4	543.92	0-48960
	4000	9.CC 276E-03	556.98	-22.810	-2.9504	9901.2	570.00	559,73
	3,00	3.56533E-C3	1.9259	-C-11153	8868-7	8477.7	545.76	0.47125
	1.+300	9,05C65E-03	536,74	-31.257	-3.3236	987C.3	570.00	579.65
	. 54	4 971405-03	9 6170	-0.14013	11560.	8524.4	546, 75	0.46114
	5.26 1.40CC	4,77149E-03	2, 51 7C 52 7, 51	-0.15813 -33.142	-3, 5949	9862.5	572.00	528.55
	8.29 1.4000	3.89486E-G3 5.97885E-Q3	3. 4291 581.71	-0.27471 -46.6C1	147C4. -4.5802	8347.1 9978.7	541.65 577.00	C. 51154 583,50
	12.37 1.4000	6 - 91765E - 03 8 - 78086E - 03	4.58C4 662.13	-0,51544 -74,511			533, C5 570, 00	0,56875
	1.4000	a. 18000E-03	4.02.13		W			00003.
	17.59	7.92179E-03	5.6634	-C.26097	19966.	7768.2	576,47	0. 64293
	1.5000	4,61912E-03	71.4, 91	-108-68	-8.6441	10284-	570,00	723.12
	23- 40	8, 57703E-03	e.5324	-1.2372 -137.81	22659.	7691.3	524. 34	0, 65 981
	1.4000	8.54647E-03	727.68	-137.81	-1C.724	10301.	570-00	740.61
	30.03	1.01166E-02	7, 26 96	-1.5919	25574.	771 3. 6	524, 96	0.45497
	1,4000	8+54129E-03	714,58	-137,-36	-12,352	10289,	570. CO	7,35,61
	38.50	1.14726E-02	7.7869	-1.8596	28857.	7940.5	529.47	0. 61 868
	1.460C	a, 73aC3E-03	678,74	-162.09	-13.432	10279.	577.00	697.03
	46.50	1.31520F-02	7.9121	-1.9859	\$2800.	2404.4	537.98	C-54554
	1,4000	9.10635E-Q3	621,59	-151.00	-14.090	10294.	970.00	620-25
	64 29	1.506786-02	7, 3499	-1 9473	37401.	9007.7	548.78	0.43974
		9. 5e 371E-03		-1.9473 -130.56	-14,965	10217.	577.00	504.96
			5, 5125	-1. 7942	420374	9418.4	54%11	
,	el.03 1.4000	1.70371E-02 9.99362E-03	346, 63	-105.19	-16.001	19091	567.03	C. 31536
	65. 8C	1.8964ZE-02	3. 4507 1 82. 30	-1.2362 -65.186	464P3. -19.666	9418.4 9613.5	531.58 535.00	0.17172
_	555	14 7 7 3 6	337	22.000.0000				
•	68.70	2.C4439E-02	2.2246	-0.8998	50138.	9418.4	. 527,59	0. 10405
	1,4000	1.040126-02	1 38, 60	-43,931	-22.024	7570.0	524.74	117-15
<u> </u>	71.8Ç	2,1662LE-02	3. 6676	~1.5661	53095.	9418.4	532-16	0.17066
	1.4000	1.031206-02	178, 55	+17,220	-22,297	9611.8	533.26	192.98
•	76.85	2.263922-02	6-0472	-2.4199	55637.	9415.4	541.C1	0, 2323
	.L. 4000	3,9143XE-92	267.11	-105.89	-21,510	9844.9	547,90	
Q	83,87	2,357356-02	7-7350	-3.0882	58075.	94[8.4	552.13	Ç. 3073
	1.4000	9.97512E-03	328.12	-171.00	-21.764	10050.	560.32	333.3
0	91.99	2.470216-02	8.2506	-3, 3724	60869.	941 8.4	554.10	0-3110
	1-4000	9,902596-03	331,98	-136.56	-27,360	10072	564, 89	350.9
	100.00	2 41 4275 63	7 6104	3 2007	64 307.			
l	1.4000	2,61427E-02 9,95610E-03	7.5194 287.43	-3, 3 785 -12 6, 56	-23,749	9418.4	551.18 559.40	D. 2730

STREAMLINE &	DENSITY	#2 U	¥3 V	FLOW ANGLOS	P-STAT P-STAG	TEMP(R) T-STAG	MACH N
0.0	4.59847E-C7 9.57847E-03	3.72154E-04 387.72	0-0 C-0	2-3683 0-7	9184-0 9925-9	557-49 570-00	0, 33 <u>500</u> 367, 72
C.19 1.4000	1.24215E-93 9.763C2E-93	C.36840 312.68	-2.14698E-02 -17.284	30 55.4 -3.1640	9419,4 9906,9	560.93 569.10	C.28974 313,16
0.70 1.4900	2.5C483E-03 9.86762E-03	C.66684 267.02	-6.15960E-02 -24.591	-5. 2616	9418.4	5%6.12 562.11	0.23197 268.15
1,4000	3.17174E-93 9.90712E-03	C, 89354 ?36-91	-0.10624 -28.167	9255.3 -6.7405	941 R.4 9703.4	553-91 558-64	C-20600 238,57
2.31 1.4002	5.C7215E-03 9.99282E-03	C, 862C0 165, 95	-C.11562 -22.795	12426. -7.8398	9418-4 9566-1	549-16 551-60	0.14921
3-C9 1-400C	6.36645E-G3 1,0377E-32	C. 73885 116,07	-0.10293 -16.162	15588. -7.9308	9418.4 9427.5	546.70 547.84	0.1022
3.80	7.6315CE-C3 1.00240E-02	C. 84717 115.60	-0.14512 -19.016	18680. -9.3418	9418,4 9487,4	547.45 549.59	117-1
4.80 1.4000	8.18364E-03 1.00078E-02	1.0214	-0.20223 -22,751	21757. -11.109	9418.4 9497.2	548.33 549.48	0.1020
5, 86 1, 4000	1.02188E-02 1.02672E-02	1,1689	-0.25799 -25.248	2591Z. -12.446	941844 9457.6	545.10 546.24	0,1023
7.07 1,4000	1.164C7E-02 1.01939E-02	1.3185 113.27	-0.34767 -29.867	28493. -14,772	9418,4	534.32 539.44	0,1029
10.08	1,24687E-G2 9.82718E-03	4. 8804 391.42	-1. 4838 -119.00	30793. -16.911	937 0.9 10227.	556,07 570 . 90	0,3539 409.1
15.55 1.4000	1.23034E-02 9.58926E-03	6, 3785 476, 59	-2. C641 -154, 23	33212. -17.932	9037.4 10299.	549.11 570.00	0.4361 500.9
22.20	1.441236-02	7 - 3222 508- 36	-2.3778 -164.99	35036e -17.991	8874.6 103CO.	546.25 570.00	0.4663
29.76	1.54111F-02 9.14339E-03	8-2542 535-60	-2.6178 -169.87	38368. -17.597	6719.1 107 P 5.	543.72 570.00	0.4919 361a
35.31	1.630238-02	9. 3567 573. 95	-2. 9764 -178. 2 6	40717. -17.256	\$505.0 16281.	539.93 570.00	0,5276
47.91	1.72077E-C2 9.04173E-C3	10.425	-3.2584 -109.37	43076. -17.358	9325.0 10293.	530.46. 570.00	0. 5599 634. 1
58.32 1.4000	1.83706F-02	11.017	-3-5911 -195-46	45974. -10.055	8338.7 10262.	536.89 579.00	0.5551
49.01	1.96124E-02 9.18564E-03	11.015	-3.5465 -194.15	49437. -19.250	6511.2 10233,	541.14 570.00	0,5164 588,1
79.47	2,1:472E-C2 9,34739E-03	15.930 512.00	-4-1511 -194-46	53124. -20.797	9743.9 10228.	\$45,03 \$70,00	C, 478
90.68	2.2F565E-02 9.4F156F-03	10.513	-4.3510 -199,36	56710. -22.484	694C.1 10171.	549.38 570.00	0.433 497,
100.00	2,43380E-02 9,59132E-03	5, 931 6 406, 00	-4, 3700 -179,58	60 215. -23.749	9110.6. 10100.	553,46 570,90	0.386

3	TREAMLINE &	DENSITY MI	h2 U	w3 Y	FLOW ANGLOS	P-SYAY P-STAG	TEMP (R)	VELOCITY
•						775752		
	1.4000	9.51036E-C7	3,97836E-04 418,32		2.3498	9066.2	555,43 570.00	0.36210 418.32
	G. 22	1.15930E-C3	0.50529	-1.31042E-02	2864.6	8989.6	594-15	0-37815
	1.5000	9,431916-03	436,20	-11,313	-1,4856	9422.1	572,00	436,35
	1.4000	2,24720E-03 9,37596E-03	1.048C 45c.22	-5.53352E-02 -24.068	5686.8 -3.0223	8892.9 9910.4	557.63 570.00	C.39647 456.86
	2.11 1.4000	3.41G48E-93 9,24111E-93	-1.6312 478-30	-0.13172 -38.622	8453.3 -4.6165	9774.3 9890.1	550. 6 3 570. 00	C.4[710 479.66
	3.85	4.47C40E-03	7,2963	-0.25840	11104.	8576.4	547.76	0.45057
	1.4000	9.12476E-03	513.67	-57. 003	-6.4204	9860.3	570.00	516, 91
_	6,24	5.4784 PE-03	3. C810	-0.45938	13652.	8320.9	543. G9	D. 49774
	1,4000	6,54631E-03	562.38	-63- 652	-8.4805	9676.9	570.CO	568,59
•	9.37 1.4000	6.49298E-03 8.83503E-03	3, 9506	-0.71633 -110.32	16235. -10.277	9161.4 9970.5	522,17 572,30	C. 54378
		041440404						546.41.46.41
	13.26	7.56025F-03 8,84217E-03	. 4. 7940 432.43	-0.95390 -125.44	16929.	8125.1 10116.	535.40 570.00	C. 56845
							537.48	
	17.60	9. 82594E-03 9. C3907E-03	5.4209 612.12	-1.1216 -126.65	27154. -11.690	8338.3 10242.	573,00	% 55005 625-09
	22, 73	1-03C34E-G2	3.6623	-1.2584	250670	8720.9	542.54	0.49314
	1,4000	9,34804E-03	550.19	-122,14	-12.516	10298.	570.00	563,50
	27.43	1.169526-02	5.4198	-1.4319 -122.44	29042.	8584.3	548.14	0.44659
	1.4000	9. 549878-03	477.62	-122.44	-13.023	10302.	\$75.00	512.40
	33.22	1.28904E-02	6.3007	-1.6953	31998.	9011.0	549.67	C. 44084
	1,4000	9,568946-03	494-79		-15,060	10298.	570,00	500.17
	39.11 1.4000	1.39870E-02 9.51783E-03	496.38	-1.0*30	34741. -14.945	10283.	547. 82 579. 00	0. 44 999 51 6.2
	45.57	1.51918E-02	7, 5911 502, 66	-2.2639 -149.91	37526.	8997.2 10282.	547-10	0.4574
••••	1.4009	9,485975-03			-16.606		<u>572-00</u>	<u>524, 54</u>
		1.62887E-02	8. 1392 499. 65	-2.5507 -156.59	40476. -17.400	892 <u>2.3</u> 19294.	570.00	223.43
_	59.94	1.754e9E-C2	8.4534	-2.8334	435624	170 P. 170 P.	548.51	0.4425
	1.4000	9.55233E-03	481.74	-2.8336 -161.40	-18,531	8992.7 16287.	577.00	508-1
	67.51	1.88245E-02	8, 5838	-3.1022	46672.	9074.2	5°C.43	
	1.4000	9.60/36E-03	453.99	-164.85	-19.870	10246	570.00	484.8
	75.22	2-006578-02	8. 1544	-3.3808	49702.	9126.1	551.79	0.40616
	1,5000	9,438446-03	436,30	-168,49	-21.115	10556	572,00	467,470
	03-19	2,13615E-02	9,1580	-3.7299	526574	9136.1	557.00	0,40393
	1.4000	9.64552E-03	430.73	-175.43	-22.160	10224.	57C-00	465.00
0	91.45	2.23679E-02	9.4366	-4.0094	55377.	911e.1	552.51	0, 3978
	3,4000	9,61336E-Q3	421,89	-179.24	-23,021	101e7e	570.20	458.39
	100.00	2.337728-02	5.4002	-4. <u>2121</u> -184. 30	57923.	9059.9	552.57	0. 39714

STREAMLINE &	DENSITY	WZ	A	FLOW ANGLOD	P-STAT P-STAG	TEMPER)	MACH NO VFLOCITY
0.0	9.352e JF - 07			2. 31.68	9925.9	551 • 74	0.40682
1.4000	9.352496-03	454.41	G* 0	0.0	445244	570.00	468.41
0.24	1.122466-03	C. 53216	-1.17144E-0	2 2752.3	8828.3	551.29	0.41100
3.4000	2. 330336-07	473,94	-10-433	-1. 2610	9921,	570,00	474,05
0.95	?.24147E-03	1.0629	-4.93643E-0	2 5554.2	8814.4	551.24	0.41248
1.4000	9.31657E-03	474.21	-22.023	-2.6590	9909.6	57C-00	474.72
2.14	3.35549F-03	1.5664	-0-11360	0214.4	5798.7	551.29	C. 411 94
1.4700	9.279226-03	472.91	-33.856	-4. 3948	9869.0	570-00	474.12
3.80 1.4000	4.44544F-03	2.1298 477.66	-C.20862	11C29a	8742.5	570.00	482.95
	45 240 005 - 03	417680		-26 2442	40,748 1		46.26.42
6.01	5.5CC59E-C3	2.80%6	-C. ?6231	12661.	8602.5	547.94	0.44869
1.4000	•.14745E-03	510,61	-69.067	-7,3504	9877,1	5??.00	514.84
8, 91	e.52229E-C3	3.6637	-0-56944	16253.	8424.8	542.06	0.49806
1.4000	4.039635-35	561.72	-40.373	-9.1398	496C*8	573.00	568.94
12.60	7.55665F-03	4.5772	-0-26374	10092.	6294.5	528-37	0-54196
1,4000	5. 976626-03	635.72	-114.30	-12.686	10129.	57C.00	616.41
17.04	8.e9771E-C3		-1 1150	21741	8376.3	537.25	C. 55209
1.4000	9. 040 72F - C3	5.3365 613.55	-1.1350 -130.49	21761. -12.007	10255.	577.00	527.28
22.92 1.4000	9.56749E-03	5. 1004 501. 73	-1.3453 -134.97	24886. -13,058	854C.1 10299.	540.30 570.00	C-52429
144000	4.504316-03.		78 370 7.1	,-N39.42.9		3100 00	597.38
27.34	1.12749E-02	6. 0899	-1.5084	20086	8761.8	544.25	0.48638
1.4000	9.37996E-03	536. 89	-133.74	-13.914	10301.	570.00	556.21
32.96	1.2:0936-02	6.4640	-1.7062	31155.	1965.6	546.23	0.46649
1,4000	9.456748-03	516.74	-136,39	-14,786	19291.	570.00	534.43
30.95	1.367608-02	6.5219	-1.9453	33043.	9898.7	547a 00	0.45851
1.4000	9.478628-03	50a.06	-142.22	-15.698	10279.	570.00	525.64
45.39	1.483766-02	7.4504	-2-2266	30971.	7912.8	547.14	0.45707
1.4000	9,49126F-03	502-13	-1 5C · 06	-10.639	10276	579.00	424,01
52.26 1.4000	1.6C327E-02	7.9027		39823. -17.680	8952.0	547.72 570.06	0. 4°C96
		*****					,,,,,,
59.49	1.724796-02	0.2471	-5.404	42812.	90000	\$45.76	0.43989
1,4000	9.542146-03	476-15	-162-65	-14,807	10560	577.00	505.12
66.90	1.84396E-02	6.4980	-3.0771	45731.	9046.9	550.00	0.4263
1.4000	9.583876-03	460.86	-165.87	-14-402	19551.	570.00	490.14
74.75	1.559508-07	8. 6605	-3.3820	4:556.	9651.6	5*7.48	0.42105
1.4000	9,540486-03	452,41	-172,68	-20,891	10224.	. 70,00	404.25
02-91	2.071745-02	9,3554	-3.7460	51 369.	994C-1	550.31	0.42301
1.4000	9.57141E-03	451.57	-1 80- 81	-21.022	10724.	577.00	486.43
91.36 1.4000	2.18337E-02 9.55493E-03	9.5717 436.45	-4.0132 -103.53	44097. -22.747	9039,3 10166,	551.19 573,00	0. 41 31 2 4 75 . 4 1
							
100.00	2,29469E-02	9-6657	-4.2617	56919.	9044.4	557.30	0.40030
1.4000	9.541336-03	422.09	-1 45. 72	-23.749	10107,	570.CO	461.15

	TREAMLINE E	¥1	W2 .	W3	W4	P-STAT	TEMP(R)	MACH NO
	CP/CV	DENSITY	<u> </u>	<u>y</u>	FLOW ANGLOS	P-STAG	T-STAG	VELOCI 74
	0.0	9.24197F-07	4, 631 AZE-04	0.0	2. 2933	8708. \$	549.09	0.43436
	1.4000	9.241076-03	501.22	0.0	0.0	6925.9	570.00	501.22
	0.24	1.C9071E-03	0.54793	-1.239(9E-02	2756.9	9679.3	549.48	C. 43751
	la5992	9+23276E-03	502,341		-1.2955	9921-6	570+00	502-49
••••	1.4002	2.14191E-03 . 9.23473E-03	1, 0843	-4.99837E-02 -22.907	5413.5 -2.6391	8711.5 9909.4	549.40 570.20	0.43300 497.50
_	2.12 1.4000	3.27 £35E-03 9.24 48 7E-03	1.5974. 487.56	-0.11143 -34.133	61 24.9 -4.0045	6733.4 • 9889.0	550.12 570.00	C. 42511 488,76
••••								
	3,73	4.37634E-03 9.26295E-03	2. C776 474. 94	-0.19638 -44.893	10841. -5.3997	2760.7 -860.8	570.06	477.04
	5-76	5-4732dE-03	2,5009	-0-31430	13564-	8770.4	551.10	0-41406
	1.4000	9,272436-03	473-01	-57.425	-6.9221	986 6. 4	570.00	476,48
	8.32	6.56051E-03	3.2741	-0.49419		8724.6	540.00	C. 43950
• • • •	1.400	9. 26277E-03	499.04	-75. 324	14285. -8.5833	9962.3	570.00	504.69
	11.53	7.637556-03	4-0784	-0.73691	19001.	6653.2	345.49	C. 47397
• • • •	1-4000	9,24261E-03	533,99	-96.465	-10.242	10092	579.00	542.64
	15,46	e, 72154E-03	4. 9327	-1,0197	21747.	8595.1	542,24	0.50595
	1.4003	7. 23557E-03	3 9 5 . 55	-116.91	-11.660	10236.	570 . CO	577.51
	20.07	9.83154E-C3	5, 6245	-1.2718	24574.	8598.3	541.36	0. 51426
	3,4000	9.25396E-03	572,09	-129.36	-12.741	10258.	5 70 - 00	586,53
	25,23	1.09576E-C2.	6.1875 564.21	-1.4892 -135.90	-13.543	103024	541.97 570-00	0. 5C076

	30.85 1.4000	1.23623E-02 9.33491E-03	6.7138 555.67	-1.7143 -141.89	30118. -14,324	8665.7 10295.	542.62 570,00	C.50225 573,50
••••		7/0			32992.	8659.1	543.25	•
••••	36. 73	1.32008E-02 9.31921E-03	7,2216	-1.9607 -148.53	-15.190	10281.	\$70.00	0,49615 566.86
_	43,47	1.43215E-02	7-7602	-2.2474	35670.	8705.8	543,51	0.49364
	1.4000	9,332086-03	341, 86	-156,94	-16-152	10263.	573,09	564.13
	50.48	1.544986-02	6.3012	-2.5670	38464.	8723.5	543.67	C-49206
•	1.4000	9.34866-03	537.30	-15e-15	-17.103	10294.	570.00	562.41
,	57.94	1.45735E-02	E. 7452	-2.6921	41272.	6740.6	544. CB	C. 40800
	1,4000	9,360278-03	530. Ç8	-174,50	-10,221	10287.	570-00	558,04
	65.78	1.703436-02	5.1879	-3. 2051	44016.	8754.2	544,80	0.48091
	1.4000	9. 36 34 3! - 23	514.55	-101.24	-19.231	10237.	570.00	550.20
1	73.96 1.4090	1.86003f-02 9.36877E-73	·9-5562 598-41	-3.5253 -187.52	46769. -20.245	8777.6 10227.	545.56 570.00	0.4732
								591,81
·	1.4000	9.305626-72	9. \$757 500. 21	-3. 8973 -195. 43	49 594 . -21 • 340	8795 <u>, 2</u> 10225•	545.49 570.00	C. 4685
_	91.24	2-109956-02	10.075	-4-1775	52409.	9344.4		0.0
•	1.4000	2.10995E-02 9.40785E-03	477,51	-4.1775 -197.99	- 22 • 520 - 22 • 520	10146,	547.76 579.00	0.4505 516.9
	100.00	2. 22937E-02	9. 9970	~4.3967	55289.	8914.5		
i	1.400°	2. ZZY37E-0Z 9. 44329E-03	448-42	-197 ₀ 31	-23.749	10100	557. C2	0, 4261

STREAMLINE &	w1	m2	₩3	H4	P-STAT	TEMP(R)	MACH N
CP/CV	OENS174	¥	Y	FLOW 4MG(0)	P-S7AG	7-57AG	VELOCIT
0.0	9,151186-07	4.816CZE-04	0.0	Z. 2743	8590.5	546,95	0.45907
1.4000	9.1511ae-C3	526.27	0.0	0.0	9025.4	570.00	526.27
0.24	1.06357E-C3	C. 55772	-1.260956-02	2635.0	8588.2	546.97	0.45682
1.4000	9,146398-03	525,86	-11.467	-1.2952	9921.6	570,00	526.00
0.95	2-12043E-03	1.1071	-5.054926-02	5268.7	4593.4	547.26	0.45576
1.4000	9.149256-03	522.09	-73. 639	-2.6144	9909.6	57C.00	572.6
2-12	3-18137E-03	1.6392	-C.11374	7502-0	6965.2	547.90	0.4501
1,4000	9.152656-03	515.24	-35. 751	-3.9692	9869.0	570.00	516.4
	•				······································		
1.4020	4.24765E-03 9.16588E-03	2. 1375 503. 23	-C.2002	10 544. -5. 3458	8632.4	548.74 570.00	0.4401 505.4
5.70	5.32641E-03	2. 6731	-0.31089	13220.	8673.7	549.39	0.4330
1.4009	9,15560E-73	494-16	-58, 346	-6.7338	7866.9	570-00	497.5
	6.42136F-03	3.2416	-0.46433	15943.	8694.1	540.35	0.4443
1.4000	9. 23784E-C3	504.76	-72.315	-6.1512	99:6.0	577.0C	510.0
11.36	7.51050E-C3	3. 5515	-C.66411	18674.	8684.2	546.31	0.4656
1.4000	9.261836-03	526,14	-88, 425	-9.5402	10075.	572.00	533.5
15,11	6.57776E-03	4. 6052	-0.91755	21377.	8624.8	542.93	0.4993
1.4000	9.25595E-03	560.20	-106.97	-10.010	10226-	570.00	570.3
19.54	9.02314E-03	5.5661	-1.1719	24016.	8568.0	540,90	C. 5186
3-4000	9.230226-03	578.62	-121.78	-11,865	10794.	570.00	591.7
24.50	1.06634E-C2	6. 22 CC	-1.4130	26 676.	A533.7	543.14	0.5757
1.4000	9.20525E-03	584.06	-132.59	-12.190	10305	572.00	594.9
49 29			- 2			7311 10	7000
30.17 1.4000	1.171C3E-DZ 9.19049E-03	6.8444 594.45	-1.6630 -142.01	29247. -13.657	4516.0 12298.	53 9, 89 577, 00	0.528C
			•				
1.4000	1.27681E-02 9.18529E-03	7.4C85 552.23	-1.9262 -153.86	31863 <u>.</u> -14.574	^{8514.3}	540. 08 970. 00	0.5262
1.4000	A. 182525-03	224.43	-125.00	-140314			599,5
42.84	1. 185676-02	7. 5798	-5.5550	34549.	8516.5	540.17	C. 5254
	9.1094][-03	576,71	-150.50	-14.560	70545	572-00	595.6
49.92	1.490946-02	8. 5740	-z. 55e0	37231.	0521.1	540.03	C. 5267
1.4000	9.193596-03	\$75.07	-171.45	-16.606	17294.	570.00	630°0
57.48	1.598155-02	5.1010	-2.9002	27902.	6529.7	540.27	0. 5245
1.4000	9.19775E-02	569.47	-161,47	-17.675	10266.	57C.00	597.6
65.44	1.705756-02	9, 5332	-3.2422	42548.	8545.6	540.99	0. 5177
1.4000	9.203616-02	558,88	-190.07	-18.783	10260.	370.00	590.3
1:.14	1. #161-E-C2	5. 2788	-3.5542	45788.	5591.6	54 (+13	0.536
1.400C	9.222956-03	543.93	-197,75	-19,942	10227.	572.00	270,0
STATUTE					****	***	
1.4000	1.92959E-02 9.25587E-03	17.257 531.50	-3. 9755 -296. CO	48096 <u>.</u> -21,185	10225.	547,95 570,00	0,4990 570.0
91.16	2.5-+57E-CZ	10.350	-4.2867 -209.67	50881. -22.482	8686.9 10167.	544.98 570.00	0.479
1.4000	9,2093E-03	504,63					548.1
100+00	2,161,08-02	10.322	-4,541.6	53695.	6767.0	547.33	0.4550
1.4600	9-22832E-03	477.64	-210.16	-23.749	10100-	579.00	521.

	STREAMLINE & CP/CV	M1 DENSITY	. #5	A	FLOW ANG(D)	P-SYAT P-S74G	TEMPER)	VELOCITY
	0.4	9.040CSE-G7	4. 98994E-04	0.0	2.2551	8470.9	54 4, 76	0.48130
	1.4000	9.Ce006E-03	550-65	0.0	0.0	9925.♥	570.00	550.65
_	G. 24	1.03019E-03	0.50641	-1.713026-02	2564.1	8471.0	544.83	0.48064
),4 <u>c</u> op	9,05902E-03	549, 81	-11.702	-1-2277	9921.6	570-00	549,93
	C. 95	7.05842E-03	1.1274	-4.88798E-02	5122.7	8469.1	544, 99	C. 47905
	1.4000	9.054396-03	54 7.68	-23.722	-2.4801	9909.4	570.00	548.20
	2.12	3.C4433E-03	1.6767	-0-11079	7674.5	8465.2	545.23	0.47655
	1,4000	9.04672E-03	544.28	-95.921	-3.7759	9889.0	570.00	545.44
	3.7e	4.10965E-03	2.2105	-0-1 96AS	10222.	8467.7	545.73	0.47158
	1.4000	9.04354E-33	537. 88	-47.9C7	-5.0897	9860.7	575.00	540.01
_	5.84	5.14320F-C2	2.7543	-C.3C760	17792.	8479.6	545.83	0.47051
	1-4000	9-051746-03	535-51	-59,807	-6.3725	9848-2	570.00	531.84
	6,41	6.193276-03	3.3500	-0.45310	15417.	5490.5	544-62	0.48275
	1.4000	9.08343E-01	547.37	-73-160	-7.6124	4036-1	\$70.00	552.24
	11.55	7. 25263E-C3	4, 6947	-0.63276	18076.	8494.7	542.83	0.50022
	1,4000	9.11777F-03	564.58	-87.246	-8.7445	10078.	570.00	571.29
	15.33	8-1C426F-03	4. 5056	-C.85640	20737.	8467.4	540.07	0,52641
	1.4000	5.139016-23	590.73	-103.13	-9.9026	10227.	570.00	599.67
_	19.75	9.33322E-C3	5. 64 CB	-1.3911	23332.	6434.1	538.46	0.54119
	1,4000	9-126856-03	604-38	-116-90	-13.947	10294.	570.00	613-78
	24.76	1.03440E-02	6-3009	-1 - 3286	25871.	8401.6	537.74	0,54766
_	1.4000	9-103256-03	629.13	-128.46	-11.909	10302.	570-00	655.33
_	30,31	1.135216-02	6, 9337	-1.5825	28401.	8375.4	537.33	0, 55135
	1-4000	9.C8225E-C3	410.78	-139-40	-12-057	10298.	570.00	626,4.9
}	36,37	1.23656E-C2	7.5225	-1.8531 -149.96	30936.	8367-4	£37,33	0,99139
-	1.4000	9.06877E-03	676-34	-149, 96	-13.039	10583*	573-00	624.52
_	42.93	1.33903E-02	6.1170	-2-1551	33502.	4350.8	537.26	0.55200
	1.4000	9,064946-03	636,18	-160,94	-14.664	10282	570,00	627×1.9
<u>.</u>	49.99	1.442456-02	8,7252	-2.4957	36094.	8358.0	537.05	0.55364
	1.4000	9. C6760E-03	624.89	-179.02	-15.962	10294	370.00	629.14
,	57.53	1-54652E-C2	9.2584	-2.8524	38691.	6368.1	537.34	0.55130
	1.4000	9.0736FE-03	\$ 9 A . 66	-184.44	-17,124	10282.	570.00	624.43
<u>.</u>	65.48	1.651616-02	5-6930	-3. 21 51	41 294.	8391.3	53F-18	0-54374
	1.4000	9.034678-03	586.88	-194.67	-18.351	10260.	570.00	6[8.37
	73.75	1.755378-02	10-043	-3.56.19	43953.	8432.5	539.42	0.5325
	1.4000	9.168195-03	570,05	-203.70	-19,438	10347,	577,00	606-31
9.	62.34	1.970156-02	12,427	-4, 5027	46692.	8479,4	540,51	0, 5241
_	1.4009	9.14301E-03	557.54	-214.03	-21.001	10225.	570.00	597.2
0	91,14	1.981326-02	10.501	-4.3530	49398.	8542.5	542.33	0.5050
	3,4000	9-17753E-03	513,04	-21 % 70	-22-400	10166,	570.00	576.5
I.	100.00	2-094046-02	12.576	-4.6534	52125.	6613.9	544.66	0.4823
٠.	1.4000	9-21472E-03	525.05	-222.22		loico.	370.00	551.7

	LTERAT	<u> </u>	<u> </u>	<u> </u>	W4	P-SYAT	TEMPERA	HACH NO
; 	CP/GY	OFFRITA	<u>u"</u>	y"	FLOW ANGLOS	P-STAG	T-STAG	VELOCITY
J		8,84519E-07 8,84519E-03	5.34933E-04 604.77	0.0	2.2095 0.0	8191 <u>.0</u> 9925.9	539, 56 570, 60	0. 53114 604.77
2	0.24	9.66363E-04	0.58447	-1.04561E-02	2414.0	5186.9	\$39.54	0. 53127
	1.4000	8.84098E-03	604,81	-10,420	-1.0249	9921.8	570.90	604.91
3	0.94 1.4000	1.93010E-03 8.83302E-03	1.1654 693.80	-4.22507E-02 -21.890	48 21 . 2 -2.0763	818C-6	539.61 570.00	0.53061 604.19
4	2.11	2.69013E-03	1.7406	9.62352E-02	7216.7	8169.2	539.72	0,52967
	1.4000	8.81905E-03	672.27	-33.290	-3.1645	9889.3	570.00	603.19
<u> </u>	3,74 1,4000	3.84581E-03 8.80210E-03	2.3055 595.49	-0. <u>17217</u> -44. 768	7634 <u>.4</u> -4.2707	9861.0	539.92 570.00	0.52779 601.16
6	5.84	4.5G292E-03	2.8913	-C.27130	11997.	8144.3	539 , 57	0. 53101
	1.400c	8.79454E-03	601.98	-56.486	-5.3605	9868.4	570, 00	604.63
7	1.4000	5.77326E-03 8.8051 X-03	3.5615 61 7.57	-0.40173 -59.535	14471.	8128.2 9959.4	537.85 570.00	C. 54667
•	11.60	6.74831E-03	-, 2906	-0.55983	16901.	elle.7	535.78	0.56511
	1.4000	8.42669E-03	635, 81	-82.9:8	-7. 4338	10001,	570.00	641,19
9	15.38 1.4000	7.73C26E-03 8.84733E-03	5. C862 657. 96	-0.75149 -97.214	19 395. -8. 4047	1022 4	533.14 570.00	0, 1 e761 665,10
10	19.77	8.6574ZE-03	5. 6117	-0.95570	21841.	8076.6	531.83	0,59904
	1.4000	8.84633E-03	658. 21	-109.88	-9, 3393	10294.	570.00	677,18
IJ	24.73 1.4000	9.64345E-03 8.82980E-03	671.66	-1.1710 -121.43	24227. -10.246	9050.5 10302.	531.72 570.00	0.60414
12	30.21	1.05775E-02	7.1364	-1.4110	26583.	8019.6	537.69	0. 60854
	1.4000	8,80466F-03	674.11	-133.40	-11.193	10298.	577.00	687.18
13	26.21	1.15067E-02	7, 7563	-1.6776	28924.	7992.9	530.41	C. 61 089
	1.4000	8.78001E-03	674.07	-145.86	-12.205	10283.	570.00	68 9. 65
14	42.72	1.244J8E-02	6,3905	-1.9824	31 280.	7971.2	530.03	0.6140e
	1.4000	8.74250E-03	674,43	-159.35	-13,293	10781.	570.00	693.00
15	1,4000	1.33845E-02 8.75397E-03	9. 0338 674. 94	-2.3327 -174.26	33644. -\4.479	7956.3 10294.	529.55 570.00	0.61797 697.08
16	57.25	1.43345E-02	9. 6119	-2.7141	36053.	7953.6	529.59	0. 41 745
	1.4000	8.75046E-03	67G.53	-149.33	-15,768	10748.	570.00	696. 75
17	65.20	1.52956E-02	10-105	-3.1203	38 453.	7965.6	530.21	0.61256
	1.4000	8.75346E-03	660-63	-204.00	-17 • 161	10262.	570.00	691.41
16	73.51	1.02833E-G2	10.516	-3.5509	40905.	7998.0	531.32	6.60)29
		.8.77050E-23	645.44	-218.07	-18,658	10228,	570,80	68].66
19	82.15	1,73122E-02	1 G. 936	-4.0424	43 463.	0045.0	532.25	0,59550
	1.4000	8.80677E-03	631. 67	-233.51	-20 , 288	10225.	570.00	473,45
20	91.54	1.83696E-02 8.85237E-03	11.113 675,02	-4.4958 -244,76	46042. -22,025	8121.5 10168.	534.54 570.00	C,57528 652.65
? }	100.00	1.94776E-C2 8.91752E-03	11.130 571.40	-4.8970 -251.42	48 721. -23.749	0227.5 10100.	537.56 570.00	0.54924

STACAHL THE &		w2		W4	P-STAT	TEMPLE	MACH NO
CD/CA	OENSITY	V	<u>v</u>	FLOW ANGIO	P-STAG	T-STAG	VELOCITY
1,4000	8.5971CE-07	5,69681E-04	0.2	2.1565	7071.2	531.45	0.56529
					1000000	5.00 L 000 M	un Charling
0.23	9.07446-94	C. 59806	-0.22136E-C3	2259.7	7860.2	533.30	0.58659
14969	8,58751E-Q3	£63,96	9.3873		9921.9	570.00	664,02
0.92	1.798316-03	1.1939	-3.37568E-02	4511.5	7845.8	533.20	0.58673
1.4000	8.57646F-03	66 3 . 90	-1 6. 771	-1.6196	9909.8	577.00	664.16
2.07	2-69178E-03	1.7858	-7.76498E-02	6752.9	7834.7	527.30	0.55661
1.4000	8.55974F-03	663.41	-28.847	-2.4898	9889.9	570.00	664.04
2.68	3.57993F-03	2.3706	-0.13996	6960.6	7816.6	533.37	0.58595
1.4000	8.53469E-03	662, 1 9	-39.096	-3.3789	9862.0	570.00	663.35
	4.46733E-03	2,5721	-0-22135	11210.	7797.6	532.95	0.58953
5.74 1.4000	8,524628-03	665.29	-49,549	-4, 25 <u>9</u> 4	9865.Z	570. CO	667,13
					14, 2, 3		
1.4000	5,36121E-03	7.6525 601.20	-0.326C9	13470.	7770.6	531.05 375.00	684.02
1.4000	86 72 3 785 - 03	001054	-014177	-30 6 364	443441	370800	00-02
11.41	6.26295E-03	4. 3624	-0.45852	15756.	7745.1	520.77	0.62436
	6.53420E-03	699, 95	-73,235	-5,9731	10073.	570.00	703.77
15.10	7.159956-03	5.1625	-0.61680	18055.	7706.2	525.77	0.64853
1.4000	6.539826-03	723.62	-86,146	-6.7571	10724.	570,00	728.93
19.39	8.C3961E-C3	5, 9210	-0.78660	20297	7666.7	524.06	0.66207
1,4000	8.523896-03	734.47	-97.839	-7,5674	10288.	570,00	742.94
24,23	6.89376E-03	6-6217	-0.96998	22471.	7615. A	522.67	0.67133
1,4000	8. 43645E-03	744.53	-109.06		10361.	570.00	···· <u>·</u> 752.46
				24549.		No. of the last	
29.62 1.4000	9.72870E-03 8.43927E-03	7. 1123 751.62	-1.1780 -121.09	-9.1519	7557.3 10299.	521.76 570.00	741.31
35,53.	1.05475E-02	7, 5575 757, 28	-134.96	26698. -12.060	7496.4	520.76 570.00	0. 48755
1.4000	8.38/185-03	131.20	-134034	-175000	105 040	310.00	769.11
41.96	1.135746-02	8.6740	-1.6981	28760.	7434.3	519,59	0.69649
3-5000	#• 33650E - 03	753•.73	-149.51	-11.976	10500	570,00	778423
48.94	1.216326-92	9.3797	-2.0315	30830.	7373.0	517.18	0. 7071
1.4060	8.29025E-03	771.15	-167.02	-35.536	10293.	570.00	789.01
56.44	1.25626E-07	10, C43	-2.4114	32.0794	7919.7	517.15	C. 71481
1.4000	6,24617E-03	774.80	-1 86 ₀ 03	-13,501	10269.	570.00	796.8
7 64.41	1 12/424 02	10 445	-2. 8380	34925.	7290.3	516.70	
7 64.4 <u>1</u>	1.37652E-02 8.20951E-03	10,643	-236.17	-14-930	10265	579.00	0.71 A1
8 72.66 1.4000	1.454071-02	11.168	-3.3148 -227.18	37014 . -16,532	7256.4 10229.	510.94 579.00	0. 71 63 6 798,41
9	1,547326-02	11.600	-3.8871	39742.	7263.1	517,32 570,00	0,71355
1.4000	8.202846-03	754.84	-251.21	-10.408	10226.	> 17. 00	795.55
0 90.91		11.945	-4.5351	41593.	7357.5	519.64	0,6961
L+QQQ	8.24965E-Q3	727.29	-274-09	-20 - 790	10170.	570+00	777.83
1 100.00	1.7619CF-02	11.855	-5-2163	44451.	7574.9	525.02	0.65450
1.4000	8.40640E-03	672.67	-296.06	-23, 749	10100	570.00	735.1

	STREAMLINE & CP/CV	OENZILA Mj	u2 U	W3	FLOW ANGEOL	P-STAT P-STAG	TEMP(R) T-STAG	WACH NO
		E (11000111						
٠	1.4000	1. 24864E - 37 8. 24864E - 03	6.00556E+C4 737.77	0.0	2.0815	7428.Z 9925.9	524,69 570.00	737.77
	C.23 1,4000	9.28650E-04 8,24773E-03	0.61092 737,25	-4.87981E-03 -5.8889	2041.0 -0.45765	7428.2 9921.9	\$24.75 570.00	0,45659 737,28
ŧ	0.90	1.65175E-C3	1.2204 737.93	-2.25477E-02 -13.634	4173 <u>.3</u> -1.0565	7414.7 9910.2	524.66 570.00	C-65734
	1.4000			-136634			7.0800	
	2.03 1.400C	2.47313E-03 0,21263E-03	1 - 6277 738 - 64	-5.30825E+02 -21.458	6243.1 -1.6636	7393.4 9696.6	524.52 579.00	0.65°40 739.16
	2.61	3.28557E-03	2,4323	-9.79885E-C2	6297.2	7362.4	274.31	0.65008
•	1.4000	0.10141E-C3	746.29	-29.824	-2.3070	9863.3	570.00	740. 81
	5.64	4.09165F-03	3.C519	-C.15368	10333.	7325-1	523.58	0. 44583
	1.4003	0.151516-03	745.87	-37,550	-2.8627	4861.5	572.00	746.82
Z	8.15	4.89742E-03	3,7472	-0.22984	12308.	7277.3	721-19	C. 69428
	1.4600	8.13093E-03	764.23	-46.930	-3.5136	9945.5	370.00	765.27
	11.20	5.649C6E-03	4.4807	-0.32049	14444.	7214.5	518.29	0.70632
	1,4000	8.11C35E-03	786.21	-56,235	-4.0912	100549	57C-C0	788.22
•	14.81	6.48998E-03	5.2824	-0.43186	16491.	7136.2	514,49	0.7344
	1.4000	0.08157E-03	613.93	-66.542	~4,6737	10214.	570.00	814.41
0	19.00	7.248498-23	6. C446	-0.54933	18434.	7045.5	511.64	0,75521
	1.400	8.02330E-03	433.92	-75.784	-5, 1927	10263-	570,00	837.35
l	23.75	7.96980L-03	4.7021	-0.67198	20375.	6937.9	504.13	0-77314
	1.4000	Y.9 3964E-03	65C. 97	-54, 316	-5.6585	10301.	570.00	855.1
2	29.04	8-65-266-03	7.5120	-0.40762	22173-	4616.3	506.59	0.7911
	1.400	7,83964E-03	667.81	-93-298	-6, 1363	102*9.	570,00	872.81
3	34.67	9.294156-03	P. 2399	-0.94493	23798.	6673.8	503.74	0.0110
	1.4000	7.719266-03	886.19	-103.76	-6.6792	10265.	970.00	892.24
4	41.25	9.8772TE-03	8.9872	-1.1646	25345.	6494.8	499,93	0. 8371
	1,4000	7.569326-03	909.89	-117.91	-7,3636	10279-	570.00	91 7-45
۶	48.19	1.03943E-02	9. 7597	-1.4061	26758.	6285.1	495.09	0.8697
	1.4000	7. 396598-03	938.95	-135.27	-9.1981	10201	370.00	948.6
6	55.7¢	1.0T945E-02	17.518	-1.6678	27901-	6016.9	468.99	C. 91 01
	1.4003	7.16936E-03	974,38	-154.51	-9,0102	10289.	570-00	986.5
7	63.74	1.11583E-02	11.219	-1. 7639	28951.	5762.9	483.28	0.9472
	1.4000	6.94779E-03	1005.4	-1 *6.00	-9.9295	10268	570.00	1020.
	72.29	1.134.36-02	11.475	-2-2401	25/09.	5402.9	470.44	0.9907
	14400Q	6,68014E-C)	1041.7	-196,51	-10,683	10230,	570,00	1,060,
9	81.32	1.12846F-02	12,510	-2.4891	29885.	5034.3	465.51	1.059
	1.4000	6.30111E-03	1098.9	-21 8.44	-11.253	10227.	570.00	1120.
0	90.74	1.08611E-C2	12.950	-2.2609	20037.	4379.3	448-04	1.165
	1,4000	5.69501E-03	1192,3	-208.90	-9.9377	10171.	570.00	1210.
	100.00	B 440436-83	12 044	-2.4936	33744	2000 4	485 83	
1	1.4000	8.66843E-03	12,066	-287.01	23746. -11.673	2990.4 10100.	402,57 570,00	1.4420

	STREAMLINE, E.	DENSITY	⊫ 2 U	N3 V	FLOW ANGEDS	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VELOCITY
	•	7.991136-07	6.311296-04	0.0	2.0256	7105.6	51 9. CO	0.70786
	1.4000;	7.99113E-33	709. 79	c. o	0.0	9925.9	570.00	789.79
	0.24	7.96961F-04	0. 541 40	1.C4174E-C4	2022.9	7007.5	516.C9	C. 72272
	1-5000	7,911236-03	604, 61	0,13071	9,305636-03	9921.0	570.00	804-91
	0.94	1,55800E-03 7-84576E-03	1-2829	-9.229426-03	4931.9 -0.41220	5979. 4 9909. 5	515-68 570-00	0. 72575
	1.4000	7.887 (01-03	E07. 64	-5. 81 20				807.86
	2.12 1.4000	2.37198E-C3 7.85353E-03	1.5233 61 c. 90	-7.52060E-02 -10.627	6023.6 -0.75084	6945.2 9889.1	515.26 573.00	0.72883 810.47
••				Version arrows		- 1000		
	1.4000	3.14372E-C3 7.83755E-C3	2.5632 815.35	-4.93351E-02 -15.693	7057.4	6896.3	514.64 570.00	0.73334 815.50
					10.00			
	3.90 1.4000	3.90382E-03 7.75660E-03	3.2271 826,64	-7.42137E-02 -19.011	9929.0 -1.3174	683C.8 9870-5	513.09 570.00	0,74469 826,86
	8.53 1.4000	. 4.65298E-03 7.70454E-03	3. 9552 850.03	-0.11281 -24.244	11061.	6741.4 9962.8	50% 81 570.00	0,76833 850-36
_					12752.	6623.9	505.47	
•	11.73	5.37949F-03 7.635C6E-03	4.7336 879,98	-0.156C3 -29.005	-1.6878	10016.	577.00	0.79891 880.46
•••				-0.21134				
	15.51	6.C7998E-03 7.54962E-03	5.5563 914.01	-34,768	15594. -2.1783	6483.4 10230.	500.36 570.00	914.67
	19.88	6.716465-03	6.3495	-0.25574	17266.	6305.5	495.49	C.86711
	1,4000	7-41461E-03	945.37	-38.077	-2.3065	10296	57C.00	948,14
	24.83	7.254216-03	7,1154	-0.28697	18740.	6058.8	489.79	0. 93489
	1.4000	7.207526-03	980.87	-39.560	-2.3596	10302.	•7C.00	981.86
	30.33	7.757716-03	7. 8620	-0.29412	20113.	3025.3	404.37	C. 94014
	1,4000	7.007136-03	1013.5	-37, 914	-2.1423	10298,	570.00	1014,1
	36.37	6-197C8E-03	8, 5913	-0.22835	21 31 2. -1. 5 2 2 5	5564.5	479.28	0. 97923
	1.4000	6.778756-03	1049.4	-27.692	Control of the	10283.	570.00	104947
,	42.95 1.4000	8-46266F-03	9.2968 1.598.9	-0.26313 -31.095	22150. -1,6708	5210.8 10282.	469.40 570.00	1.0352
		6,467988-03		- • •				1099,4
	50.03 1.4000	4.76805E-03	9. 5838	-0, 32304 -36, 842	23070	4933.9 10294.	461 . 97 570 . 00	1.0013
							•	
•	57.59 1.4000	8.56944E-03 5.94064E-03	10.596 1181.5	-0.45994 -51.284	23728. -2.4455	4624.8 10288.	451.59 57G.00	1.1378 1182.4
	65.56 1.4000	9.03+39E-03 5.61035E-03	11:107	-0.61193 -67.733	24052.	4273.6 10259.	443.82 570.00	1.1923
	73.01	0.724015-03	11.493	-0.55898	23945	3607.7		
•	1.4900	5.215436-03	1297.9	-67,626	-7. 7639	10227,	431.61 570.00	1.2662
<u> </u>	82.40	9,637746-03	11.724	-0,45866	23402.	3407.0	416.42	1.3579
	1.4000	4. 76806E-03	1357.3	-52. 871	-2, 2307	10225.	570.00	1378.3
<u> </u>	91.07	8-435376-03	11.693	7-14958E-02	23028.	3093.5	404459	1.4298
	1.4000	4,411026-03	1469,7	0.4747	0,34445	10160.	570.00	1409,7
	100.00	8.78996E-03	12.408	0.33139	24002.	3029.0	404.02	1.4332
•••	1.4000	4.3668>6-03	1411.6	37.701	1.5299	10100.	570.00	1412.1

	STREAMLINE & CP/CV	DENSITY		W3	FLOW ANGLOS	P-STAT P-57AG	TEMPIR S 7-STAG	MACH N
							•	
	0. <u>0</u> 1.4000	6.93237E-07 6.93237E-03	6.81970E-04 593.75	0.0	1.7913 0.0	5923 <u>.</u> 5	570.00	983.75
	C.26	6.93206E-04 6.86301E-03	0.68981 995,10	6.32568E-03 9.1253	1793.5 0.52540	5743.1 9921.4	487, 57 573,00	0. 91940 995,14
	1,03	1.34168E-03 6.84298E-23	1- 3775 996- 98	7-04318E-03 5-5975	3575.4 C. 29295	5722.7 9908.1	487-26 570-00	0. 921 40 997, 00
	2.10	2.06112E-03 6.80448E-03	2. C624 12C0.6	1.03542E-02 5.0234	5335.8 C. 28745	5685.1 9885.9	486.66 570.00	C. 92534
	4.09	2,72426E-03 6,74783E-03	2.7434	. 1.97523E-02 7-2505	70 57. 5 0. 412 52	5623.7 9854.9	465.59 570.00	0. 93230
	6.39	3. 36960E-03	3.4465	4-87034E-02	6744.0	5534.3	402.40	0.9496
	1.4000	0,67737E-Q3 3.98528E-03	1922-8	0,11705	10375.	9687.9	570.00 472.20	1022,5
	1.400C	6.58141E-03	1649, R	27.613	1.5067	9987.2 5163.4	577.00 477.26	1.029
	12.63 1.4000	6.39749E-03	1094.3	27.591	1.4443	10123-	570.00	1094
·	16-59 1-4000	5.05087E-03 6.25613E-03	5.7634 1149.2	0.10440 20.709	13273. 1.0506	10244	\$70.00	1129.
	21.10 1.4000	5.57541F-03 6.13860E-03	6.4247 1152.3	0.18126 32.511	14674.	4840.2 10299.	459.39 570.00	1.007
· -	26.13 1.4000	6.C4954E-03 5.99464E-03	7.1080 1175.0	0.19899 32.893	15990. 1.6635	4681.3 10301.	455.00 570.00	1.124
2	31.66 3.600C	6.48720E-03 5.84399E-03	7,7712 1197,9	C-1 4030 21.628	17196. 1.0343	451 8.7 10294.	450.52 570.00	1.151
<u>.</u>	37-68	6.89922E-03 5.64726E-03	8.411P 1219.2	C-20234 29-321	1834C. 3.3776	4363.0 10290.	570.00	1:177
	1,4000	7.29106E-03 5.55773E-03	9. C490 1241-1	0.19279	19437.	421 3.4 102 84.	441.73 573.00	1.204
<u> </u>	51.13 1.4000	7.62296E-03	9. 6568 1266.0	0.19468 25.538	1°1244 50 34 5°	4041-1	436.37	1.237
	58-52 1-4000	7.86024E-C3 5.19278E-03	19.198 1297.4	0.21418	21115. 1,2032	3630.9 10287.	429.84 570.00	1.274
7	66.24	7, 96873E-03	1^.634 1334.5	0.22067	21518.	3572.1	421.70	1.326
;	1.4000 - 74.31 1.4000	0.00037E-03	10-592	0.34119 42,646	21726. 1.7779	3303.5 10226.	576.05 412.72	1.30
2	82,6C	4.66350E-23 7.99147E-03		9.30413	21,032.	3644.9	573 <u>,00</u>	1374
	1.4000	4.39940E-03	11.055	38.053	1.5405	10225.	397.82	1415
	1,4000	4,229186-03	192742	52,346	2.0858	10168.	579,00	
l	1,90,60	8,45490E-03	17-172 1437-7	- 0-32509	23184. 1.5299	2857.1	397,36 570,00	1440

5	TREAMLINE 8	DENSITY	n #5	v 13	FLOW ANGEDS	P-STAT P-STAG	TEMPIR) 7-STAG	MACH W
	¢r/ <u></u> y	VE#3111	••••••	······································				YELYYA
	3.4000	5.8064E-07	6.75678E-04 117C.6	<u>0,0</u>	3.5538 0.0	4543.8 9725.9	455 <u>. 95</u> 570 . 00	1,1183
	0.26 1.4000	5.81494E-04 5.81C916-03	C.68816 116944	6,54145E-03 11,134	1554.5 0,5446?	4549.6 9921,4	456.37 570,00	1.3170
	3.03	1.17529E-C3 5.80558E-03	1,3739	1.346P3E-02 11.4:9	31 05. 9	4545.9	456.24 577.00	3.3163
_	2.51 3.4060	1.75477E-03 5.77945E-03	2. C549 1173.0	2. #2632F -02 16.307	4655.5 0.78801	4521.6 9885.8	455.84 370.00	1.31%
	4,10	2.525965-03 5.74106E-03	2. 72.88 1174.2	3,22311E-02 22,484	6141.7	4485.2 9834.8	455-20 570-00	1.1230
_	6.39	2.585196-03	?.4143	8.22797E-02	7634.0	4436.9	453.36	1.1347
	<u> </u>	5.7C229E-03	4,3261	28,318 0.15585	1.3864 9164.3	4414,3	370.00 451.41	1193+! 1195-?
	1.4000	3.6 ÷763E-03	1192.8	45.052	2.3631	4407.8	570.00 449.50	1.137
••	1.4000	5,7154ZE-05	1202-1	51 - 009	2 - 4737	30121.	570,00	1203.
	3.4000	4.6031CE-03 5.68642E-03	5.6033 1217.3	0,23549 46,858	12234.	4357.3 30244.	576.00	
	2C-93 3-9000	5.1294DE-03 5.63149E-03	6.5077 3239,0	0.28993 56,533	13653. 2,6317	4289.6 10298.	443.82 570.00	1.192 1.251.
·•	25.90 3.4000	5.54715E-03'	6.9896 1237.7	0.34797 61.619	15050. 2.8500	4255.4 10301.	570.00	1.202
	31.37 1.4000	6.11100E-03 5,49122E-03	7.6470 1251.2	0.55254 57.682	16318. 2.6596	4141.4 10795.	439.42 570,80	1.210
••••	37.33 1.4000	6.52992E-03	8.2731 1267.0	C.44318	17472. 3.0663	4024.3 16283.	436.01 370.00	1.239
_	42.73 1.4000	6.93748E-03 3,25931E-03	2.8912 1205.2	0.48416	19557. 3.1169	5900.4 10283.	432.10 570.00	3.263
	50.59 1.4000	7.24626E-03	9.4764 1307.8	0.55433 77.050	19499.	3750.3 10294.	427.35 570.00	1.793
	57.67 1.4000	7.52591E-05	10.015 1330.7	0.65473	20514. 3.7404	3593.3 10287.	421,97	1.324
	65.34	4.95873E-33 7.75650E-03	10.5034	0.69849	21012. 3.9042	3426.5	570,00 416,47 570,00	1327. 1.556
	1.4000 75.57	4.79145E-05 8.00524E-05	1334.2 19.687	90.048	21744.	10260.	412.37	1.362
	81.97	4.65605E-03 8.28515E-03	11.515	0,68110	22557 ,	10270, 3190.7	408,44	3,40
	1.4000	4.5492CE-03	1389. 6	82.207	3.3850 23508.	10226e 3157e1	570.00	1392
	1.4000	4.487516-03	1396.4	48, 897	2, 0247	19171,	570,00	1398
	1,90.00	9.06814E-03	32.658		24496. 3.5299	3139.7	40°.22	1.40

_	STREAML INE &		43	W3	14	P-STAT	YEMPER	MACH NO
	CP/CV	DENSITY	y <u>".</u>	y	FLOW ANGIGE	P-STAG	T-STAG	AE FOC Y LA
	0.0	5,358796-07	6, 6570CE-04	0.0	1.4288	4961.1	441.35	1.2060
	1.4000	3. 35879E-03	1242.3	0.0	0.0	9923.9	370.00	1242.3
_	0.23	5.44162E-04	C. 67574	6. 6093EE-03	1450.8	4042.0	441.63	1.2033
	3-4600	3,398965-03	1341.4	12,144	0.56039	992145	579-99	1341.9
•••	1.01 1.4000	1.08693E-03	1241.3	1.74762E-02.	2897.6	190843	441.73 570.00	1-2050
	2.27 1.4000	1.62477E-03 5.33712E-03	?. C101 1242.1	3.71546F-02 22.868	4332.0 1.0547	4044.3 9886.4	441.54 570.00	1.2061
								100
•••	4-07	2,15068E-03	2.6816	6. 91563E-02	5755.7 1. 4773	4029.9	379.00	1,2065 1242.6
_	4,29	2-08810E-C3	3, 3541	9.71344E-02	7172.7	6024.2	44C-30	1.2136
	1.4000	5,29470E-03	1247.6	36.209	1,6622	9884,4	370.00	1248.3
	9.07	3.22241E-03	4.0489	0, 15075	8405.7	3963*0	439.41	1.2241
•	1. 40CG	5.29344E-03	1256.3	46.781	2,1322	9981.5	370.00	1,2251
-	12.37	3.771706-03	4,7684	0.21468	10288.	3980.5	436.70	1.2334
	1-4000	5.31046E-03	1264.2	36.919	2,3779	10113.	572.00	1203.3
	16.23	4,30511E-03	5,4912	0. 23473	11532. 2.6560	3933.6	474,29	1.2500 1276.9
	1.4000	5.3042ZE-03	1275.5	39,169	2. 6560	10240.	373.00	1276.9
_	2C. 39	4.81203E-03	c.1624	0.33579	12907.	3909.3	432.20	1.2626
	1.4000	3-27309F-03	1284.8	69,782	3-1099	10298.	370, 30	1286,7
	23.47	3. 30483E-03 5. 23283E-03	6, 84 93 129Co 2	79.611	14251 a 3 a 5309	3670.1 10302.	430,92 570,00	1.2704
			- T- T- T-	Tr. 1071755			- X	37.797
	30.04 1.4000	5.74646E-03 5.16741E-03	7.4943 1299.4	0.48051 83.326	15501. 3,6986	3663.3 30296,	428.84 570.00	1.2029
•	36,69	0,19192E-03		0. 60372 97. 501	16670.	3721.9 10262.	426,37 570.00	1313.6
-	43.00	6. 55963E-03	0.7255	0.60525	17799.	3638.2	423.61	1.3145
	1.4090	5.00474E-03	1325.1	103,43	4.4905	10242	570.00	
	49.76	6.97541E-C3	9, 3236	0.78553	10062.	3545.2	420.34	1.3342
	1.4000	4.91404E-03	1336-2	112,55	4.8130	10244.	370.00	1340.9
-	36.97	7.364415-03	9, 9162	0.89026	19934.	3470.9	417.67	1,3492
	1.4000	4,83948E-03	1344.5	120.89	3, 1 302	10288.	57C,00	1331,9
	64.62	7.74258E-03	10.311	0. 901 42	21033.	3416.8	416,28	1,3500
	1.4000	4.78233E-03	1354.0	116.12	4.9019	10764.	57C. 00	135%0
	72.73 1.4000	8. 22760E-03	11.133	0.96711	22291.	3409.8	416.44	1.3574
			13,532			10429	57.9.00	1358.3
١	1,4000	4,74544E-03	1352-1	0,79928 91,394	23684, 3,8668	3478.7 10227.	417,13 570,00	1, 3331
_								1200000
,	90.43 1.4000	9.25476E-03 4.40142E-03	12.471 1347.6	0.66091 71.413	25042. 3.0335	3448.1 10173,	41 8. 43 577. QO	1.3456 1349,4
	100,00	5,72869E-Q3	13.581 1344.6	35, 910	26308. 1.5299	3451.6 10100.	419.42 379.00	1,3398

	STREAML INE &	51 2545 154	- b2	W3	#4 #4	P-STAT	TEMP(R)	MACH NO
	CP/GV	DENETTA	<u>u</u>	¥	FLCM ANGION	P-STAG	T-STAG	VELOCITY
	0.0	5-01559E-07	6.50444E-04	C.0	1 . 3472 -	3791.7	430.01	1.2758
	1.4000	5.01559E-03	1296.8	C-3	0.0	9925.9	570.00	1296.8
_	0.25	5.10468E-04	C.66193	6.23231E-03	1371.1	3700.6	410.03	1.2757
	1.4000	3.013916-03	12.99×7	75 209	0.53945	9921,6	572.C0	1296, 8
	C, 99	1.02730E-03	1.3220	1.87694E-02	2740.1	3701.6	430.23	1,2745
	1.4000	5.01323E-03	1295.7	18.396	0.61341	9438.4	570.00	1295.8
-	2.23	1.524886-03	1.4782	3. 64304E-02	4100.6	3493.8	430.23	1.2745
	1,4000	5,00237E-C3	1295.6	25-169	1.1129	9887-1	570.00	1295.9
	3.96	2.0 22236-03	2.6302	7.282416-02	5457.0	3689.5	430,47	1.2731
•••	1.4000	4.99390E-03	1294.3	35. 825	1.5855	9857.1	57C-00	1294.8
	6.19	2,536236-03	3-2901	0-1 0-06	6813.3	367P.0	429.79	1.2772
	1,4000	4.98617E-03	1257.2	41.616	1.8464	986C.7	572.00	1297, 9
	8.91	3.034836-03	3,9678	0.15395	8173.4	3656.3	427.48	1.2887 1306.7
	1.4060	4.97873E-03	1305.7	50.660	2.2219	9476-1	570.96	1306-7
_	12.16	3.547658-03	4.6638	0.22093	9554.4	3641.2	425.83	1.3011
	1,4000	4. 99214E-03	1314.6	62.275	2,7121	10104.	570.90	1336-1
	15.92	4.C4764E-03	5.3657	0-27807	10918.	361 3. 9	423-34	1.3161
•	1.4000	4.97385E-03	1325.6	6R. 700	2,9667	10236.	570.00	1 327. 4
-	20.21	4-32795E-03	6-0398	0.36205	122290	3576.9	421.37	1.3280
	1,4000	4,94590E-03	1333,9	79.959	3.4305	10298.	570.00	1336.3
	24.99	5.0CC51E-03	6.6907	0.46229	13515.	3546.0	420-28	1.334
	1.4000	4.91594E-03	1336.0	92,448	3. 9525	19302.	575,00	1.334
-	30-25	5.453276-03	7.3275	0.54250	14751.	3304.0	419-90	1.3430
	1,4000	4.87371E-03	1343.7	99,481	4.2342	10298,	570.00	1347,4
.	35.99	5.89832E-23	7. 9503	0.67049	15967.	3464.2	417.70	1.3502
	1.4000	4.832216-03	1347.9	117.67	4.8206	10283.	570.00	1352.1
_	42.20	6.3:564E-03	8,5875	0, 75 699	17215.	3438.7	416.86	1.3553
	La 4000	4.80e38E-Q3	1253ak	119.48	5-0500	16560*	570.00	1354.5
<u>.</u>	48.90	6. 82569E-03	9, 23 99	0.84348	18496.	3423.9	416.20	1,3593
	1.4000	4. 793176-03	1353.7	123.57	3.2130	10292.	570.00	1359.
_	56-10	7.342896-03	9.4152	0. 91861	19888.	3443.8	416,93	1.3544
	3,4000	4-81262E-03	1350.3	125.13	5,2943	10269.	579.00	1356.1
	63.41	7.89420E-03	12.614	0.87420	21368.	3487.2	415.47	1.344
	1.4000	4.85306E-03	1343.8	110.68	4.7085	305080	570.00	1348.
	72.05	E. 50575E-G3	11.327	0.88813	22480.	3561.4	421.64	1.326
	1.4000	4.921396-03	1331,0	194.34	\$ <u>,48</u> 34	10530*	572,00	1325,
ł	80-64	9,146868-23	12.084	0.71962	2465%. 3.4081	3637.4	424,22	1,310
	1.4000	4.95586E-03	1321.1	78.674	3.4061	10228.	570,00	1323.
· ·	90.16	4.74031E-03	12.769	0.64197	26220.	3690-1	424.59	1.296
	1,4000	5.0-031F-03	1311-0	65. 908	2.8781	10174.	570, 90	1312,
ı	100.00	1.023848-02	13.386	0.35750	27542.	3693.7	427.62	1.290 1127.
·	1.4000	5.0 32 84E-03	1307.4	34.918	1.5299	10100.	570.00	1307.

STRE	AHLINE &	w1	b2	и3	W4	P-STAY	7EMPERT	MACH NO
	CP/CV	OENSTTY	V	Y	FLOW ANGIDS	P-STAG	T-STAG	AEFOCIIA
	C.O	4,73212F-07 4.73212E-03	4.34993E-04 1341.9	0,0	1.2791	3412,1 9025,9	420.12 572.00	1,3356
	0.24	4.82823E-04 4.72992E-03	0.64748 1341.9	5.49095E-03 11,373	1305.1 0.48558	3410.5 9921.6	420-12 570-00	1.3356
	C. 98 1.4006		1. 2942 1340.4	19.611	2609 <u>.0</u> 0.03605	3413.2	422.37 570.00	1.3341
	7.15 1.40°D	1.445G4E-03 4.72179E-03	1.9369 1340.4	3. 41 507E-02 26.401	3905-2 1-1204	3406.9 9887.0	427.40 570.00	1.3339 1340,6
	3.85 1.4000	1.52279E-03 4.71255E-03	2.5752 1339.3	7. 26135E -02 37. 765	5195.7 1.6151	3401 • 7 9858 • 4	420.57 570.00	1.3320
	6.C7 1.4000	2.400375-03 4.70668E-03	3.2190 1741,4	0.11157 46.480	6488.4 1.9845	3 29 3 • 2 9876 • 7	420. C5 570.00	1.3340 1342.2
	8, 75 1, 400C	2.67593E-03 4.69945E-03	3.0833 1345.2	7-16072 55-864	7702.9 2.3710	3373.2 9970.3	414.21 579.00	1.3471 1350.4
	11.93 1.40CQ	3.35464E-03 6.598775-03	4, 5554 1357, 9	0.22965 60.458	9090.5 2, 2660	3355.0 10094,	416.12 570-00	1.3597 1359,7
	15.61 1.4000	3.030156-03 4.69423E-03	5.2399 1368.1	0-29425 76-826	10395. 3.2142	3333.3 10231.	413.73 570.00	1.3743
	15.01 1.4000	4.29408E-03 4.67812E-03	5.9C10 1374.4	0.37375 87.038	11666. 3,6236	3309.1 10295.	412.16 570.00	1.3039
	24.50 1.4000	4.75880E-03 4.66502E-03	6. 5478 1375. 9	0.47C87 98.948	12932. 4.1132	3296.2 10302.	411,40 570.00	
	25.67 1.4000	5.22539E-03 4,65778E-03	7.1933 1376.6	0.545E6 104.46	14203. 4,3396	3298.4 10259.	411-36	1,3106
	35.34 1.40G0	5.71024F-03 4.66584E-03	7. 8437 1373.6	0.64962	15515	329E.3 10284.	411.87 570.00	1.3955
	41.50 1,4000	6.23574E-G3 4.7033JE-Q3	8.5768 1367.4	0.71236 114.23	1692 0. 4.775 2	3536.1 10279.	413.28 570.00	1.3770
	48.20	6 - 801 09E-03 4 - 7 5 3 3 4E - 03	9.2469 1359.3	0.75129	18641. 4.6454	3 394.3 102 9 1.	415.18	1.3654
	55.44 1.4000	7.42544E-03 4.85394E-03	9.9923 1345.7	C.78217 105.36	20093. 4.4758	3485.2 10290.	416.35	1.3463
	63.25 1.4000	8.07368F-03 4.94785E-03	10.748 1331.2	0.69645 86.262	21798. 3.7076	3502.6 10271.	621.88 570.00	1.3249
	71.63	e. 73640E-03 5.03907E-03	11.485	0.07511	2353Ze 3,4686	3681.1 10231.	425.63 570.00	1.302
8	50,56 1,4000	9,39424E-03 5.112C4E-03	12.239 1304.2	0,56019 59,695	25236. 2.6207	3756.3 10228.	428.13 570.60	1.207
	90.04 1.4000	9.947565-33 5.154365-03	12.921 1293.7	0.56053 58.126	26820. 2.5726	3007.6 10177.	430-41 570-00	1.273
	100.00	1.04963E-C2 5.14609E-03	13,530	0.36156 34.446	26167. 1.5299	3810.6 10100.	431,44 570.00	1.267

	TREAMLINE &	DENSITY DENSITY	is2 U	h3 V	FLOW ANG(D)	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VELOCITY
l	0,C 1.4CC0	4,49170E-C7	6.15758E-C4 1381.7	0.0	1.2163	3162.0	411.C9 570.00	1.3903 1301.7
2	0.24	4.58464E-04	C.62349	4.76824E-03	1246.3	3160.4	411.C7	1.3903
	1.4000	4,47953E-03	1701.0	10,409	0.4 31 26	9921,7	57C-00	1381,8
)	0.94 1.400C	9-16-05E-04 4-48314E-03	1,2655	1.69745E-02 20.701	2491.4 0.65901	3162.6	411.30 572.00	1.3890
	1200		and the same	NE CONTROLLA	207001235	6000 100	.00 11395	
4	2.15	1.372C4E-03 4.47151E-03	1.8940 1360.4	3-85704E-02 28-112	3729.3 1.1667	3156.7 9888.6	411.33 570.00	1.3698
•	3.82	1.02468E-03	2. 51 77	7.2448CE-02	4959.4	3149.4 -	411.40	1.3884
2	1.4000	4.46039E-03	1379.8	39.704	1.6483	9859.7	570.00	1300.4
•	5.95	2.276126-03	3,1466	0.11456	6193.3	3142.7	411.00	1.3904
	1,4000	4-45526E-33	1361.2	50,287	2.0851	9872.5	57C-00	1 382-1
z.	e . 57	2.72228E-03	3.7917 1387.0	0.16403	7435.5	3128.9	409-40 579-00	1.400
	1.4600			And the state of t	10161/002200			
	11.69	3.19227E-03 4,45957E-03	4.4519 1354.6	C.23101 72.367	8696.8 2.9735	31?0.4 10084	407.68 570.00	1.410
•	15.31	3.e5769E-C3	5. 1786	0.29414	9976.4	3114.2	405.82	1.4721
-Z	15.31	4.47111E-03	1402.1	10.417	3.2825	10227.	570.00	1404.
10	19.43	4.12326E-03	5.7912	0.36077	11251.	3115.5	405.17	1.426
	1,4000	4.46025E-03	1404.5	27,498	3. 5648	10289.	579.00	1407,
II	24.05 1.400C	4.60349E-03	6.4516 1401.9	0.44005 95.591	12557.	3135.1	405.76 570.00	1404
	29.10	5.136306-03	7-1257	0.48916	13916.	3172.3	407.15	
12	3,4000	4.53571E-03	1395.5	95.795	3.9270	10299.	570.00	1.414
13	34.12	5.64571E-03	7.0191	0.54939	15363.	3234.1	409.55	1.399
P.A	1.4000	4.601020-03	1345.0	97.312	4.0192	10286.	\$70.00	1366.
14	41.00	6-23676E-03	8.5457	0,5493Y	16935.	3324.0	412.89	1.379
	1.4990		1370.9	91.293	3.8100	10270.	570,00	1373.
15	47,75	4.79503E-03	1336.3	G. 55901	10602. 3.4355	3424.0	416.33 577.00	1.358
	55.07	7.53162E-03	10-085	C-56075	20 356.	1542.1	427.28	1,334
10	1.4000	4.910458-03	1339.1	74.452	3.1623	10290.	570.C0	1341.
17	62.98	6-1-074E-C3	10.642	C.47346	22082.	3640.7	423.81	1.313
¥	1.4000	5.00521E-03	1924.0	57.018	2.5064	10272.	570.00	1375.
1.8	71.44	8.82940E-03	11.963	0.50476	23762.	- 3722.3	424.58	1.294
		5-07936E-03	1369, 9	57,160	2+4996	10232,	570.00	1317,
91	80,44 1,4000	9-43810E-03 5-12791E-03	12.292	0.41659 44.139	25 373. 1.9411	3772.6 10229.	428.66 570.00	<u>1,204</u>
20	89.94	1.001846-02	12,900	0.51718	209710	3010.0	430,40	1,273
-v	1.4000	5,156748-03	1293.6	51.622	2.2852	10177	570.00	1294.
	150.00	1.05266E-CZ	13.575	0. 36254	24240.	3612.0	431.49	1.266

57	REAMLINE &	OENSITY	n n5	43 V	FLOW ANGLOS	P-STAT P-STAG	TEMPLA) T-STAG	MACH NO VELOCITY
						3047.6		
•••••	1.4000	4,36519E-97 4,36519E-03	4-11281E-04 1400-4	0.0 C.0	1.1499 0.0	9925.9	406.78 570.00	1-4164
	004840	4-47139E-04	0.62615	4-44307E-03	1218.6	3046.0	406.77	1.4165
	1,4000	4.15312E-03	1407.4	9. 9815	0,40839	9921.6	570.00	1400.4
	0.95	8-93905E-04	1-2509	1-89420E-02	2436-4	3047.9	405.98	1.4152
	1.4000	4.36347E-03	1399.3	21.190	0.86758	9909.4	570.00	1399.3
	2.13	1-33830E-03	1-6722	3-842308-02	3647.4	3043.0	407-03	1.4149
	1.4000	4,355846-03	1358.9	29.009	1,1879	9849.0	579-00	1399.2
	3.76	1.78004E-03	2.4890	1.203936-02	4851-1	3036.4	407-12	1.4143
	1.4000	4.345555-03	1396.3	40.473	1.6579	9860.3	570.00	1398.9
	5.89	2.22353E-03	3.1169	0.1141	4360aB	3032.5	406.85	1-4160
	1.4000	4.342805-03	1309-1	51.454	5-13-5	9870-4	570-00	1400-0
	8.49	2-675:96-03	3, 75 63	0,14251	1284.2	3024.5	405.48	1.4243
	1.4000	4.34596E-03	1404.4	60.861	2.4411	9961.2	370.00	1405.9
	11.57	3.125:16-03	4,4044	0.22617	8534.0	1024.4	404.11	1.4324
	1-4000	4.36C58E-Q3	147949	72,363	2,9362	10363.	570.00	1411.7
	15-14	3.59197E-03 4.38503E-03	5. C843 1415.5	0,28489 79,313	9816.3	3030.a	402.71 570.00	1.4412
	1.4000							
	19.26	4.06564E-03 4.41187E-03	5.7535 1415.1	0.74132	11111. 3,3951	3049.5 10286.	4C 2-72 570-00	1.4411
				******		**********	,,,,,,	
	23.87	4.56146E-03	1409-1	0.40672 89.164	12455 <u>.</u> 3.6206	3789.5 10301.	570-00	1412.0
	28.99	5. 36752F-03	7-1205	0.42789	13672.	3150-2		1.4191
	1.4000	4.517C9E-03	1399.4	86.071	3.5191	10299.	406.33 570.00	1402.1
	34,64	3.453G7E-03	7,4345	0.47396	15303.	3734.1	409-55	1,3440
···-·	1.4000	4.600996-03	1345.9	83.842	3.4620	10280	972.00	1390.4
	40-45	4-246245-03	6.5805	0.47431	17009.	3340-7	413,43	1.5759
	1.4000	4.7077eE-03	1369-3	75.692	3- 1679	10276.	\$70.00	1371.4
	47.63	6.90603F-03	. 9.3495	0.44797	14703.	3448.9	417.09	1.5539
	1.4000	4.81782E-03	1355.6	64. 8h\$	2.7432	70540*	570.50	1355.4
	54.99	7.56717E-03	17,119	0.44849	20444.	3556.6	423,65	1.3311
	1.4090	4.927145-03	1337.3	59.268	2.5377	10290.	570-00	1338.4
, 	62.93	R. 20604E-03	17.864	0.37401	22127.	5644.8	423.94	1.312
	1.4000	5.009238-03	1 323. 9	45.578	1.9717	10272.	570.00	1324.1
1	71.41	5. 3. 3 148-03	11.572	C.42902	23751.	3717.1	424-65	1.296
• • • • • • • • • • • • • • • • • • • •		5.069466-03.	1231145	48,422	241232	10232,	570,00	7315
2	1.4000	5,47989E-03	12.289	38.476	25309.	3750.0	427-92	1.200
	- 200-			- A	770	10229.	579.00	1306.
•	89.97 1.4COO	5.57607E-03 5.1282E-03	12.950 1298,1	C.49629 49,146	24904	3790.6 10177.	429.53	1.276
					2-166]		570-00	1799,
L	1.4000	1.04612E-02 5.1145CE-03	13.563	0.35224 34.561	20143a 1.5299	3782-0	437.51 570.00	1.272

57	REAMLINE &	61	W2 /	H3	W4	P-STAT	TEMPIAL	MACH NO
••••	CP/CY	DENSITY	y	Y	FLOW ANGIDS	P-STA0	T-STAG	AEFOCITA
ı	0_0	4.25452E-07	6-03323E-04	C. 0	1-1628	2939.9	402,62	1-4418
	1.4000	4.25452E-03	1416.1	0.0	0.0	9925.9	57C. 00	1416.1
	0.23	4.36375E-04	0.61981	4. 18243E-03	1192.6	2938.5	407.61	1,4416
		4.272575-07.	1515.2	9,5045	QA38724	9921-8	570-00	1414-1
<u> </u>	0,94	8.77411E-04	1.2362	1.87712E-02 21.516	2394.0	2940.4	402.82	1,4405
	1.4000	4.252998-03	1417.0	21.516	0.84992	9909.6	570.00	1417.2
,	2.11	1.306476-03	1.8508	7.47e28E-02	3570.4	2937.3	402.94	1.4398
	3,4000	4.247366-03	1416.4	29.665	1.1998	9889.4	570,00	1416.7
	3.74	1.73894E-03	2-4613	7. CP940E-02	4751-1	2933.3	403,11 570.00	1.4367
	1.4000	4.239696-03	1415.4	40.770	1.6499	9861.0		
	5.84	2.17446E-03	3-0774	0. 1 12 50	5941.2	2934.1	403.04	1.4391
• • • • • • • • • • • • • • • • • • • •	3,40 <u>0C</u>	4, 241 43[-03	1417.7	51.737	2.0936	9867.4	570,00	1414,2
<u> </u>		2,616065-03	3,7131	0.15786	7152.4	2934.1	462.02	1.4454
	1.4000	4.25247E-03	1419.3	6). 342	2.4344	9954.3	570.00	1450.6
	11.47	3. 07049E-03	4.3684	0.21637	8399.6	2945.3	401.11	1.4509
	1-4000	4,278225-03	142247	70,467	2.8356	10075,	570,00	1424.4
	15.03	3.54222E-03	5.0508	0.26906	9695.1	2967.0	400.29	1.4560
	1-400C	4.3184%-03	1425.9	75.675	3.0379	10223.	570.00	1427.
,	19.11	4.02827E-03	5.7304	0.31170	11020.	3005.0	401-06	1.4513
	1,4000	4-34560E-03	1422,4	77,378	3-1135	10284.	570.00	1424,7
l	23.72	4, 542 80E-03	6,4209	C. 36771	12411.	3044,2	403,19	1.4383
	1.4000	4.43094E-03	1413,4	79.402	3, 21 53	teloi.	370.00	1415.7
2	28.85	5. 091 76E-03	7,1319	0. 37273	13884.	3146.1	405.25	1.4196
	3+4000	4,51494E-03	1400.7	73, 203	2.9917	10259.	570-00	1402,4
3	34,52	5.677736-03	7. 8614	0.36471	15445.	3247.0	410.04	1,3966
	1.4000	4.61502€-03	1364.6	68.110	7.8142	10500-	\$70.00	1386.3
4	40.76	0. 30176E-03	8.6143	0.37312	17094.	3361.1	414,17	1.3715
	1.4000	4,728256-03	1367.0	54.509	2.4802	10278.	570,00	1769,2
5	47.57	6.53849E-03	9-3606	0.34004	18764.	3465.3	417.66	1.3505
	1.4000	4. 834166-03	1352.0	49.006	Z. D740	10240.	570.00	1352.
6	54,97	7.502478-03	10,140	0.34797	20484.	3562.5	420.99	1.3304
	1,4000	4.93068E-03	1337,3	47.872	1.9655	10290.	570.00	1376-1
Z	62,92	8.19646E-03	10,849	0.29071	22107.	3632.1	423.52	1.3150
	1.4000	4.996816-03	1326.1	35.467	7. 2250	10272.	570,00	1326.6
	71.41	8.756196-03	11.545	0.36964	23674.	3485.6	425.77	1.3014
	1.4000	5,04359E-03	1315a7,	41,930	140257	105)2,	570-00	1316.3
9	80,44	9.355838-03	12.271	0.31880	25183,	3713-0	424,71	1,2950
	1.4000	5.069576-03	1311.6	34.075	1.4882	10229.	570.00	1312.1
e	89.98	9.50530E-03	12.927	0,46699	266450	3737.8	428.14	1.2071
	1,4000	5,06673E-03	1304.4	47.171	2,0489	10177,	579,00	1305.5
u	100-00	1.C4093E-02	13.530	0.36157	27975. 1.5299	3738.9	429.11	1.2813
	1.4000	5.076748-03	1300-6	34. 735		10100.	570.00	

	STREAMLINE & CP/CV	DENSITY	Ú Ž	W3	FLOW ANGIOS	P-STAT P-STAG	TEMPIR) T-STAG	WACH N
			**					
	1.4000	4.05578E-07	5. 861 G4E-04 1450. 0	0.0	1-1134	2749,5 9925,9	394.99 570.00	1.4484
- 11	C.23	4.17090E-04	C.60479	3.567238-03	1145.4	2746,3	394,98	1,4884
	<u> </u>	4,05405E-03	145C. 0	4.5527	0,33794	9021,0	570,00	1450,1
3	9.92	8.34246E-04	1.2086	1.757508-02	2299-5	2751.8	395, 26	1,4867
	1.4000	8.34246E-04 4.05633E-03	1446.7	21.067	0.63311	9909.9	570.00	1440. 9
4	2.06	1.251 44E-03	1-6113	3. 65683E-02	34 36.2	2756.1	395.67	1.4843
	1,4000	4.05851E-03	1646, 9	29.212	1.1566	9890.1	579.00	1447.2
5,	3-67	1.67C55E-07 4.06232E-03	2. 4127 1444. 2	6.45CD8E-02	4543.8	2742.8	396.26 577.00	1.4804
	DESCRIPTION OF THE PERSON OF T		The second second	No respectively	100000000000000000000000000000000000000	100000	and the second	
	5.73 1.4000	2.09744E-03 4.08052E-03	3.0228 1441.2	0.10092 48.117	5752.8 1.9122	2779.9 9844.7	396.93 570.00	1,4765
7	8.27	2.5384CE-03	3.6545	0.13608	6962.5	2903.2	396.86	1.4769
	1.4000	4.11547E-03	141.3	53.610	2.1302	9953-5	396.86 570.00	1447.
	11.30	3.00182E-C3	4, 3215	C. 17802	6231.9	2843.9	397.20	1.474
	1,4000	4,17164E-03	1439,6	59,302	2.3548	10066.	570,09	1440.4
9	14,84	3,49493E-C3	5- C220	0.20855	9180.3	2901.9	3 97, 94	1.4710
	1.4000	4.2498E-03	1436- 9	59.671	2. 3779	102160	570.00	1456.7
10	18.93	4.01910E-03 4.3378ZE-03	5. 7295 1427. T	0.22115 55.106	10985. 2.2104	2978.6 10241.	400.08 579.00	1,457;
	879						-,,	
11	23.55 1.4000	4.56396E-03	6.4503 1413.3	0.23491 51.471	2.0457	3975-0 10301-	570.00	1414.
12	20.73	5.144CBE-03	7.1845	0.21436	14016.	3181.8	467,49	1,412
	3.4000	4,54944E-03	1396.7	41,676	1.7092	10299.	£70.00	1397.
13	34.46	5.74300E-03	7. 9220	0. 20106	15608.	3280.2	411,49	1.387
	1.4000	4,45590E-03	1379.6	35.010	1. 4537	10287.	570.00	138C.
14	40.76 1.4000	4.35468E-03	8.6662	0. 1 8360 20. 092	17231. 1.2137	3388.3	415.13	1.365
		4.755536-03	1363.7		und floor	10278.	577.00	1364.
15	47.62 1.4000	6.95637E-03 4.63399E-03	9.4098 1352.7	0.16152 23.219	15832. C. 48337	7465.1 10290.	417.65 570.00	1,350
16	55.04	7.55102E-03	10,140	0.19789	20414.	3528.9	419,44	1.337
	1.4000	4. 897426-03	1342.9	26.207	1.1180	10290.	570.00	13424
17_	63.01	8.11409E-03	19.841	0.17394	21915.	3560.1	421.38	1.328
	1.4000	4.933725-03	1936.1	21.437	21915. 0.41920	10272	570-00	1336.
10	71.49	8, 46665E-93	11.517	0.28676	23384.	3690.2	422.93	1.310
******	<u> </u>	4,959735-03	1329.0	33,084	3.4264	10231,	570,90	1,729,
.12.	1.4000	9,19952E-03 4,97222E-03	1326.0	9.75907 28.161	24814,	3613.3 10229.	423,40 570,00	1.315
-				0-42999		3629.3		
20	90.01 1.4000	9.72723E-93 4.98075E-93	12.851	44.205	26218. 1.9164	10177.	424.55 570.00	1.308
	100.00	1.021015-02		0, 35945		3629.8	425,49	
? }_	1.4000	4.9705LE-C3		35,178	27525 ₀ 1.5299	10100.	570-00	1,303

CP/CV			٧	FLOW ANGION	B-ETAC	T-CTAC	MACH NO
	DEVILLA	······································			P-STAG	T-STAG	VELOC171
0.0	3.90173E-C7	5.75496F-04	C-0	1.0755	2604.4	368.92	1.5258
1.+000	3.901735-03	1475.0	0.0	0.0	9925.9	570.00	1475-0
0.21	4.D2210F-04	C.55339	2.61632E-03	1109.C	2633.4	388.92	1.5258
1.4000	1,905216-03	14.75.0	6,5035	0.25267	9922.0	570-00	1475.0
6.95	8.05717E-04	1-1468	1.441 44E-02	2720.3	2611,4 4910-2	389, 39	1.5729
1.4000	3.90742E-03	14 72. 9	17.890	0.69567	4410.2	570.00	1473.0
2.03	1.2:327E-G3	1.7823	2.96515E-C2	3341.5	2628.3	390.33	1.5171
1.4700	3-923236-03	1469-0	24,439	0.95312	9890.6	570-00	1469.2
7.62	1.62738E-C3	2.3812	4.94445E-07	4478-1	2653.6	391.71	1.5086
1.4000	3.94704E-03	1463.2	30.363	1.1855	9963-1	570.00	1463.6
5. 46	2.05687E-C3	2. 9945	7-48710E-32	5653.7	2695.3	393.47	1.4978
1.5000	3,99117E-C3	1455.9	36,400	1.4372	9862.4	570-00	1456.3
8.19	2.50972E-03	3.0411	9.30954E-02	4693.7	2749.2	304.69	1.4502
1.4000	4.05837E-03	145C.8	37.094	1.4646	9950.8	570.00	1491.3
11.22	2.5°360E-03	4.3219	9.11126	8213,5	2827-0	396.40	1.4798
1,4000	4, 14534E-03	1443.7	37.167	1.4747	10045.	579.00	1444.2
14.79	3.51363E-C3	5.0450	0.11482	9628.7	2913.2	396.31	1.4681
1.4000	4. 261 486 - 03	1435.0	32.678	1.3037	10213.	570.00	1436.2
14.90	4.0587JE-03	5.7743	9.708078-02	11100.	3015.2	401.48	1.4487
1,4000	4.37571E-03	1 422 . 7	23,919	0.96320	10261.	570-00	1422.9
23.58	4.62591E-C3	6.507C	8.57123E-C2	12621.	3122.1	405.28	1.4255
1.400C	4.488528-03	1406.6	18.529	0.75468	10101.	570.00	1-06-0
24.61	5. 20407E-03	7-2384	5-42944E-02	14166.	3222-1	409.96	1,4032
1,4000	4.59051E-03	1390-9	10.+31	0.42968	10299.	570-C0	1391.0
34.60	5.77973E-09	7- 9-01	4.277611-02	15702.	3305-6	412.11 570.00	1.3840
1.4000	4.67347E-03	1377.2	7.3889	0.30739	10286.	570.00	1377.3
40.93	6.35186E-03	8.6784	4.600906-02	17229.	3373.8	414,62	1.3689
1•40C0	4.74134E-03	1346.3	7,2434	0.30375	10270.	573-00	1366,3
47.81	6.907466-03	9, 3944	4-82169E-02	18719.	3410.5	416.04	1.3603
1.4000	4.747496-03	1360-0	6. 4854	0.29407	fc 500°	570-00	1340-1
55.23	7.45711E-03	15.099	0.11151	23192.	3455.0	417.31	1. 3524
1,4000	4-823918-03	1354.3	14,953	0.63257	16500	570.00	1,354.4
63-17	7.98129E-03	13.778	0.10862	21 690.	3474.0	418-18	1.3471
1.4000	4.840 33E - 03	1350-5	13.609	0.57737	10271.	570, 00	1350.5
/1-63	8.504051-03	11-440	0-24053	22 998.	3-73-2	419.30	1.340
]-40ÇQ	4,85407E-03	1345.2	26,244	3 20 45	10231	570,00	1345,
80.60	9,012906-03	12:117	0.22408	24371.	3498.3	419,51	1.339
1.4000	4.85866E-03	1344.4	24-662	1.0595	10228.	570.00	1344.
90.06	7.51942E-03	12,753	0.40312	25725.	2508.4	620.47	1.333
1,4000	4.86164E-03	1339.7	42.147	1.0125	10177,	570,00	1340,
	9,999406-03		0.15672 35.674	27006.	35CP7	421.39	1.327

STREAML INE &	DENS17Y	b2 U	h3	FLOW ANGIOL	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VELOCITY
1.4000	3.84935E-07 3.84935E-03	5.71047E-04 1462.5	0.0 0.0	1.0625	2555.6	365-82 570-00	1.5386
1.4000	3-97430E-04 3-84790E-03	0.50959	1.90727E-03	1297.0 0.18535	2554.6	386.82 573.00	1.5307 1403,5
A49049	7-967215-04	1.1799	1.177326-02	2198.2	2566.0	387.44	1.5349
1.4000	3.458786-03	1466.9	14,777	0.57171	9910.3	570.00	1491.6
2.03 1.4000	1.20255E-03 3.88350E-03	1.7744	2.371 C9E-02 19.717	3315.2 G. 76557	7591.1 9890.7	388.74 570.00	1.5269 1475,7
3.61	1.61826E-03	2. 3753	3-756266-02	4456.0	2628.0	392.62	1 - 5153
	3.919826-03	1467.8	23.212	C-93601	9863.3	570.00	1468-0
1.400G	2.05323E-03 3.57892E-03	2.9537 1458.0	3.51667E-02 26,86F	5645.4 1.0557	2683.8	392 . 99 570 . 00	1 • 5007 1 • 58- 3
7 8.16 1.4000	2.51547E-03 4.06239E-03	3-64-84	6.27574E-02 24.960	6974.3	2753.0 995C.6	394.65	1.4893
11,22	3.01079E-03	4. 3389	6.79393E-02		2840.5	357.10	1.4755
1,4000	4-167798-03	14411 5. C705	5.682226-02	0.89705	10765. 2940.0	570.00 399.34	1.461
1-4000	3.24133F-C3 4.28951E-03	1431.0	16.610	0.66465	10514	573.20	1431.
18-94	4.09198E-03 4.40583E-03	5. dC34 1418.2	3. 046 76E -02 7. 4457	11184. c. 30080	3044.2 10782.	402.57 570.00	1.4420 1416,3
1 23.66 1.4C00	4.65589E-03 4.51174E-03	6.5330 14C3.2	1.45797E-02 3.1315	12697. 0.12707	3144.8	406.12 570.00	1.4205
2 28.92	5.22175E-03 4.60017E-03	7. 2555 1389.5	-1.29297E-32 -2.4761	14211. -0.10210	3231.5 10299.	469.30 570.00	1.4011 1389.5
334.72	5.77143E-03	7.9646 1376.3	-1.61244E-02 -2.7904	15701. -0.11599	3298.6 10256.	411.97 570,00	1.3655
4 41.06 1.400	6.32916E-03 4.71796E-03	6.4701	4. 1406E-05		335C.8 10276.	413.81 573.00	1.3730
5 47.93 1.4060	6. 86456F-03 4. 75158E-03	9.3741	1.29A21E-02	_	3382.6	414.78 572.60	1.3679 1365.6
4 55.34	7.3966/6-03	12.069	1.55425E-02		3409.7	415.74	1.7621
1.4000		1361.3	11,572	0.48703	10293,	572.00	13:1,4
763.27 1.4000	7.9C612E-03	10.749 1359.4	8.86618E-02	21421 <u>.</u> 0.47299	3422.1 10271.	41 A. 39 570.00	1.3581 1358.5
15 71-71 1-4000	8.41717E-03	11.396	0.22589 26,837	22791. 1.1356	2437.1 10231.	417.37 570.00	1.2522
10 00.65	8.91619E-03	12.067	23.563	24140. 1.0101	3439.4	417.49	1.3515
90.09	5.41314E-C3	12.594	6.34565	25472.	3447.6	418.36	1.3461
1.4000	4,801226-03	1349.0	41.709	1.770)	10176.	572.00	1349,7
100.0Ç 1.4C00	9.88785E-C3 4.79110E-C3	13.301	0.35523 35.926	26741a 1.5299	3447.7 10100.	419.28 570.00	1.3407

5	TREAPLINE &	DENSITY	n.2	W3	FLOW ANGEDI	P-5147 P-5146	TEMPIRI T-ST46	WELOCITY
			5.684286-04			2527.4	345.59	
	0.0 1.4000	3.81894E-07 3.81894E-03	1488.4	0.0	0.0549	9925.9	570.00	1.5463
_			C- 5 F764	9-83315E-C4	1090-5	2526.5	365-60	1.5463
	1.400	3.94419E-C4 3.4175TE-C3	1488.4	2.4906	9.58741E-02	9455-0	570-00	1486.4
	0.9C	7.92372E-04 3.832745-23	1.1748	8.24483E-03 10.405	Z187.6	2541.8	386.39	1.5414
	1.4000	3-035 142-33	1403-6	10.403	60-0141	771 703	317600	
	2.02	1-199C6E-03	1.7726	1.577231-02	3307.0	2575.9	368-09	1.5309
	1-4000	3-86726E-33	1476.3	13-154	0.50980	9890-7	570.00	1476.3
	3-61	1.61902E-03	2.3775	2.236276-02	4458.5	2624.9	392.49	1.5161
	1.4000	3.91658E-03	1468.5	13.612	0.53491	9863.3	570.00	1468.5
_	5.66	2-761-06-03	3-CC26	3-08271 E-CZ	5666-9	2694.2	393-42	1-4980
	1-4000	3.98795E-23	1456.4	14.953	C.58823	9562.2	57C.00	1456.5
		1 3030-03	3 4443	2.7191CF-02	6954.9	2774.2	395.79	1 - 4835
	1.4000	2.53392E-03 4.08658E-03	3.6657	10.731	0.4 2499	9951.3	577.00	14460Y
		110000000000000000000000000000000000000				1200	all and the same of the same o	
	11.27 1.4000	3.03476E-03	4.3641	2.01348E-02 5.6256		2872.4 10067.	399.34 570.00	1.4679
		4,20133E-03	1436.1		0-26434			
	14-55	3.57°36E-03	5-1004	1.070776-03	9783.7	2973.8	470, 61	1.4540
	1.4000	4.32511E-03	1426.5	V-58830	1.151938-02	10217.	570.00	1426.5
	19.05	4-1 2467E-03	5. 8314	-3-30626E-02		3072.3	403.62	1.4350
	1.4000	4.43527E-03	1413.8	-8-0158	-0,32485	10243-	570.00	1413.8
	23.78	4,678556-03	6.5531	-4.78698E-02	12754.	3167.5	406-49	1-4149
	1.4000	4.52782E-03	14CC. 7	-10.232	-0.41853	10301.	5 70.00	1400. Y
	29.05	5-22775E-03	7-2540	-6-72414E-CZ	142284	3230.4	409-28	1.4012
	1,4900	4,599446-03	1389.5	-12,863	-0,53038	10299.	570.00	1389,4
			7-5604	050005-05	15669.	3281-6	4.0.0.00	
- -	34-86	5.76457F - 23 4.44912E - 23	136G. 9	-6.05800E-02	-0.43602	10285	411.26 577.00	1,3992
	41.20	6.29576F-03	8-6544	-3.27113E-02		3327.0	412.71 570.00	1.3804
	1.4000	4-68697F-03	1374.4	-5-1958	-0.21656		217.09	1375,1
	48,07	6- 113966-03	9.3482	-1 - 1 8529E -02		3241.6	413,34	1.3766
	1.4000	4.71044E-03	1371.0	-1.7395	-7.26479E-02	102-1.	372.00	1371.9
_	55.47	7.331441-05	10-035	6.76131E-02		3361.6	414.05	1.3723
. 	1.4000	4.730316-03	1368.7	0.2223	0.38604	10290.	579.00	136P. (
	63.38	7.82858E-03	10-498	7.446546-02	21 235.	3369.2	414.55	1.3693
	1.4000	4. T3549E-03	1360.6	9.5120	0.39860	10270.	570.00	1346.6
	71.79	8.327361-03	11.349	C-21523	- 220ale	3340.9	415-41	1.3441
	1,4000	4.741966-03	1342.6	25.040	1.0864	10231.	570,00	1362.
				. 20444	23910.	3361.4	415-46	1.3631
	1.4000	#. #1963E-03 4.74214E-03	12.016	0.20444 23.150	23910. 0.91477	10228.	570.00	1362.0
	90.12	9.3C112E-73	12.643	0.38370	25221.	3507.6	41 6-29	1.35
•	3-4000	4.74140E-03	1 358.3	41.232	1.7383	10176-	570.00	3356-9
	100-00	9.77127E-03	13.243	0.35369	26477. 1.5299	3197.7	417-18	1.353
	1.4000	4.73136E-03	1354.5	36-175	1.5299	10100.	570.00	1355

	STREAMLINE & CP/CV	DENSITY	#2 U	V N3	FLOW ANGEDS	P-STAT P-STAG	TEMP(#) T-STAG	WACH NO VELUCITY
	277-23	3-81559F-C7	5. 681 37E-04	0.0	1.0540	2524.3	301-46	1.5472
X	1.4000	3. 81558E-C3	1489.0	0. 0	0.0	9925.9	370.00	1489.0
2	0.22 1.4000	3.94982E-04 3.81430F-03	0.50011	-1.96425E-04 -0.49720	1091.1 -1.913646-02	2523.5	345.47 570.00	1.5471
		7.9364cE-04	7.1786	3. 72699E-03	-	2547.9	386.44	
A	1.4000	3.02393E-03	148% 0	4. 6959	2191.1 0.18118	9910.3	570.00	1.5411
4	2.03	1.233985-03	1.7778	5.691 12E-63	3319.6	2546.0	300.52	1.5282
	1,4000	3.07acet-03	1476,4	4,7271	0.18343	9890.7	570.00	1476-6
5	3.62 1.4000	1.63057E-03	2.3854	3.8°740F-03 2.3458	4497.6 9.25367E-02	7646•2 9863•0	391.40 570.00	1.5105
•	5.69	2.08179E-C3	3- 02 20	2.41810E-03	5717.7	2726.1	394.74	1-4-00
	1.4600	4,02382E-03	1451.1	1-1616	4.596406-02	9863.2	570-90	1451-1
7	1.4660	2.56315E-03 4.12866E-03	3.6912 1440.1	-1.2C989E-02	7C 29.1 -0.18780	2815.R 9957.0	397, 38 570, 90	1.4730 1440.)
8	11.34	3.07432E-C3	4.3943	-2.97612E-52	8416.3	2917.6	399.93	1.450
	1.4000	4-244716-03	1429.4	-9,4529	-0.37891	10070.		1427-
9	1.4000	3.61084E-C3 4.36235E-03	5.1307 1420.9	-5.43 359E-02 -1 5. 940	9872.7 -0.60642	3004.3 10221.	401, 43 570, 00	1 4 21.
0	19.18	4.15249E-03 4.45939E-03	5.8551 1410.1	-8.91250E-02 -21,464	11335.	3095.6 10285.	404. 47 570. 00	1.430 1430.
 -			-	-9. 85697 E-02	*****************	3167.0	406.93	1.415
1	1.4000	4.65154E-03 4.53452E-03	6,5660 1349,5	-21.010	12767. -C.86007	10301.	\$70.00	1 399.
2	29.21	5.222425-03	7.2646	-0.10801	14217.	3220.4	408.90	1.403
	1.4000	4.58880E-03	1391.0	-20,683	-0.85185	10299.	570.60	
3	35.07	5.74044E-03	7, 54.92	-9-20864E-02	15612. -0.86371	3756.5	410.37	1.394
	41.36	6-25-69E-03	8.6332	-5-4 8061 E-02	17000	3263.7	411.42	1.300
4	1,4000	4,65037F-03	1340.3	-8. 7624	-0.26372	10279	572,00	1380.
	40.22	6.7544F-03	9- 31 83	-2.8491 0E-02	18365.*	2297.6	411.77	1.386
	1.4000	4.06605E-03	1378,6	-4.2156	-0.17510	10291.	576.00	1370.
6	55.60	7.263648-03	5.9577	5.563356-07	19731.	1312.2	412.31	1.302
	1,4000	4.650538-03	1376.4	7.6541	0,31083	10290.	572, CO	1 376,
7_	63-49	7.75020F-03	19.655	6.47091E-02	21049.	3?16.1	417.68	1.360
	1.4000	4,691926-03	1374.6	8,3493	0.34796	10270.	57n.00	1374
10	71-68	8.24\tlt-C3	11.301 1371.2	0.20762 23.191	22372. 1.0525	3375.2	413-45 570-00	1.376
								1371
l¶	1.4000	8,72417E-03 4,61474E-93	11.963	0.19853 22.756	236el, 0.95274	3324.3 10228.	417.45 570.00	1.376
20	90.15	9.20465E-03	12.507	0-37610	24973.	3329.0	414.22	1.37
- -	1,4900	4,632628-03	1367.4	4C-860	1.7115	10176.	570,00	1368

s	TREAMLINE E CP/CV	W1 DEMSI7Y	W2 U	, y	FLOW ANG(D)	P-STAT P-STAG	YEMPIRI 7-STAG	VELOC17Y
	0.0 1.4000	3.84490E-07	5.70666E-04	0.0	1.0614	2551,4	386.64 570.00	1.5399
_	0.23	3.98542E-04	0.54150	-1.650578-03	1100.1	2550. Y	326.65	1.5394
	1.4000	3, 84 3 70E - Q3	1484,2	-4, 1614	-0.16066	9922-0	572,00	1484,2
•	1.4000	3.84717E-03	1479,6	-1.82243E-03 -2.2739	2211.1 -8.80527E-02	2573.8 991d.1	387.78 570.00	1.5328
	2.05 1.4000	1.21829E-03 3.91909E-03	1.7907	-6.48202E-03 -5.3206	3355.6 -0.20740	2624.4 9896.4	39^.17 =70.00	1.5181 1469.9
	3.65	1.65297F-03 3.98836E-03	2.4080 1456.7	-1.74965E-02 -10.579	4543.9 -0.41607	2692.6	393.35 570.00	1.4485
	5.74	2.112438-03	3. G471	-2.875276-02	5794.8	2777.6	396.83	1.4773
	1-4000	4-07816E-03	1447.3	-13.610	-0.54764	9865.0	572.CO	1442.4
	1.4000	2.60924E-03 4.18302E-03	3.7221 1491.4	-5.25414E-02 -20.206	-0.60675	9955.6	399.42	
	11.45	3.11273E-03 4.29214E-03	4.4262 1422.0	-7.61156E-02 -24.453	8512.3 -0.98520	2958.8 10374.	401.65 570.00	1.4477
	15-11	3.64372E-03 4.39641E-03	5.1590	-0.1030e -25.291	9955.0 -1.1440	3041.9 10224.	403.14 575.00	1.4384
					_	3110.0	405.Cl	
	19.33	4.1727CE-03 4.47531E-03	5.6732 1407,5	-0.13451 -32.236	11367. -1.3129	10287.	570.00	1.4272 1407. q
	24.10 1.4000	4.69475E-03 4.53175E-03	4.5718 1399.8	-0.13648 -29.070	12797. -1.1697	3164.3 103dl.	406.83 570.00	1.4161 1400. Y
	29.39 3.4000	5.20765E-C3 4.56990E-03	7,2587 1393,9	-0.13624 -26.161	14162.	9201.9 10299.	409.23 570.00	1.4074 1394,1
	35 <u>+ 20</u> 1•400	5.7C89CE-03	7.5327 [369.5	-0.11286 -19.768	15537. -0.61506	3225.7	407.26 570.00	1.4014 1364.4
-	41.53	4,20875E-03 4,61024E-03	8.6082 1386.5	-6.86681E-02 -11.060	16690. -0.45704	3244.1 10279.	409.99 570.00	1.3964
	48.37	6.70037E-03	9.2858 [38k.9	-3.9C40CE-02	18226.	3252.0 10242	410.13 570.00	1.396
	55.74	7.19496E-03	4,4587	4.81545E-02	19566.	3262.3	410.53	1.3930
	43,61	4,63925E-33 7.67209E-03	1364,1	6. 6928 5. 83095E-02	0,27705 20860	3267.5	570.00 410.80	1,397(1,397(13,054)
-	1.4000 71.97	4.62873E-03	1382.9	7.6002 0.20238	0.31487 22164.	10269. 3270.6	470-00 411-50	1383,0
	070¢a1	4.63051E-03	1379.7	0,19446	1.C304 23456s	3268,5	570,00 411,45	1,380,1
	1.4000	4.62845E-03	1380.0	22.531	0.93541	10228.	570.00	138C-1
	90.18 1.4000	9.10356F-33 4.62520E-03	12.530 1374.4	0.36967 40.607	24731. 1.4899	32 7 2 • 0 10 1 7 6 •	412-18 570-00	1.263 1377.
	100.00	9.56221E-03	13,126 1372.6	0.35055 36.660	25962.	7272.0 10100.	413.06 570.00	1.378

	ITERAT	104 NO 300	-STATION NO 4	3 A-T NUER -	0.000¥	-OUTER - 2.0172	GUYPUT NO.	3
	STREAMLINE & CP/CV	DENSITY	n F5	yrs Y	FLOW ANGLO	P-STAT P-STAG	TEMP(R) T-STAG	MACH NO VELOCITY
	0.0 1.40C0	4.02110E-07 4.02110E-03	5.45727F-04 1455.6	0.0	1,1052 0,0	2716.6 9925.0	393.63 570.00	1.4967 1455.6
	C. 23 1. +000	4.17901E-04 4.02002E-23	C.6CA25 1452.9	-5.25836E-03 -12,583	1140.6 -0.49531	2716-1 9921-8	393.66 570.00	1.4966 1455, 5
	1.4000	8,40343E-04 4,04380E-03	1.2192 1450.8	-1-52139£-02 -18-104	2308.0 -0.71493	2739.9 9909.6	394.78 570.00	1 - 4897
	2-11 1,4000	1-216375-93 4-095326-33	1.6392	-3.45754E-02 -27.089	3500.4 -1.0778	2791.2 9889.3	397.11 570.00	1.4754
	3.76 1.4000	1.72757E-03 4.15760E-03	2,4683 1428-8	-6.29755E-02 -36.355	47 29.3 -1. 4576	2854,1 9860,4	399.98 572.00	1.4579
_	5.90 1.4000	2.19715E-03 4.23036E-03	3.1146 1417.6	-8.89978E-02 -40,506	6704.9 -1.6367	2923.1 9870.6	402.60 570.00	1.4419
	6.55 1.4000	2.68465E-03 4.30764E-03	3.78 9 2	-C-12269 -45-700	7370.7 -1.8545	2987,0 9963.3		1.4333
_	11.72 1.4000	3.18479E-03 4,38021E-03	4.4851 1408.3	-0.14880 -46.721	8692.4 -1.7001	3042.7 10086.	404.74 570.00	1.4288 1409.1
	15,44 1-4000	3.69210E-03	5,1991 14 Ca,1	-0.16935 -45.866	10077.	3086.9 10229.	404.78 570.00	1.4286
_	19.69	4.18587E-03 4.48212E-03	5. £930 140e.5	-0.18854 -45,000	11433. -1.6325	3114.9 10293.	405-17 570-00	1,4262 1407.2
	24,47 1,4000	4.67816E-03	6.5677 1403.9	-0.17643 -37,713	12740. -1.5386	1137.2 10302.	405.83 570.00	1.4222
_	29.77 1,4009	5-1:984E-03 4-51626E-03	7.2341 1402.0	-0.16204 -31,407	14769. -1,2633	3149.4 10299.	406-31 570-00	1.4193
-	35.57 1.4000	5.43363E-03 4.52023E-03	7, 8904 1400-5	-0.13039 -23.143	15358. -0.94470	3155.1 10244.	404.69 570.00	1.4170 1400.7
	41.88 1,4000	6.11755E-03 4.5256ZE-03	8,5520 1399,5	-7.80466E-02 -12.871	16655. -0.52689	3160.9 10280 _e	405.95 570.00	1.4154
<u>.</u>	48,69 3,4000	6.50206E-03 4.52645E-03	9.2167 1400.3	-4.6 94 8 7 E -03	17942. -0.24185	3160.4 10292.	405.79 570.00	1.4164
	56.02 1.4000	7.05453E-03 4.53073E-03	4,8780 1 394,4	4.31069E-02 6,1071	19236. 0.25003	3164.9 10289.	406. 98 579.00	1.4132 1394.5
<u>.</u> _	63-84 1-4000	7,51930E-03 4,52485E-03	17.519	5.32575E-02 7.0826	20492 . 0.29009	3161.6 10268.	407-11 570-00	1398,3
•	72.15 1.900Q	7.94761E-03 4.52393E-03	11-153 1396 ₄ 3	0-19742 24-714	21761°. 149 <u>1</u> 49	3165,4 10230,	407.47 573.00	1.411 1396,
ę.	1.4060	8.44984E-03 4.51986E-03	11.402	0-19047 22-542	23022. 0.92451	3161.7 10728.	407.57 570.00	1396.
0	90, 25 1, 4000	8.90945E-03 4,51493E-03	17.415 1393.5	0.35963 40.365	24264, 1,6592		408.23 579.00	1.407 1394,
ı	100.00	4.35806E-03	13.007	0. 34738 37.121	25472. 1.5291	3163.1	409,09 570.00	1.402

	CP/CY	OENSITY WI	u LZ	, M3	FLOW ANG(D)	P-STAT P-STAG	TEMPERS T-STAG	AEFOCITA HVCH VO
			•		••			
	Q.0 1.4000	4.34911F-07 4.34911E-03	1402.9	0.0	0.0	3031.4 9925.9	406,18 570,00	1.4201
	0.24 1.4000	4.53178F-04 4,34814E-03	0.63565 1402.7	-8.49291E-03 -19.741	1235.7 -0,76548	3031.4 9921.4	406.21 57°,00	1.4199 1402, 8
···	0.98	9,61236E-04	1.2706 1460.6	-7.69512 <u>E-02</u> -29.707	2473.2	3039.1 9908.9	406.65 570.00	1,4172
	2.20 1.400C	1.36585E-03 4.371135-03	1. 9066	-5.70455E-02 -41.760	3721.1 -1.7136	3058-1 , 9887-7	407-62 570-00	1.4113
	. P 4 71441,						***************************************	
	3.91 1.4000	1.82720E-03 4.35604E-03	2,5421 1391.2	-9.42874E-02 -51.602	-2.1242	3076.4 9858.0	570-00	1302.8
	6.11	2-293e3E-03	3-1072	-0-12452	6243-2	3092.3	404.04	1.4027
	1-4000	4.494755-02	1389.6	-54,289	-2. 2373	9870,1	570-00	1390.6
	8.02	Z.766CJE-C3	3. 4522	-0-15698	7532.6	3102-1	408-29	1.4072
	1.4000	4.426776-03	1392.7	-56. 754	-2.3336	9972.9	510.00	1393.8
	12.05	3.24176E-03	4.5332	-0.17771	8835.4	3106.5	406.98	1.4152
	1-4000	4,447C7E-03	1398,4		-2,2449	10099,	570-00	1399.5
	15,80	3,719456-03	5.2260	-0.18937	10147.	3107.0	405.47	1.4244
	1.4000	4.4646E-03	1465.0	-50, 832	-2.9720	10234.	570.00	1406-0
	20.08	4.10683E-C3	5, 8993	-0.19871	11429.	3101.9	404.56	1.4299
	1.4000	4,46733E-03	1409.0	-47.461	-1.9292	10248	570.00	1409,8
	24.87	4-64639E-03	6a 55 33	-0-17958	12685.	3096.2	404.30	1.4315
	1.4000	4.441946-03	1410.4	-38,649	-1.5697	10302.	5 70.00	1410.9
	30.14	5.10314F-03	7. 2025	-0-15926	13934.	3090.0	404-11	1.4327
.	1.4500	4.455116-03	141344	-31,200	-1,2667	10290.	577,00	1411-7
	35.94	5,55543E-C3	7,8443	-0,12647	14170.	3002.7	404.01	1,4333
	35.94 1.4000	4.445846-03	1412.0	-22.765	-0.92366	10263.	570.00	1412.2
	42,23	6.C1313E-03	8.4937	-7.26182E-02	16421.	3079.4	403. 91	1.4334
	1. 4000	-4.451 9RE-Q3	1412-5	-12,077	-0.48905	10240.	570,09	1412• <u>•</u>
	49.01	6.46737E-03	9.1465	-4.29670E-02	17665.	3072.4	403-51	1.4363
	1.4000	4.43630E-03	1414.3	-6. 6437	-0.26915	10502.	570.00	
	54.29	4-92778E-03	5.7970	4.75187E-02	19923-	3071.9	403-54	1.4361
	1,4000	4,43534E-03	1414.2	6-8591	0.27790	10289,	570.00	1414,2
	64.07	7.374C1E-03	10.428	5,52455E-02	20142.	3265.4	403.54	1.4341
•••••	1.4000	4.42598E-03	1414.1	7, 4919	C. 30 354	10267.	570.00	
	72.33	7.82874E-C3	11-054	0-19793	21377.	3044.5	404.00	1.4333
	1.4000	4.422526-03.	1412.0	25,292	1,0250	19230.	570,00	1412.2
	81.98	0.279306-03	11.696	0,19922	22610.	3061.7	403.84	
	1.4000	4.41722E-03	1412.7	22.975	0.93174	10227.	570.00	1412.4
	90-31	4.72690E-03	12.302	0.35301	23623.	3062-0	40444	1.4306
	1,4000	4,41099E-23	1409.7	40,430	1.6436	10174,	570.00	1410,3
	100 00	A 145445 CT	12 444	0.34424	15600			
	1.4000	9.16594E-03 4.40127E-03	12-809	37.557	25009. 1.5299	3061.5	405 <u>-29</u>	1,4255

STREAM		W1		, b.3	146	P-STAT	TEMP(R)	MACH N
CP/	<u></u>	DENSITY	<u>U</u>	·····	FLOW ANGIOS	P-STAG	T-STAC	VEL OC 17
	0.0	4.53509E-07	6.23035E-04	0.0	1, 2323	3214.9	413.10	1,3776
. 1.4	1000	4.33909E-03	1372.6	0.0	0.0	9923.9	570.00	1372.6
	0.25	4.7260CE-04	C. 64592	-8-90627E-03	1285.7	3710.6	413-22	1.3773
	cca	4,530258-03	1372.3	-10,803	-0.78512	9921,5	570,00	1372,4
	1.00	9.43144E-04	1. 2971	-2.56479E-02	2564.0	3212.7	413-14	1.3777
1.4	000	4.330565-03	1372.4	-30.311	-1.2653	9909.5	413.16 570.00	1372.7
	2.23	1.41435E-03	1.9400	-5.94217E-02	3839.9	1205.5	413.14	1,3777
	-QCD	4.520546-03	1372.1	-42.013	-1.7339	986.9	579.00	1372,7
	3.99	1.57828E-03	2.3777	-9.36726E-C2	5099.8	3191.9	413-01	1,3704
1.	400 O	4.30286E-C3	1 372.4	-33. 91 5	-2.1247	9834.7	570.00	1 2 73 . 3
	6-22	2-34028E-C3	3-2213	-0-12351	6355-0	3174.5	412-07	1.3063
,	4000	4. 48 B55E-03	1376-5	-52,770	-2.1958	9001.0	570.CO	1377.5
		1 401445-01	3.6812	-0.15238	7624.5	3154-1	410.18	1.3958
1-	4000	2,50309E-03	1364.6	-54.360	-2.2463	9977.5	***************************************	1385.
		-	4, 5344	-0.16968	8470.3	3192.4	407.00	1,4091
	12.20 4000	3.266CCE-03 4.47457E-03	1394.6	-51.934	-7.1334	10106.	37C.CO	1395.4
			121					
	13. <u>57</u> 4000	3,72533E-03 4,47101E-03	5,2375 1404.3	-9.17773 -47.636	10173.	3112.0	405,66 570.00	1.4231 1409.1
	00.50	incomete data			72 7 30	11210	100	13 13 23
	2C.26	4.10329E-03 4.45792E-23	5. 9C10 1410, 6	-0.18433 -44.062	11422. -1.7892	3092.7 10298.	404.22 372.00	1.4320
		·						
	25.04 4000	4.44089E-03	1413.7	-0-16444 -35-517	1 2648. -1. 4391	3073.7 10302.	403 <u>.53</u> 370.00	1414.
	30.14	3-07616E-03	7.1073	-0.14361	13869.	3041.7	403.06	1.439
	4000	4,625965-03	1415.9	-28.291	-1.1446	10298.	570,00	1616,3
	34.12	3. 51 861E-03	7.8224	-0.11704	15001.	3048.7	407,73	1.441
1.	4000	4.410496-03	1417.5	-20.302	-0.8 2060	19283.	3 70.00	1417-0
	42,40	5.4674E-03	8.465B	-3.9581 0E-02	16311.	3041.2	402.47	1.442
	4000	4,40260E-03	1418-7	-9. 9844	-0 - 40 324	16561*	570.00	341.0,
	49.14	6.41332E-03	5.1120	-3,139326-02	17533.	3031.1	421,96	1 - 443
1.	4000	4. 39371E-03	1420.4	-4, 8949	-0.19738	10293.	570.00	1470.
6	56.43	4. 96527E-03	5. 7577	5.597776-02	18774.	3028.3	401.90	1.446
1.	4000	4.35030E-73	1421.1	8.1526	0.32869	10289.	570,00	1421-1
7	64.19	7.303398-03	10.304	A-35096E-02	19976.	3020-3	461.74	1,446
	4000	4. 37 927E-03	1421.3	9.6932	0.35043	10266.	576.00	1421.
8	72.42	7. / > 3 E6L - C3	11,006	C-20092	21196.	3020-1	402.24	1.444
10	• • • • • • • • • • • • • • • • • • • •		1537a9	25, 913	1,0459	10230,	370,00	1419,
9	01515	8,19887E-03	11.644	G-19416	224150	3014.7	402.66	3, 443
1	4000	4.368698-03	1420. Z	23. 461	0.93529	10227.	570.00	1473.
0	90.34	8.04G85E-C3	12.247	0.34980	23615.	3014.4	402.43	1,441
	4000	4,361086-03	141744	40,482	1,6340	10174,	370,00	1417,
1	100.00	9.075306-03	12.832	0.34271	24790.	3013,6	403.47	
	4000	4.332146-03	1414.0	37.763	1.3299	10100.	370.00	1414.

2	TREAMLINE & CP/CV	OENZITA M!	b2 U	W3 V	FLOW ANGLOS	P-STAT P-STAG	TEMPIRA T-STAG	MACH NO VELOCITY
			4 444 300 44					4
X	1.4000	4,71929E-07 4,71829E-03	6,34175E-04 1344,1	0,0 0.0	1, <u>2757</u>	3398.2 9925.9	419.63 570.00	1.3385 1344.1
2	0.26	4.929576-04	C-66239	-8-69059E-03	1532.6	3394.0	419.68	1.3363
		<u></u>	134348	-17,631	<u>-0,75171</u>	9921-5	472.00	1343,4
3	1,02 1,400C	9-81059E-04 4-69659E-03	1.2204	-2.81437E-0Z -25.668	-1. 2211	3378.7 9908.2	- 419.16 570.00	1,3414
•	2.29	1.46016E-03	1.5707 1549.6	-5.77565E-02 -59.555	3951.4 -1,6787	3345.9 9886.2'	419.25 570.00	1.3449
	1,4000	4,440965-03			-			1350-2
5	4,06	1,92657E-03	2. 6101 1354. 6	-9.25132E-02 -47.916	-2.0256	3301.6 9855.5	417-03 570-00	1,5542
	1.4000	4.61271E-US	1334.0		-2.0236	402243	210-00	137760
•	6.52	2.304756-03	2.2550	-0.11818	6467.2	5252.9	414.91	1.2671
	1,4000	4.56798E-03	1564.1	-49.555	-2.7805	9885-1	570.00	1365.0
7	9.08	Z.83959E-03	3.5089	-0.14414	7713.5	5204.7	412.00	1.3847
	1.4000	4.55203E-93	1376.8	-51.474	-2.1411	9931.6	570.00	1 577.0
•	12.55	3.29047E-03	4. 5763	-0.16353	3958.0	3158.0	408.79	1.4042
	1,4000	4, 50251E-03	1390, 5	-49,697	-2,0465	10112.	570.00	1591-7
•	16.14	5,74096E-03	5.2498	-0-17191	10203.	3120.3	4C5. 9C	1.4217
	1.4000	4.47895E-03	1403.3	-45.955	-1.6756	10234.	\$70.00	1404-1
10	20.44	4-18210E-03	5, 5040	-0.17955	11420.	3085.8	405.96	1.4336
	1,4000	4.45G82E-05	1411.7	-43.005	-1.7449	10298.	570-00	1412.4
	25.24 1.4000	4.61721E-03 4.42256E-03	6.5407 1416.6	-14.922	12617. -\.4122	3058.0 10302.		1.4402
12	30.52 1.4000	5.05218E-03 4.39930E-03	7,1742 1470,0	-0.14158 -28.023	13817. -1.1305	3036.0 10297	402.09 570.00	1.4450
						20.00		1420,1
	34.30	5.48491E-01	7. 6021	-0.11247	15700. -C.82737	5017.2 10283.	401.54	1422.4
	1.4000	ar	142203	getting Till and	W. L.	W4 - 100 Pm	577.00	1424.0
14	42,56	5.92467E-03	0.4393	-5.90716E-32	15 208.	3005.2	401.10	1.4510
	1.40C0	4.3%540E-03	1424.4	-9, 9704	-9.40104	10281.	570-00	1424,5
15	49.31	6.36243E-03	4- CAC3	-3.48909E-02	17412.	2992.0 10293.	400.46	1.454
	1.4000	4.353126-03	1427.2	~70 4837	-0.22010	102436	\$70.00	1427.
16	56.50	6.8CT24E-C3	4.7195	5.65860E-0Z		2986.6	400.51	1.455
	1,4000	4.347C4E-03	1427-8	8,3125	0.33157	10289.	570,00	1427-1
	64.30	7.23978E-03	10.341	5-85872E-02	19817.	2977.0	400.19	1,4560
	1.4000	4.554256-05	1428.3	6,0646	0.32351	10246	\$70.00	1428.
16	72.51	7.671536-03	10.559	0.26148	21021.	2975.4	407.53	1.454
	1.400Q	4,33932E-Q3	1426.4	26,294	145319	10730,	570,00	
12	81.20	4-12101E-03	11,593	0-19019	22777.	2969.4	400,33	1.455
	1.4000	4.32145E-03	1427.5	23.419	0.9 39 85	10227-	570.00	1,455
50	90.37	8.55741E-03	12.193	0.35011	\$3419.	2968.5	40C. 89	1.452
	1.4000	4-51431E-Q3	1424.6	40,912	1.6449	10174,	570, 30	1425,4
	100,00	8.98764E-03	12.776	0,54120	24578.	2967.8	401.70	1.447
	1.4090	4.304678-03	1421.4	57,963	1.5299	10100.	570.CO	1421.

**	STREAMLINE \$ CP/CY	DENSITY	₩2 U	W3	FLOW ANGID)	P-STAG	TEMP(#) T-STAG	MACH NO VELOCITY
X	0.0	5.01328E-07 5.01328F-03	6.50328E-04 1297.2	0.0	1.3466	3699.3	429.94 570.00	1,2763
2	C. 26 1.4000	5.25172E-04 5.01312E-03	0.58106 1296.8	-5.27129E-03 -10.037	1410.6 -0.44345	3699.8 9921.3	430.01 570.00	1.2758
3	1.05	1.0419ZF-03 4.97531E-03	1.3562	-1.82232E-02 -17.490	2800.5 -0.76981	3662.8	42 9. 94 570.00	1.2023
4	2.36 1.4000	1.54155E-C3 4.90616E-03	2.0201 . 1310.4	-3.93774E-02 -24.895	4149.5	3597.1 9885.0	427.01 570.00	1.2939 1310.7
5	4.17 L.4000	2.015176-03	2,6679	-6-469C9E-02	5440.0	3511.1	424,45	1.7094
•	6.41	4-81965E-03 2-47717E-03	3, 3161	-32.054 -8.46167E-02	-1.3890 6693.1	3417.7	570.00 420.74	1322.5
	1,4000 9,30	4.73287E-03	1334.7 3.5713	-34.159 -0.11319	-1.4617 7921.9	9890.9	570.06 416.31	<u>1379-1</u> 1-3566
	1.4006	4.65524E-03	1354.3	-58.715	-1.6326	9989.6	570.00	1358,6
	12.62 1.6000	3.35883E-03 4.58407E-03	4,6321 1379.1	-9.13643 -40.619	9128.1 -1.6071	323 8.0 101 23.	411.56 570.00	1,3874 1379,7
	1.4000	3.78730E-03 4.52282E-03	5. 29L0	-0.15247 -40.259	103zo. -1.6506	3162.6 10244.	407-41 570-00	1397.6
10	20.80 1.4000	4.20270E-03 4.46130E-03	5. 92 66 1410. 2	-C.17189 -40.899	11474. -1.4613	3096.0 10298.	404.33 570.00	1.4313 1410.8
.11	25.62	4.41055E-03	6.5437 [419.3	-0.16147 -35.023	12604. -1.4135	3040.9 16302.	402.23	1.4441 1419.7
13	36.91 1.4000	5.02011E-03 4.36019E-03	7.1595 1426.0	-0.14829 -29.539	13737. -1.1867	2998.4 10296.	400.48 570.00	1.4556
13	36.68 1.4000	5.42651E-03 4.32075E-03	7.7674 1431.9	-0.12874 -23.723	14861.	2962.1	399.44 570.00	1.4612
14	42,93	5.84507€-03 4.29572E-03	8.3893 1435.3	-7.05998E-02 -12.079	16016. -0.48216	2938.2 10282.	398.52 570.00	1.466
15	1,4000	6.76054E-C3	4. C133	-5.92611E-C2	17165.	2914.5	397.47	1435, 3 1, 4732 1430, 7
-10	1.4000	4,27244E-03	9-6398	-9.4658 	18343.	2953.4	397.09	1434.7
	1.4000	4.26016E-03 7.10249E-03	10-247	7.3437 3.17935E-02	0.29194	10286.	570.00 396.75	1441,3
18	72.71	7.526636-03	12.854	0.20170	20650.	2002.4	570,00 396,43	1.4765
	1,4000	4,23132E-01 7,95592E-03	1441-7	26.790 0.17395	1.0645	10229,	570,00	1442,0
	1.4000	4.22295E-03	1443.0	21.664	21825	2874.9 10227.	376,65 570.00	1.4782
20	90.44 1.4090	9.37593E-03 4.21392E-03	12.071 1440.4	0.35646 42.537	22981. 1.6915	2972.3 10173.	397-15 570-00	1.4752 1441.1
- 21	1,4000	#. #0041E-03	1437.3	0.33762 36.387	24122. 1.5299	2671.2 10100.	397.92 570.00	l.4704

11ERAY LOW NO. = 300 O. O.SCHARGE(CD), 7HF US7(VD), AND PRESSURE 1PO) - COEFFICIENTS

WF WF/WFO WF/WFI VO VO/VDO VO/VDO PO YHRUS7(LBF)

2736.5 0.94843 C.96668 10169. 0.38698 0.34129 69382. 2.490178 05 1
2532.9 0.92397 0.80903 10408. 0.39610 0.34933 65244. 2.37669 05 2
2604.9 0.95662 0.91448 12531. 0.47668 0.4057 61681. 2.331442 05 3
2604.9 1.04364 1.0609 12953. 0.47668 0.4057 61681. 2.331442 05 3
2604.9 1.04364 1.0609 12953. 0.49295 0.43474 60433. 2.30012E 05 3
2604.7 0.96382 0.92737 12994. 0.49651 0.43612 5723C. 2.20016F 05 9

	MF	wF/wF+	WF/WF1	V O	40/4D+	A0\A0-J	PO	THRUST(LBF)
•	2734.5	0.44843	C. 46C6B	101690	0.38698	0.34129	69302.	2.499176 05 1
	2532.4	0,92397	0. 88903	1C408.	0,39610	0. 34933	65244.	2. 37669E 05 2
	2604.9	0.95042	0. 91 448	12531.	0.47468	0.42057	61681.	2. 331 44E C5 3
	2463.9	1-04364	1.00609	12953.	0,49295	0.43474	60433.	2.30612E 05 4
	2641.7	0.96382	0, 92737	12994.	0.49451	0.43612	5723C.	2. 20616F C5 '\$
	2644.4	1.03778	0. 99853	14015.	0.53337	0.47039	349250	2.145035 05 6
	2784.3	1.01569	C. 97746	13337.	0.51390	0.45499	.3410.	2.10:838 0: 7
	2715.3	0.99068	0. 93 122	13357.	0,50632	7.44629	51324.	2.032C7E 05 8
	2733.7	C. 99740	0. 95968	14115.	C. 53714	0.47372	48693.	1. 973176 25 9
	2728.8	0.99927	0.96148	14982.	0.56634	0.49944	461110	1. 91616E 05 10
	2738.8	0.99925	0. 96146	13450.	0.59589	0.32552	43574.	1. 460446 05 18
	2738.2	0.99506	C. 96126	16524. 1752 6.	0.66703	0.55438	38385	1. 60733E 03 12 1. 75657E 05 13
	2736.4	0.99912	C. 96134	16673.	0.71071	0.62679	25665	1.707146 05 14
	2742.1	1.00045	3. 96262	20114	0.76544	0.67506	32822.	1. 663076 05 15
	2743.7	1.00104	0-96318	77063.	0.83951	0.74938	29459.	1-61851E 03 16
THRUAT	2740.8	1.00000	0, 96217	20277.	1.0000	0.86192	24202	1. 58586E 05 17
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	2749.5	1-07315	C. 96522	26995.	1.1034	0.97312	21676.	1.391 076 05 18
	2768.9	1.01026	C. 97205	31 785	1.1830	1.0433	19863.	1.60059E 05 19
	2700.0	1.00700	0. 96892	32929.	1.2331	1.1052	17889.	1.596485 05 20
	2742.5	1.00062	C. 96278	34202.	1.3016	1.1479	16407.	1, 56995E 05 21
	2737.3	0.99878	0. 96171	34893.	1.3279	1.1711	15690.	1.589128 05 22
	2737.1	0. 99665	0. 96 C88	33248.	1,3414	1.1030	15370.	1. 59019E 09 23
	2737.2	0.99867	0. 96091	35508	1.3513	1.1917	15147.	1. 59136E 05 24
	2737-1	0.99866	0, 96059	35715.	1.3592	1.1987	14976.	1.592528 05 25
	2737.1	C. 99864	0. 96068	35 9 63 .	1,3655	1.2043	14847.	1.59372E 05 26 1.59497E 05 27
	2737.1	0.95862	C. 96CB6	36025	1.3709	1.2091	14745.	1. 59497E 05 27
	2737.0	0. 99860	0. 94654	36132.	1.3758	1.2133	14667.	1.59629E 05 28
	2736.9	0.99858	0. 96C82	36272.	1.3904	1.2174	14503.	1. 59765E G5 29
	2736.9	0.99856	C. 96C=0	30?91.	1.3849	1.2214	14508.	1.59904E 05 30
	2736.8	0.99634	0.96078	36512.	1.3895	1.2254	14432.	1. 60043E C5 31
	2736.8	0.99853	C. 96077	36634.	1.3942	1,2295	14353,	1.601736 05 37
	2736.7	0.99851	0.96075	16760.	1.3969	1.2337	14272.	1.60320E C5 33
	2736.7	C. 99450	0.96074 0.96973	36486.	1.4037	1.2360	14109.	1. 67455E 05 36
	2736.6	0.99848	0. 96072	37012. 37138.	1.4065	1.2422	14105.	1.60568E 05 35
	2736.6	0. 39647	C. 96071	372040	1.4101	1.2506	13935.	1.6071 0E 05 36 1.60646E 05 37
	2736.4	0.99646	0. 96070	373A7.	1.4220	1.2548	13452.	1.60971E 05 38
	2736.6	0.99846	0. 96070	37506	1.4274	1.2589	13769	1.610936 05 39
	2776.6	0.99845	C. 9607C	37627.	1.4319	1.2628	13489.	1.61214E 05 40
	2736.6	0.99846	0. 96070	37741	1.4363	1.2667	13012	1. 61 331 6 05 61
	2736.6	C. 99346	0. 96071	37852.	1.4405	1.2704	13536.	1. 41 44 76 05 42
	2730.6	0. 99847	C. 96071	3795 60	1.4445	1.2736	13450	1. 61941E 05 49
	2736.7	0.59849	C. 96C73	30059.	1.4484	1.2773	13403.	1.616745 05 44
	2736.7	C. 99850	0. 96074	30153.	1.45 20	1.2005	13344.	1.417878 05 45
	2736.6	0.99852	C. 96076	38243.	1.4554	1.2835	13289.	1, 61893E 05 44
	2730.6	0.99532	C. 96076	30325.	1.4785	1.2663	13240.	1.61996E 05 47
	2736.9.	0.94857	0.96CB1 -			1-2890 -	13194	" 1.42109E 09 48
	2736.7	0.99651	0. 96075	31471.	1.4641	1.2912	13156.	1.621926 05 49
	273644	0,99837	0.96052	38530,	1,4543	1,2932	13120.	1,022055.05 70

	STREAML INE &	W1	42	L/3	W4	P-STAT	TEMP (R)	MACH NO
	CP/CA.	DENSITY	U		FLOW ANG(O)	P-SYAG	T-STAG	AELOC LA
· Y	0.0	4.72865E-07	3.262C2E-04	0.0	2.3955	9360.6	560.53	0, 24065
	1.4000	9.72995E-03	337,31	0.0	0.0	9925.9	570-00	227-21
2	0.0	9.662846-07	3-44851F-04	0.0	2.3857	9797.2	559.44	- 0.30710
	1.4000	9.652846-03	356.15	0.0	0.0	9925.9	570-00	356.15
3	e.0	9.630586-27	3-621116-04	0.0	2,3748	9227.0	559.23	0.32465
	1.4000	9.63058E-33	376.00	0.0	0.0	9425.9	570.00	374.00
4	0.0	9.57255E-C7	3.799816-04	0.0	2.3627	9149.3	555.07	0,34315
	1.4000	9.57255E-03	, 396.95	0.0	0.0	9925.	570.00	396.95
3		9:30757E-07-	3.466C8E-04	o. 6	2.3492	4062.5	***************************************	0.36293
	1.4000	9. 50757E-03	419.25	0.0	0.0	9925.9	570-00	419,25
	0.0	9.434575-07	4-18018E-04	0-0	2.3339	8965.2	553-66	0.38414
•	1.4000	9.43457E-03	443.07	0.0	0.0	9925.9	370.00	443.07
·	0.8 ·	9.35231E-07	4. 36235E-04	0.0	2.3167	**************************************	551.72	0.40697
	1.4200	9.35231E-03	458.50	0.0	0.0	9925.9	570.00	468,58
	C-0	9.25855E-07	4.59427E-04	0.0	2.2970	8731.9	549,50	0. 431 84
	1.4000	9. 25855E-03	496.22	9. C	0.0	9925.4	573.00	496.22
	0.0	9.15100F-07	4.81636E-04	<u>G.0</u>	2.2745	4590.2	546.94	0.4341Y
	1.4000	9.15100E-03	526,32	0.0	0.0	9925.9	570.00	524.32
10	0.0	9-02670E-07	5-049C5E-04	0.0	2.2460	8427.3	543.96	0.48424
	1.4000	9-02670E-03	559.35	0.0	0.0	9925.9	570.00	555.35
1T	0.0	N. 86C35C-07		0.6	Y-7170		345.41	6.32326
**	1.4000	0.88035E-03	596.20	C. 0	0.0	9925.9	570.00	594,20
		e. 70569E-07	5.55284E-04	0.0	2,1790	8010.7	536-14	
12	1.4000	0.7C569E-03	637-84	0.0	0.0	9923.9	570.00	0,56197
13		8.45062E-07		c-o	¥. 1'557	7735.X	550.80	0. 60767
13	1.4000	8.49C62E-03	686-27	0.0	0.0	9925.9	570 . 80	686.27
						••••		
14_	1,4000	8.21459E-07 8.21459E-33	6-11617E-04 744-79	0.0	2.0742	7395.3	523.83 570.00	0,66387
					76.0		195	
15	0.0 1.4COP	7.42979E-67 7.82979E-03	6.47967E-04 671-18	0.0	1. 9904	6905.6 5925.9	513. e7 570.00	0.73901 821.10
		••••••						
16	(.) 1.4000	7-10740E-C7 7-10740E-03	6.77561E-04 953.32	0.0	1.8306	5730 <u>-4</u>	494.35 575.00	0.87470
	1. 4000			1315	11.5-2.5	447764		953-32
1A	0.0	6.56179E-07	9. 4667 9E-ge	0.0	1.7079	5392.4		0, 57503
	1.4000	6.56179E-03	1746.7	C-0	0.0	9925.9	570.00	1046-7
18.	. O.Q	5-46452E-Q7	4-80979E-04	0.0	1-5471 -	- 4407-4	457.77	

	1.4000	5-464528-03	1141.2	0.0	0.0	9925.9	570-00	1161.2
19	0.0	5.79554E-07	6.7541 0E-04	0.0	1.5312	4531.9	455.61	1.1204
 - 	1.4000	5.795548-03	11.72+3		0,0	9925.9	570-00	1172,3
20	C.O	5.73221E-07	6.77836E-04	2,0	1.5164	4462.7	457.61	1.1327
	1.4000	5.732206-03	1102.5	0.0	0.0	9925.9	570.00	1102.5
21	0.0	5.673318-07	6.76241E-04	0.0	1.5027	4398.7	451.74	1.1441
	1.4000	5.673316-03	1192.0	2.0	0.0	4925.9	570.00	1192.0
<u>2</u> 2	5.0	5.61805F-07	6.746338-04	0.0	1.4898	4338.6	449, 98	1,1549
	1.4000	5.61805E-03	1209.8	0.0	0.0	9925.9	570.00	1200-0
53	0.0	5.56584E-07	6. 7301 7E-C4	0.0	1.4775	4282.4	448.30	1.1651
	1.4000	5.56584E-03	1209-5	0.0	0,0	9925.9	570. oc	1209,2
24	0.0	5.516058-07	6.713906-04	0.0	1.4658	4228.9	446.69	1.1749
	1.4000	5.51.0056-03	1217.2	0.0	0.0	9925.9	570.00	1217.2
25	0.0	5.468745-07	6.657656-04	0.0	1. 4347	4178.2	445.15	1.1842
	1.4000	5.46874E-03	1224-7	0.0	0.0	9925.9	570-00	1224.7
26	C.0	5-423418-07	4.44138E-04	0.0	1.4440	4129.8	443.67	1.1932
0.0	1.4000	5.42341E-03	1232.0	c. 0	0.0	9954.9	570.00	1232.0
-2i	0.0	3.37986F-07	6-56510E-04	. c.o	1.4337	4083.5	442.24	1.201
	1.4000	5.37986E-03	1236,9	0.0	0.0	9925.9	570-00	1238.9
28	0.0	5.33789E-07	4.64RBOE-04	c. o	1.4236	4038.9	444.86	1.2102
	1.4000	5.33746E-03	1245.6	0.0	0.0	9925.9	572.00	. 1245.6
29	0.0	5.25733E-07	6.53251E-C4	0.0	Y. 4142	3996.0	439.52	1.2183
	1,4000	5.257338-03	1252.0	0.0	0.0	99?5.9	570.00	1252.C
30	0.0	5.25ELOF-07	6-616726-04	G.0	1.4049	3954.7	438.21	1.2762
200	1.40C0	5.25810E-23	1250.3	0.0	0.0	9925.9	57C.00	1256.3
31	0.0	5.220C7F-07	6. 59596E-04	0.0	1.3959	3914.7	436,94	7.2539
	1.4000	5.22007E-C3	1264.3	0.0	0.0	9925,9	570.00	1264-3
32	0.0	5.1831 X-07	6.583716-04	0.0	1.3871	3875.9	435.70	1.2414
	1-4000	5.183136-03	1270.2	C- 0	8.0	9925.9	570.00	1270.2
-33	0.0	5.147206-07	6. 367418-04	-0.0	Y. 3786		434.49	Y.2487
	1.4000	5.147206-03	1275.9	0.7	0.0	9925.9	570.00	1275,9
34_	C-0	5.11274E-07	6.52127E-04	0.0	1.3702	3901.9	473.31	1.2559
	1,4000	5.11224E-03	1201.5	0.0	0.0	9925.4	574.00	1281.5
35	0.0	3.07613E-07	4.53509E-04	0-0-	1.3421	3766.5	432.15	1.2624
	1.4000	5.07813E-03	1286.9	0.0	0,0	9925.9	970.00	1286.9
36	0.0	5.04485E-07	6.518938-04	0.0	1.3542	3732.0	431.02	1.2498
-	1.4000	5. 04486E-03	1292.2	0.0	0.0	9925.9	570.00	1205.2
37	· 0.0	5.012256-07	6.302776-04	8-a	1.3464	3696.2	429.90	1.2765
*	1.4000	5.012256-03	1297.4	0.0	0.0	9925.9	570.00	1297.4
38_	0.0	4-190476-07	6.466676-04	0.0	1.3388	3665.4	428.81	1.2831
	1.4000	4. V8047E-03	1302.4	c.c	0.0	4925.9	57C.00	1302.4
39	6.6	4.544386-07	6.47663E-04"	b_ 6		363375		1.2096
	1.4000	4.94938F-03	1307.4	0.0	0.0	9925.9	57C.00	1307-4
40-	0.0		6-45443E-04	0.0	1,3240	3602.2	426.68	1.2959
40-	400	-7a7117/6-0/		0.0	197674	3002.2	456600	

_	1.4000	4.910976-03	1312.2	0.0	0.0	9925.9	570.00	1312.2
41	0.0	4.88914E-07"	6.43865F-04	0.0	1.3169	3571.7	425.44	1.3022
	1,4000	4.899136-03	1316.9	6.0	0.0	9925.9	570.00	1316,9
42	0.0	4.85990E-07	6-472728-04	0.0	1.3099	3541.0	474.62	1.3004
- 22	1.4000	4.65989E-03	1321.6	0.0	0.0	9925.9	570.00	1321.6
43	0.0	4.491216-07	4.474828-04	6.5	1. 1030	3512.6	425.62	1.3144
**********	1.4000	4.631216-03	1326-1	0.0	0.0	9925.4	570.00	1326-1
44	0.0	4.8C297E-07	6.3909ZE-04	0.9	1.2962	3483.9	422.63	1.3704
	1.400C	4.802978-03	1330.6	0.0	0.0	9652	573.30	1330.6
43	7.	4.775336-57		0.6	7.2945	3435.8	421.45	T.3263
	1.4000	4.77533E-03	1335.0	0.0	0.0	9925.9	570.00	1335.0
46	0.0	4.74815E-07	6.35935E-04	0.0	1.2029	3428.3	427.69	1.3321
	1.4000	4.748(56-03	1339.3	0.0	0.0	9925.9	570.00	1339.3
47	0.0	4.721466-07	6.34364E-04	0.0	1.2765	3401.4	419.74	1.3379
	1.4000	4.721446-03	1343.6	0.2	0.0	9925.9	570,00	1343.6
48	0.0	4.695216-07	6.32795F-04	C.O	1.2702	3374.9	419.81	1.3435
	1.4000	4.655701-03	1347.7	0.0	0.0	9925.9	570.00	1347.7
49	6.0	4.66 93 8E-07	6.312336-04	0.0	X-39.m.	3344.0	417.09	Y. 3491
	1.4000	4.5e938E-03	1351.9	0.0	0.0	9925.9	570.00	1351.4
50	0.3	4.643956-07	4.25674E-04	0.0	1.2574	3323.5	416.97	1.3546
	1,4000	4-04395E-03	1355.9	0.0	0.0	9925.9	£79.30	1355.9

S'	TREAMLINE &	w1	W2	w3	44	P-STAT	TEMP(R)	MACH NO
100	CP/CV	DENSTIV	U	V	FLOW ANGIDS	P-SYAG	Y-STAC	VELOCITY
Υ	100.00	2.65403F-02	4,3146	-4.1066	65468.	9360.6	557.75	0.33134
	1.4000	9,77844E-03	351-15	-194,51	-23.749	10100.	570.00	383.64
2	100-00	2.59820E-C2	5.5179	-4.1879	64139.	9297.2	556.47	0.34605
	1.400C	9.73110E-03	366.33	-161.18	-23.749	10100.	570.00	400-22
3	100-00	2-541408-02	9.7211	-4.2773	62790.	9227.0	335.44	0.36173
	1.4C00	9.67858E-03	382.51	-166.30	-23,749	10100.	570.00	417, 97
4	190-00	2.48366E-02	9, 9288	-4.3687	61420.	9149.3	554-12	0.37850
	1.4000	9.62076E-03	399.76	-175.90	-23,749	10100.	570.00	436.78
·	100.00	2.42457E-02	10.142	-4.4626	60022	4042.5	552.62	0. 19661
	1.4000	9.5549AE-03	416.32	-184.06	-23.749	10100.	570.00	457.02
30	100.00	2.164C5E-02	10.362	-4.5592	58593.	8965.2	550-91	0.41620
	1.4200 -	9.481596-03	478.30	-192.85	-23,749	1010C.	570.00	478.86
·	100.00	2. 3C198E-G2	17.587	-4. 6581	57130.	8855.9	348.99	0.43746
•	1.4003	9-39892E-03	455.89	-202-35	-73.749	10100.	570.00	502.44
	100.00	2.23778F-02 9.30469E-03	10.919	-4.7602 -212.72	55622 <u>.</u> -23,749	8731.9 10100a	545.78 570.00	0.460E0 528.18
			100 = 510151					
9	150.00	2.17114E-02 9.19641E-03	17.058 509.30	-4.8653 -224.04	£060. -23.749	10100.	544.23 570.00	0.48658 556.42

10	100.00	2,10164E-02 9,07169E-03	11.304 537.64	-4. 9735 -236. 65	52437. -23.749	8427.3 10100.	541,26 570,00	0.51525 587.60
								197
17	100.00	X-058[5E-05	11.558	-3.0436	50725	V236.7	537.73	0.54774
	1.4000	8.92461E-03	569.69	-25C.75	-23.749	10100.	570.00	622.62
12	100.00	1.94964E-02	11.821	-5. 201 Z	48905.	F01C.7	533,48	0.54507
	1.4000	8.74908E-03	676.31	-246.78	-23,749	10100.	570-00	662.41
13	100.00	1.86376E-02	12.094	-5. 3214	46921.	7735.1	524.17	0.62931
	1.4000	8.53294E-03	648.90	-285.52	-23.749	10100.	570.00	709.94
14	_100.0C_	1.76668F-02	12-378	-5.4464	44687.	73*5,3	521,23	0.68399
27	1.4000	8.25554E-03	70C. 64	-306.50	-23.749	10100.	570.00	765.46
15	100-00	1.64923E-02	12.675	-5, 5760	41946.	e905.6	911.32	0.75748
	1.4000	7.464828-03	758.51	-334.15	-23,749	10100.	570.00	839, 62
3.	100.00	1-405456-02	12.993	-5.7170	37806.	6030.4	491.90	0.89097
	1.4000	7.142836-03	686.51	-390.11	-23.749	10100.	570.00	968.64
1y	100.00	Y-323656-02	15.745	-2.6454	34304	9342:4	476.44	b. 49092
	1.4000	6.59450E-73	1036.3	-214.55	-11.675	10100.	570.00	1060.2

	1.4000	5.69375E-03	1172.5	31.313	1.5299	10100.	570.00	- 1172.9
9	100.00	1.17238E-02 5.82443E-03	13.874	0.37054 31.606	31020. 1.5299	4531.9 10100.	453.35 570.00	1.1343
		750 a.s.	LEDAL U.S.					
<u> </u>	1.4600	1.16111F-02 5.76C78E-03	13.657 1193.5	0.37009 31.874	30762. 1.5299	10100.	451-36 570-00	1193.9
i	100.00	1.1507cE-02	13.840	0, 36964	30 523.	4398.7	449.50	Y.1577
	1.4000	5.70158E-03	1202.8	32.123	1.5299	10100.	570.00	1203.2
<u> </u>	1,4000	1.14101E-02 5.64605E-03	13.823	0.36919 32.356	30 300. 1.5299	4378.8 10100.	570.00	1.1684 1211. \$
····-	100.00	Y:13140E-02		0.36675	36891.	4787.4	446.6Y	Y.1784
	1.4000	5.593596-03	1219.8	32,576	1.5299	10100.	572.00	1220.2
•	100.00	1.12327E-02 5.54354E-03	13.789	0.36828 32.786	29892. 1.5299	4228.9 10100.	572.00	1.7883
5	100.00	1.115116-02	13.772	0, 36782	29704.	4178.2	442.95	1.1976
-	1.4000	5.49600E-03	1235.1	32.985	1.5299	10100.	573-09	1235.5
6	1:4000	1.10733E-02 5.49045E-23	13.755	236736 33,176	29525 ₀ 1,5299	4129.8 10100.	441.47 573.00	1,2065
y	156.65	1. C9958E-02	13.738	0. y669I	29333.	4003.5	440.03	Y.2151
	1.4GCD	5.40667E-03	1249.0	33. 359	1.5299	10100.	572-00	1249, \$
	100.00	1.04274E-02 5.36449E-03	13.721	0.36645 33.535	29188. 1.5299	4038.9	478.67 370.00	1.2235
9	100.00	1.085876-02	13.704	0.36599	29 a 30 a	3946.0	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	1.2313
·	1.4000	5.323746-23	1262.0	39.705	1.5799	10100.	570.00	1262.5
<u> </u>	100.00	1.07924F-02 5.26431E-03	13.667	0,36553 33,670	28877. 1.5295	3954.7 10100.	436,04 579,90	1,2394
i	100.00	1.072846-02	13,670	0.36503	287294		434.78	1.2470
1	1.4000	5. 24609E-03	1274.1	34.029	1.5299	10100.	570-00	1274.6
2	100.00	1.06664E-92	13.452	0.36462	28585.	3875.9	433.54	1.2545
	1.4000	5. 20896E-03	1279.9	34.184	1.5249	10100-	570.00	1,2545 1280,4
3	100.00		13.635	0.36416	26446.	3036.4	432.34	1.2018
	1.4000	5.17285E-03	1285.6	34,334	1.5299	10100.	570.00	1 286.0
14	100.00	1.05481E-02 5.13772E-03	13.518	0.36371 34.481	20311. 1.5299	3801.9	421.16 573.00	1.2689
5	100.00	1.044146-65	13.601	0.36325	20180.	3766.5	450-01	1.2756
	1.4000	5.10344E-03	1756.4	34.624	1.5299	10170.	579.00	1276.9
36	100.00	1.04363E-02	13,584	0.36280	29052.	3732.0	429.88	1,2827
	1.4000	5.070016-03	1361.6	34.763	1.4299	10100.	572.90	1302.1
Y	100.60	1.036236-02	13.367	0.36234	27427.	3694.2	424.77	1.2094
	1.4000	5.03723E-03	1306-7	34.909	1.5299	10100.	573.66	1307.2
	100.00 1.400C	1.032598-03	13.550	35.033	27805. 1. 5299	10100-	424.68 570.00	1.2959
19	166.00	Y.C2788E-02		0.36143	27336:	3633.5	425.61	1.3024
	1.4000	4.974058-03	1316.6	35.163	1,5299	10100.	570.00	1317.1
	100.00	1-02249E+02.	41a516a «	0.36098	27570	3402-2	424-57	

	1-4600	4.943488-03	1321.4	35.290	1.5299	10100.	570,00	1321.6
41	100.00	1.015006-02	13,499	0.36753	21457.	3571.7	423, 53	1.3150
	1.4000	4-91350E-03	. 1326-1	35.415	1.5299	10100.	570.00	1326,5
42	100.00	1-013226-02	13.482	0.36008	27345.	3541.0	472.52	1.3711
	1.40CC	4.884128-03	1330-4	35, 538	1.5299	10100.	570.00	1331.1
43	100.00	1.008546-32	13.463	0.35965	27234.	3512.6	421.52	1.3271
·	1.4000	4.055295-03	1335.1	35.650	1.5299	10100.	570.00	1 335.6
44	100-00	1-003946-02	13.449	0.35918	27129.	3483.9	420.53	1.3331
	1.4000	4.8269CE-03	1339.6	35.776	1.5299	10100.	575.00	1340-0
43	100.00	4.95452E-03	13.412	0.35873	21024.	3855.8	419.56	**************************************
	1.4000	4.79913E-03	1343.9	35.892	1.5299	10100-	570,00	1344.4
46	100.00	9.450436-03	13.415	0.35828	26922.	3428.3	419-41	1-3447
	1.4000	4.77181E-03	1344.2	36.006	1.5299	10100.	570.00	1348.7
47	100.00	9.90721E-03	13.390	0.35763	26821.	3401.4	417.66	1.3594
	1-4003	4.74499E-03	1352.4	36.118	1, 5299	10100.	570.00	1352.0
48	100.00	9-264775-93	13.381	0.35738	26722-	3374.9	416.73	1.3561
	1.4000	4.71861E-03	1356.5	36.228	1.5299	10100.	570.00	1357.0
49	100.00	9.82339E-03	13.365	0.35694	26624.	3349.0		\$ 1686.Y
	1.4000	4.492666-03	1360.5	36.337	1,5299	10100.	570-00	1 361,0
50	100-00	9.78203E-03	13-346	0.35649	26529	3323.5	414.91	1.3671
-	1.4000	4.667096-03	1704.5	36.444	1.5290	icico.	570.00	1345.0

DEAR.	• 65	-30CIPS	A		380.0PS	A								
1	1. 709	0.000	···	1.009	0.136	3	1.009	C. 271	4	1.009	C- 407	5	1.009	0.541
···•	1.009	2.679	·· - j		0. 814		1.009	0.950		1.004	1.006	10	1. 209	
11	1. 309	1.357	12	1.009		13	1.009	1. 620	14	1.709	1.764	15		
21	1.009	2.035	17	1.009	2.171	10	1.009	2.307	19	1.009	2.442	50	1.009	2.570
DBAR		.000195	IA!		640. OPS	FA								
-	2.645	0, 200		P. 444	C.119	_	8-649	6, 238		9.649	0.357		8. 649	0.475
		0.594	7	8.649	0.712		9.649	2. 737	•			ló	8.649	
	9. 644		17 17	8. 649	1.30Y	. 13.	3.647	1.4Z4	1.	8.649	1. 545	15	8.649	1.663
. 10			17_	8.649	1.991	1.0	5.649	2.020	1•	8.649	2.139	50	8.649	2.250
21		2.376												
JEAR	= 59	.0001PS	IAD		920 . 0 <i>P</i> 5	FA								
1	12,329	0.COO	2	12.329	C-111		12.379	0. 221		12.329	C. 372	5	12.379	0.443
	12. 329	0.554	7	12.329	C. 664	. 6	12,329	0.775	9	12.329	0. 486	10	12.329	0,994
-11	12, 325	1.107	-12	12.329	1.210	- 13	12.377	1.328	-13	12.329 12.329			12.32	
	12.329			120324		76	120329	1.002		120 >24	1,772		120 327	20103
OGAR	• 50	.000(#5	141		200. 0PS	FA					·········			
_	14,386	A 844		14,384	A 184	_	94 942	0.212		14.356	A 11 A		VA 584	A 430
	14.386		-	14.386			14.386	7.743		14.396			14.386	
··•••	1 4. 30c	1.042			·· 1.166		14.386	1.274	1:	14.386	1. 340	115	74.300	
	14.346		17	14.386	1.098	10	14,386	1.005	1.	14.386	1.911		14.306	
	14, 386				• • • • • • • • • • • • • • • • • • • •	••								
CHAR	4	5.0001PS	IAT		48C. QPS	FA							·	
. 1	15.486	0.00	2	15.486	0.104	3	15.486	0.200	4	15.486	0. 311		15.486	
	15.486	0. 514		15.400				0.726	•				15.486	
11	15.486	1.C37	12	15.466	1.141	13	15.464	1.245		13.486			13,484	
	15.486	2.074		13.446	1.660		15.486	1. 763	1.9	17.486	1.667		15.484	1.97
OBAR	4	C <u>. 0001P</u> S	1.61		760 <u>. 0</u> 75	F6	•••••••					- · · · · · · · · · · · · · · · · · · ·		
-1	16.424	0.00	- 7	16.424	0,102	-	16.424	C. 251	<u> </u>	76.324	0.355		16.424	0.40
•	16.424	0.500	7	16.424	0.610		16.424	9.712	9		2.013		16.424	0. 91
~ • • ·	14.474	1.017	12	14.444		" [3	16.424	T. 220	14	16.424	1.321	15	16.424	1. 42
	16.424												14.424	

ISUBAR	1	35	OCCEPS	A }	5	040.3PS	FA								
1	17.4	19	0.000	2	17,449	0.101	3	17.449	0.201	4	17.449	0.301	5	17.449	0.402
6	17.4	49 -	0.502	7	17.449			17.449				0.804		17.449	0.904
11	17.4	4.5	1.074	12	17.449	1.105	13	17.449	1.205	14	17.449	1.306	15	17.449	1.406
16	17.4	49	1.507	77	17.449	1.607	10	17.449	1.707	19	17.449	1. 108	20	17.449	1.908
21	17.5	49	2.009												
150BAR	<u>.</u>	30	000162	(<u>A)</u>		320.0PS	FA						•		•
	22.3	33	0.005	2	22.333	0.101	,	22,333	0.272	4	72.333	0.303	- 5	22.333	0,404
6	22.3			7	22.333	C-637	À	22.333	9.70R	9	22.333	0.509	10	22.333	
11	22.3		1.C11	12	22.333		13.	22.333	1.213	14	22.333	1.314	is.		
16	22.3		1.516	17	22.333			22.333	1.719	19		1.620	20		
21	22.3		2.C22												
1506AR	•	25	.000(PS	IA)		630.0PS	FA								
1	40.0	73	0.000	2	40.073	0.104	3	40.073	0.207	4	40.073	0.310	5	40.073	0.414
6	40.0	73	0.517	··-ÿ-	40.073	0. 621		40.073	0.724		40.775	7.628	10	4C.073	0.931
11	40.9	73	1.535	12	40-073	1.130	13	40.073	1.242	14	47.073	1.345	15	49.073	1.449
16	42.0	73	1.552	17	45.073	1.656	10	40.C73	1.759	19	40.073	1.862	25	40.073	1.960
21	40.0	72	2.045							-					

RETURN FROM "ISOGAR"

STR	EARLINE &	wi	WZ	W3	W4	P-STAT	TEMP(P)	MACH NO
	CP/CV	DENSITY	U	V	FLOW ANGID)	P-STAG	Y-SYAC	AE FOCI A
[4.41582-01	3,11 494E+84	0.0	2,4844	9419.4	561:32	6. 27484
	1.4000	9.77285E-03	119.25	0.0	0.0	9 925, 9	570.00	319-25
2	0.0	9.65795E-07	3.5321 eF-04	0.0	2. 3805	9263.8	555, 07	0.31560
	1.4000	9.65795E-03	355.73	0,0	0.0	9925.9	570.00	345.73
j	4.0	9.023286-07	5.055 CBE-04	0.0	2.2473	8422.8	347.08	0.49006
	1.4000	9.02328E-03	560,23	0.0	0.0	9925.9	570.00	560, 23
	0.0	9.21 283E-07	4-67876E-04	0.0	2.2886	8679.5	549.54	0. 44204
	1.4000	9-218836-03	507.52	0.0	0.0	4452.4	570.00	101.32
5	5.0	4-2444E-0A	3.721546-04	9.5	5.3911	9184-0	557.49	0.33500
	1.4000	9.55647E-03	357.72	0.0	0.0	9925.9	570-00	307.72
6	0.0	9-630076-07	3.62272F-04	0.0	2.3747	9226.3	558.22	C. 32402
	1.4000	9-630378-03	276.19	0.0	0.0	9925.9	572.00	376,14
¥	6.6	9. 51036E-07	3.478366-04	6.0	2, 3498	9066.2	35¥.45	0. 36210
	1.4000	9-519366-03	<u> </u>	0.0	0.0	9925.9	577.00	410.32
8	0.0	9.35288E-07	4. 381 01E-04	0.0	2.3168	8854.7	551.74	0.40482
	1.4000	9.352095-03	468,41	0.0	0.0	4425. 6	570.00	468.4
ġ	0.0	4.24107E-07	*** 631 82E-04	6.6	2, 2933	\$700.8	549.09	6,4363
	1.4000	9-241076-03	501.22	0.0	0.0	9925.9	579.00	501.23
0	0.0	9.151146-07	4. 91 602E-04	0.0	2.2743	059C-5 -	546.95	0.4590
	1,4000	9-15118E-03	526.27	0+0	0.0	9925.9	570.00	326.2
1	6.0	9.060C3E-07	4. 449.41-04	0.0	X. X931	8470. 9	314.76	0.4613
	1.4000	9-06006E-03	550.65	0.0	0.0	9925.9	571,00	550-69
2	0.0	8.95714E-07	5.16926E-04	0.0	2.2333	8336.5	542,28	0. 5055
	1.4000	8.95714E-03	577.11	0. 3	6.0	9425.9	570.00	577.1
¥	0.0	8-84519E-07	3. 34413E-94	0.0	2.2095	9191.8	53% 56	0.5311
	1.4000	8.645196-03	60 77	0-3	0.0	9925,9	570,00	604.7
4	0.0	8.72C86E-07	5.521728-04	0.0	2,1830	8030.3	536.51	0. 5586
	1.4000	8.72086E-03	634-31	0.0	0.0	9925. 9	570.00	634.3
5	0.0	8.59710F-07	5.69681E-04	2.6	2,1365	7871.2	533.45	0.5032
	1.4000	8.59710E-03	662.64	0.0	0.0	9925.9	579.00	662.6
6	0.0	8-46143F-07	5.8607CE-04	C-0	2.1274	7697,9	537-07	0.4137
	1.400C	0.46143F-03	692.64	0.0	0.0	9025,4	57%.00	692.6
¥	····· `o.o		6. ce556E-04	0.0	5.0015	7428.2	524.66	
	1.4000	8-248648-03	737.77	0.0	0.0	9975.9	570.00	737.7

	1.4000	8.13472E-03	761.10	0.0	0.0	9925.9	570.00	761.10
19	0.0 1.4070	7.99113E-07 7.99113E-03	6. 11129E-04 789. 79	0.0 0.0	2.0256	7105.6 9925.9	51 8. 08 570, 00	0.70786 789,79
20	0.0	7.537946-07 7.537946-03	6.60350F-04	0,0	1.9262	6547.9	506,12 570,00	0,79439
ž1 · · · ·	0.0	6.93237E-07	6.81970E-04		1.7413	3023.5	489.45	0.40713
	1.4000	6.93237E-03	983, 75	0,0	0.0	9925.9	570.00	983.75
22	1.4000	6.1C535E-07 6.1C534E-03	1122.1	C.6	1.6030 5.0	4674.6	570.00	1122.1
25	0.0 1.4000	5.80344E-07 5.80644E-03	6.75676E-04 1170.6	0.0	Y. 5336 0.0	4543.8 9925.9	455. 95 570. 00	Y. 1103 1170. 6
24	0.0	5.566CCE-07	6.73023E-04	0.0	1,4775	4282.4 9425.9	448.30 \$70.00	1.1650
25	0.0	5.358796-07	6.657COE-04	0.0	Y. 4266	4061.1	441.55	1.2060
	1.4000	5.35879E-03 5.17741E-07	1242.3 6.50115E-04	0.0	1.3458	9925.9 3470.0	570.00 435.51	1242.3
20	1.4000	5. 1774nE-03	1271.1	0.0	9.0	9925.9	570.00	1271-1
54	1.4C00	3.01559E-07 5.01559E-03	6.50444E-04 1296.8	C. 0	1.3472	3761.7 9925.9	430.01 570.00	1.2750 1296,8
24	0.0	4.86843E-C7	6.42740E-04	0.0	1.3119	355C.5	424,92 570,00	1.3066
29	0.0	4.732126-07	6. 34 993E-04	0.0	1. 2341	3412.1	425.12	1.3356
30	1.4700	4. 73212E-03 4. 60378E-07	1341.9 6.27171E-04	0.0	1. 2480	9925,9 3283.3	570,00 415,53	1,3634
	1.4000	4.40378E-03	1362.3	0.0	3,6	9925.4	570.00	1362-3
M	0.0 1.4000	4.48170E-07 4.48170E-03	6.19256E-04 1381.7	0.0 0.0	0.0	3762.0 9925.9	411.08 570.00	1,3403
32	1.4000	4,36519E-07 4,36519E-03	* 6.11281E-04 1400.4	0.0	1.1899	3047.6 9925.9	406.75 570.00	1,4164
.7X	0.0	4.25452E-07 4.25452E-03	6.03323¥-04" 1416.1	0.0	7. 7454	2434.4 9925.9	402.62 570.00	7.4416 1418-1
34	0.0	4.15082E-07 4.15082E-03	5.95530E-94	0.0	1.1372	2840.1	398,64	1,4459
35	1.4500	4.055786-07	3° •81.04£-84	0.0	7. Y136	2749.5	370.00	1434.7
	1.4000	4.05578E-03	1450.0	0.0	0.0	0925.9	570.00	1450.0
36	1.4000	3. 47179E-07 3. 97179E-03	5.81318E-04 1463.6	0.0	0.0	2670.1 9925.0	391.70 570.00	1.5087
37***	C.0 1.4200	3.90173E-07 3.90173E-03	5.75496E-04 1475.0	0.0 c.o	7.6735 0.0	2634.4 9925.9	385.92 570.90	1,525¢ 1475,0
30	0.0	3.84935E-07	5.71047E-04 1483.5	0.0	1.0625	2555.6	366,42	1,5386 1403.5
-74	0.0	3. 61854E-07 3. 61894E-03	**************************************	0.0	7.6349	2527.4 9925.9	585,50 570.00	Y.3463
40		J. 81554E:07_			<u>le0540.</u>	2224.3,	365.46	L1912

	1.4000	3.815581-03	1457.0	0.0	0.0	9925.9	570.00	1489.0
41	0.0	3.04490E-C7	5.7C666E-04	0.0	1.0614	2551.4	396.64	1. 55 99
	1.4000	3-44490E-03	1484.2	0.0	0.0 '	9925.9	570,00	1484.2,
42	0.0	3.412265-07	5.7638CE-04	C-0_	1.0761	2614.3	399, 34	1.5232
	1.4000	1.9122eE-03	1473-3	5.0	0.0	9925.9	570.00	1475.3
43	0.0	4.0211CE-07	***5327E-04***	0.0	1.1042	2716.6	393.63	1.4967
	1.4900	4.021106-03	145*.6	0.0	6.0	9925.9	570.00	1455.6
44	7-0	4-10974E-07	5-969768-04	0.0	1.1419	2850.3	399.39	1.4615
	1.4000	4.16474E-05	1431.7	0-0	0.0	9425.9	57).00	1411.7
-45	a.p		6.101486-04	0.0		3031.4	406-18	Y. 4201
	1.4000	4.34911E-03	1402.9	0.0	0.0	9925.9	570-00	1402.9
44	c.e	4.539096-07	6.23035E-04	0.0	1.2323	3210.0	413-18	1.3776
	1.4000	4.539046-03	1372.6	0.0	0.0	9925.9	570-00	1372.6
47	0.0	4.718296-07	6.341756-04	6.0	1.2757	3390.2	414.63	1. 3365
	1.4600	4.71829E-03	1344.1	0.0	0.0	9925.9	572-00	1344.1
4.8	C-0	4- Feee5E-07	6-47642F-04	0.0	1.3115	3540.7	424.86	1.3069
	1.4000	4. 640656-73	1320-5	C. D	0.0	\$425.9	570.00	1320-5
49	3.0	3-0132eE-07	6.5C328E-04	0.6	Y. 3466		42 9. 94	
	1.4000	5.013256-03	1257.2	0.0	0.7	9925.9	572.00	1297.2
50	0.0	5.15+62E-C7	e.57322E-04	0-0	1.3816	3851.6	434.92	1.2462
	1-4000	3-13-041E-03	1273.9	0.0	0.0	9925.6	575-00	1275.9

	STREAMLINE &	wl	w2	w3	W4	P-STAT	TEMP(R)	MACH NO
	CP/CV	OENSITY	U	V	FLOW ANG(D)	P-STAG	1-SYAG	VELOCITY
1	10C-00	2.445796-02	8.9775	-3.9501	65712.	941874	··55e.73	0.31755
	1.4000	9-82156E-03	336.78	-148,18	-23,749	10100.	570.09	367.93
2	100.00	2.66336E-02	7.4574	-1. 2813	65495.	9418.4	557.13	0.26607
	1-4000	9.97517E-03	2 5C. 00	-123.20	-23.749	9893.4	557.92	305.91
3	100.00	2.61427E-02	7.5194	-3, 3065	64307.	9418.4	591.10	0.27306
	1.4000	9.956106-03	287.63	-126,56	-23,749	9910.2	559.40	314,24
4	100.00	2.533096-02	P-e154	-3.7908	62452.	9405.2	559.51	C. 32076
	1.4000	9.811705-03	340.12	-149.65	-23,749	10100.	579.00	, 371.5e
5	196.00	2.43380E-02	9,9316	-4.3700	60215.	\$110.8	553.46	1468E-0
	1,4000	9-591328-03	408, CB	-179, 56	-23,749	10100.	570.00	445-84
6	Tac-vc	2.34996-02	10.669	-4.6943	58275.	888,2	549.50	0.43184
171	1.4000	9.421088-03	454.20	-199.65	-23.749	10100.	570-00	496.22
	100-20	2.33472F-C2	S. 8002	-4.3121	57923.	9059.9	552.57	0, 39714
	1.4000	9.553308-73	418-86	-164-30	-23.749	10100.	570-00	457.61
	100-00	2.294698-02	9.6857	-4.2617	56817.	9044.4	552.30	0.40030
	1.4000	9.541336-03	422.09	-155.72	-23.749	10100.	570-00	461.15
₉	100.00	2.229376-02	5, 5970	-4, 3987	55289.	6914.3	557.02	0.47615
	1,4000	9.44329E-03	448.42	-197.31	-23,744	10100-	570.00	489, 91
10	100.00	2.161096-02	10.322	-4.5418	53695.	6763.0	547.33	0.45503
	1.4000	9.32632E-03	477.44	-210.16	-23.749	10100.	570.00	521.83
-11	100.00	2. 09464E-62	18:376	-4:8534	35152	8613.4	544.66	0.48233
	1.4000	9.214728-03	505.05	-222.22	-23.749	10100.	570,00	551.78
12	100.00	2.023446-02	12-844	-4.7714	50479.	8438.4	541.44	0.51332
	1.4000	9.080256-03	535. 93	-235.81	-23.744	10100.	570.00	503.51
13	- 10c.00	1.947766-02	11.139	-4. 8970	46721.	8227.5	537.56	0, 54928
	1.4000	8.917526-03	571.40	-251.42	-23.749	10100.	570.00	624.27
14	100.09	1.859316-02	11.500	-5.0600	46686.	7933.0	531.99	0. 59767
	1.4000	6.606356-03	618.51	-272.14	-23.749	10100.	570.00	675.74
-i5	100.00	1.761906-02		-3.2163		7574.4	525.02	0.45450
	1,4000	M.4G440E-03	672.87	-796.96	-23,749	10100.	570.00	735,12
14	100.00	1.610416-02	12.430	-5.4692	41022.	4851.4	510.81	C. 76116
	1.4C00	Y. 6-915E-03	771.66	-33 9, 62	-23.749	10100.	57°-00	843.27
-17	100-02		12.068	-2.4936	23766.	2490.4	402.57	Y.4420
• 1	1.400C	4.32797E-33	1388.9	-287.01	-11.675	10100.	570.90	1418.3
	100 a0G			G-29649 .	201340	.2310.8	373499	1.0101

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	1.4000	4.6 72686-03	1363.7	36.420	1.5299	19100.	579.00	1364.2
41	100.00	7,56221E-03	13.126	0.35055	25962.	3272.0	413.C6	1.3789
	1.4000	4,61533E-03	1 372.6	36.600	1.5299	10100.	570.00	1373.1
42	130-00	9,458746-03	13.066	0.34897	25714.	3216.7	411.05	1,3905
	1.4000	4.55948E-03	1381.4	36.893	1.5299	10100.	570.00	1351.9
43	100.00	9.35806€-03	13.007	0.34738	25472.	3163-1	409.09	1.4024
	1.4000	4.50513E-03	1389.9	37.121	1.5299	10100.	570.C0	1390-4
44	100.00	9.26035E-03	12.948	0.34560	25236.	3111-3	407-14	1.4141
	1.4000	4.45233E-53	1340.2	37, 342	1.5299	10100.	570.00	1398,7
43	100-00	9. Y6594E-03	12.869	0.34626	25004	3061.4	405.29	Y. 4255
	1.4000	4.40127E-03	1406.2	37.557	1.5299	10100.	570-00	1406.7
46	100-00	9-07530E-03	12.632	0-34271	24790-	3013.8	403.47	1.4366
	1,4000	4,352148-03	1414.0	37.763	1.5299	10100.	570.00	1414.5
47	100.00	8-967846-03	17.776	0.34120	24576.	2967.8	401.70	1.4473
	1.4000	4,30467E-03	1421.4	37.963	1.5299	10100.	570.00	1421.9
48	100-00	8-901546-03	12.719	0-33968	24369.	2922.8	399.95	1.4580
	1.4000	4-257876-03	1426.6	38.140	1.5209	iotoo.	570.00	1.59.3
.5.4	106.00	6.600416-03	12.649	0.33762	24122.	2871.2	397.92	Y . 4704
	1,4000	4,20411E-03	1437.3	38.387	1.5299	10100.	570.00	1437, 8
50	100.00	6.70058F-03	12.578	C-33763	23879.	2820.7	395.91	1.4828
	1.4000	4.151106-03	1445.7	36. 8CZ	1.5374	10100.	570.00	1446.7

PRINTO	ut of	CONSTANT	PPES	SUPE PLO	T VALVES					• • • • • • • • • • • • • • • • • • • •			••••••	
150mar	- 6	5.000(PS	(A)	9	340. OPSF	<u> </u>		-						
1	1.370	0.000		1-116	0,136	3	4-875	0. 127	•	5.315	0.125	5	1.084	0.271
	4.8C5		¥	5.207	0.253	••••		0.407	••	4. 547		1ó	5.131	0.360
11	1.070	C- 542	12	3.935	3.517	13	5.094	2.527	14	1.259	0.678	15	1.945	0.644
16	5.292		17	1.052	0.614	18	3.958		19	3.120	0.760	20	1.050	0.949
21	4.237	0. 930	22	5. 266	0.684	23	1.056	1.085	24	4.768	1.017	25	6.056	0.996
26	1.070		27		1.143	5.8	6.084	1. 1 20	29		1.355	30	4.976	1.269
	6-114		32	1.190	1.488	. 33	2-019	1.602	34		1.696	35	3.471	1.624
	3,197		37	3. 131	2-096	36.		2.227	39		2.158	40	1. 240	2.404
43	4.153		42	2.000	1-508	43	3.000	1.688	44	4.000	0.455	45	4,000	0.873
46	4.000	2.556	47	>• 000	0.095	48	>-600	1.276	49	6.000	0.964	50	4.000	1.261
ISGBAR	- 6	C-00C(PS	14)		64C.OPSF	4								
	2.742	0.000	-,	3.846	C. 000	_	0.581	0.000	-	2.509	0.132		3,407	3.130
	9.534		Ť	2. 301	0. 266	•	3. 230	0.261	•	9.607	0.233	10	2.070	
	3.200		12	··· 9. 728	0.349	~13	1.936	0. 535	···14	3.129	0.524	15 -	6. 720	0.492
ie	7.376		17	9.941	0.464	ié	1.722	0.670	19	3.27	0.654	žó	6.321	0.620
<u>23</u>	8.223		22	1C. 174	0. 5 77	23	1.687	C. 805	24	3.438	0.782	<u>25</u>	6.376	0.743
20	6.719		27	10.264	0.692	28	1.067	0.940	29	3.548	3.911	30	6.520	0.065
31	8.963	0.827	32	10.233	C. 807	33	1.753	1.072	34	3.739	1.032	35	6.721	0.965
36	1.930	1.203	37	4. 933	1.161	38	7.448	1.092	39	2.200	1.331	40	4.135	1,288
•1	8.956		42		1.452	43		1.427	44	9.172	1.294	45	9.281	1.409
40	5.467		47	6.253	1.613	48	9.351	1.524	49	4.829	1.742	50	6.367	1.733
31	9.412		25.		1.916	33	6.352	1.0.0	54	4,475	1.755	55	4.525	
7.6	6.187		57	9.550	1.869	5.	4.734	2.167	59	5.432	2.133	60_	9.654	1.961
61		2. C84	62		2.147	63		2.285	64	2.000	7.42	-65	\$.000	1.235
71	3.200		67	4.000		75	4-000	0.451		- 5.000	1.696	70	5.000	2.222
76	8.000		77		2.071 0.853	78		1.201	77	10.000	1.076	19.	8.000 10.000	0.549
			!	78 000	V	; =.	48000						10.000	0.097
1 SOHAR	- 5	5.300193	TAT		1920.0PSI	A				· ·-				
•	14-493	0.00	•	14.639	0-104	·····	14.584	A 313		14.501	0.316	•	14.407	0 434
	14.315			14.151		····	2.716	6.923			- 0. 91 R	···· 16	14-089	0.748
11	2.670		12		1.047		13.032		14	2.762	1.166	15	3.229	1.177
	13.792		17	13.627			19.436	1.140		11.313	1.302	20		1.416
21	13-137	1.525	22	13.119	1.634	23	13-152	1.742	24	13.246	1.847	25	13.361	1.951
	13.627		··· 27	14.036	2.136	. 50	3.000	0.848		3.000	1.321	30	14.000	0.610
31	14.000	2.130												
150dAR	. ,	0.030(PS	SIA)		200.005	A								
	10.474	```o. 396''		14.226	0.161		13.145	0.501.	•	14.341	0.302		17.851	0.002
		0.502		17-343			17.062	9.703	i Q	16.403	0.007		16.567	
···· 11	16. 333	1.019		10.117		··'13	15.074	1.234		15.621	1.745		15.409	
16	15-245	1.564	11	15.150	1.071	.16	15.109	1.777_	19	15.114	1.782	20	15.179	10064

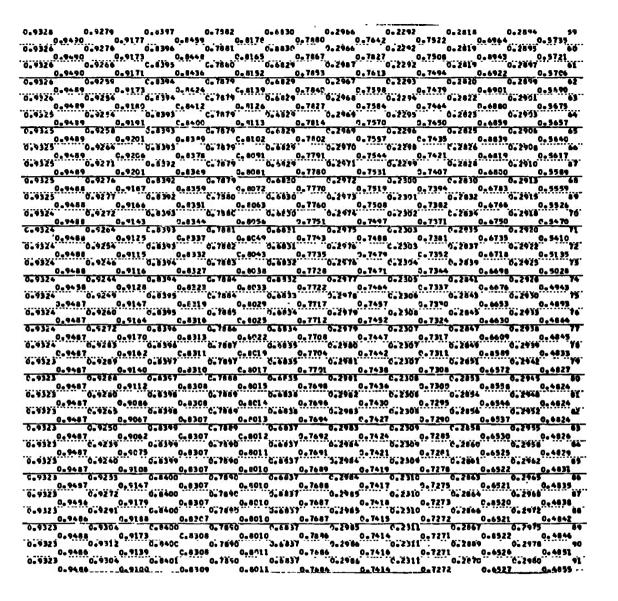
21	15.541	2.072	ŽZ	16.000	1.183	23	17.000	0.721	24	18.000	0.330			
13004				• •••••••••										
	20.094	0-000	,	19.919	0-101	3	19-906	0-202		19-639	0.302	•	10.747	0-403
	19.607	0. 574	Ť	19.432	0.604	A	19.213	0. 202	9	19.005	C. 605	10	18.620	0. 905
11	16.249	1.005 _	12.	17.932	1.106	13.	17.461	1. 205	. 14.	17.028	1. 305	15	16.707	1.414
21	16.103	2.047	22	14.000	1.927	23	16.000	1. 954	24	17.000	1.312	25	18.000	1.001
26	19.000	0.807	21	2 C. OCO.	0.076			7.2222						
ISOBAR	- 40	0-00C(PS	TAT		760. OPS	71								
									. 					
	21-067	0-220	2	20.976	C-101	3	20-947	0-202	4	20.894	0.303	- 5	20-808	0.404
	21.067	0.534	··	20.512	0.605	A	2C. 241	0. 706	9	20.017	0.836	īố	20.800 19.734	0. 907
11_	19.371	1.007	12	19.000	1.107	13	18-716	1 - 207	14	18.274	1.3C7	. 15	17, 843	
16	17.335	2-C39	22	17-003	1.606	18	18-000	1.716			1.876	20	16.336 20.007	1.935
26	21.0C0	0. C 50												
- 1 KOWAN	· · · · · · · · · · · · · · · · · · ·		171		60407084	F4	· · ·							***
130022														
-	21 - 824	0-000	,	21.968	0-101	•	21 - 8 5 8	0.202	•	21.022	0-303	4	21 - 762	0.404
	21.926	6. 505					21.257	0.707	····•	. 54.452	0.807	- Xę	21.767	0.908
11	20.372	1.008	12	15.959	1.109	13	19-695	1-209	14	19.279	1.309	15	10.054	1-409
16	18.336	1.508	17	17.009	1.604	18	17.418	1.707	19	16.996	1.627	20	16.682	1. 920
26	21.000		- "	11000	10003		18.000	10303		19,000	10370	- 63	20,000	1.075
		C PARANA			CAYATTANA									
ISOBAR	- 30	0.0001PS	IAP	· ·	• 320. OF	-				_			_	
		-												
	23.857	0.000	- 2	23.398	0-101	- 3	23.855	0.203	+	23.775	0.810	10	22.655	0-910
11	22.543	1.011		21.921			21.223	1.211	14	29-727	1.311	15	20.214	
1.	14-653	1.311	17	19-922	1.610	1.0	100229	1.0704	··· 19	17.645	1.000	5Q	17.055	1.907
21	16.650	2.C23	<u>22</u>	17. COO	1.911	23.	18.000	0.005	24	19.000	1.597	25	20.000	1.444
						-	234000	0. 103						
TSUBA	- 2	5.00C(PS	TAT		3400. OP	FA					,-			
											T-00 D-0000			
1	27.673	0.000	2	40.341	0.000	3	27.664	0.102	4	44.334	0,105		27.677	0.204
	48.505	0. 209	. 7	27.629	0-305 C-611		49.021 27.271	C.314		27.601	0. 407	10	47, 757	0.419
- 11	27.532	1.017	- 15	27.385	1-114		25.AAY	1.219	- 12	30 322	4 414	70	26.854	1.419
21	26.650	1.518	22	26.320 20.900 35.003	1.614	23	29.475		74	34-147		25	19,732	1.713
40	21.370	40 / 30	21	35.003	1.747	26	10.629	1. 311	24	\$0.0IU	1.030	30	35. 214	Y-851
31	17.725	1.509	32	26.160	1.930	37	35.489	1.754	34	16.643	2.014	35	20.125	2.032
	33,497			17.000	1.963	39		1.862				40	2C.003	3-645
41	21.000	1.604	42	27,000	1.556 0.852	48	27.030		44			50	25.000	1.360
89	26.000 30.000	1-415	42	31.000	1.594	53			- 34	33.003	1.593	55		1.650
36	35.000	1.747	···-39	49.000	0.109			6.443			49 7.77.		34,000	3, 432
	(5				20.00F	SFA								**********
														
1	33.600	0. COO	2	44.125	0.000	3	33.507	0.103	4	44.128	0.104	5	13.609	0.205
6	44.025	0. 200		33.596	0.308		43.71	0.312	9	33.540	0.410	16	43.243	0.416
11		0. 213	12		C. 519	13	33.77	C-616	14	41.212	7.622	15	34.114	0.719
16	33.600 44.025 33.636 39.185	0.724	17	48. 257	1.000	3.2	17.14	2.00	24	49.159	2.013	20	49.051	1.777 ?.C15
	20004	*****			86.702			- COXII		AC # 123	CRY C	<u></u>		:C'LZ.

21-177 34-000			2.093 0.794 					
	r. 219			50.000		 	 	

(P	PD5 WA	CC/AAY'S 'RES	decalation					
1	4	13	14	16		7.6	20	22
9268 0.9	059	7931	6.7312	0.5971	0.5339	0.4562	0.4414	0.4296
	0. 921	0.6370	71 0. 7 0. 7534 97 C. 7	0-5433 0-6 0-5433	0.3926	0.3604		
9282 C.9	0.922 126	A 4111	A 36 4A	0.409	0-3536	0.3443	0.4294	2.4175
0,9445	0.922	1 0.61 6.6152 5 C.61	27 0.7	0.43	277 0.5	452 0.462 0.3270 491 0.466	9 0.43	1 0-4250
9289 C.9 0.945Z 9295 C.9 G.9458	0.920	5 C. 81	33 0. 7	566 C.	372 0.5	491 0.466	1	0.4190
9295 C.9 G.945 <u>6</u>	0.919	0.6165 7 C.61 3.8211	C. 7683 36 G. 7 C. 7728	561 0.4	0.3158 0.5 0.3038	0.3689 561 0.469 596 0.47 6.2775 647 0.49	7 0.42	0.4059 57 0.4132 0.4032
9274 0.9	159	J- 8211	C. 7725	0.6497	C.3038	C-2916	0.4090	0.4002
9299 0.9	1 AY	0-4232	0.7752	0.6575	0.2952	C.2775	0. 3096	0.3446
0.9463	175	7 C. 6250	E. 7772	C. 6641			0.3693	
0.9463	0.916	0.8266	C6 C-7	574 0.1	628 0.5	C-2560	A 5335	0.4645
0.4462			19A 0_7	0.6691 564 C. 0.6726.	5672 2.5	20 31	3 3,41	29 0.3925 C. 7841
9297 0.9 0.9461 9296 0.9	0,914	0.40	73 0.1	550 C.	6710 C.S	849 0.52	0.3692 79 0.41 0.3625	0.3030
9296 0.9	0.912	0.8293 5 0.80	0.7000 073 0.1 0.7868 057 0.1	938 J.	0.2851 6746 °.5	0. 2468 897 0. 53	0.3625	Ar. O* 3AD.
9294 C-0						0.2442	0-1554	0-3405
9294 0.	203	0.4317	0, 7921	0.6788	0.2871	0.2426	0.3484	0. 3770
9293 0.	210	0. 6	770 0,	0.6794	0.2886	0.2426 975 C.52	0.3420	0.3726
0.9457	C. VG	0.00	C 70.31	C. ARAY	A. 5003	0-3413	77 Ue 46	87 0.404
9293 0.	0.90	72 G. 6	011 0.	514 C.	6861 0.6	0.53	11 0.49	24 0.412
9293 0.4 0.9494 9293 0.4 0.9496	0.90	P 5 C 8	005 0.	521 0	6665 0.0	0.53 0.2407 0.54 0.2402	32 0.49	45 0.419 0.3555
9293 0.	0-90	0.8354 54 C.B	0.7840 002 0. 0.7844 002 G.	0.6786	0.2926 6864 C.	0.2402	63 0.50	0,3616 45 0,419 0,3555 58 0,427
0343	9234	0.8362	0.7444	0.6788 <u>527 0.</u> 0.6785	0.2934	Da 2 39 7	0.3251	0.3494
9294	9242	0- 8370	0.7949	0.6785	0.2939	0.2392	97 0.5227	67 0.435 0.3435
9296 0.	9249	43 C. 6 0. 6377	0.7456	0.6788	6874	0.2386	05.3206	0.3435 93
0,9459	0.90	41 0.8	011 0.	0-6793	6670 0.0	0.59 0.2379	0.31 96	41 0,457
9299 0		39 G. 6	010 7670	569 C.	6912 C.	243 0.40 C.2370	12 0.54	78 0.462
0.0442	7264	0.8384 39 G.6 0.8390 39 O.6	027 0. 7870	7583 0.	6949 0.	C.2370	7.3166 10 0.56	0. 3296 32 0. 470
. 9300 0. 0. 9463	9277	0 0 304	0.7878	0.6624	0.2946	6343 0.61 0.2361 6407 0.62		
.9302 0.	6276	C.8402	276 0. 3. 7585	0.6811	0.2946 0.2946	0.7355	6.3120	
0.9465 0.9304 C.	<2 66 90	0-1607	0. 2892	o late	0-2946	0-2346	C-3096	6. 121.9
0.9467		37 C. 6	050 0.	7626 0.	7048 0.	0.2339	0. 10 72	0.3201
	0.90	37 0.8	064	7642 0	7091 . 0.	4615 0.64	72 0.61	34 0.494

CUTPUT FROM DATA SET NO. 14

9**<u>1</u>9....



0.9323	0.9	301	C-8433	0.7589	0.64	0.7721	0.7452	0.2397 C.731	0.2868	0.2993	125
0.9323	0.9	0.8874	0.8403	0.7849	8043	0.7720	0.7452	0.2307	0.2868	0.2993	126
0.9323	0.9	001	C. 8403	0.7889	0.683 0.9043	0.7720	0.7451	0.2307 0.731 0.2307 0.731	0.2867 2 0.65	70.2992	127
0.9323	497	0.9309	0.8403	0.7889 8339	5404	0.7720	0.7451	0.2307 0.731 0.2397 0.731	0, 2867	0.2992 79 0.	128
0.9323	1487	0.9286	0.6433						C. 2867 2	0.2992 79 0.	4912
0.9323	9467	258 C.9459	0.8403 0.8402 0.8402	0.7889	0.663 0.6041 0.6041			0.2307 2.731 0.2307	0.2867 2 0.65 C.2867 2 0.65	0. 2993 0. 2993	.4913 -4913
0.9323 0.9323	467	0.9484	0.8431	0.7869	0-8041			0.2377	2 0.65 0.2867 2 0.45	0.2491 0.2441	.4913
	9467	0.9340	C-8401	8332	C. 8041	0.7719 35 0.7719	C.7450	0.2307	2 0.65	61 0.2991	·493 4 V4
0.9323	9487	0.9064		8331	C. 9C 40		3030	0-2307	2 0.65	et 0	134
0-9323	9467	0,669	0.	6331	0. 8040	0.7718	0.7450	0 . 731	2 0,65	0.2990	• 4•15
0.9323	9447		0.9400	6332 0.7669	0.68			0.2307	0.2866	0. 2990	4915 136
0.9323	0.	0.842		0.744	0.66	35 7.7718 35 0.7757	0.793	0.73		0.2490	137
6.4353	9487 C.	9000	C.8401	0,7486 8335 0,7469 8336	0.66 G. 8539 G. 6638	35	5.2960 0.7450 0.2960 0.744	6.2357 9 0.731	0.2667 2 0.85 0.2867 2 0.65	0 2990	730
A:4353,	9486	0.913	C- 54 01	C. 78EB	C. 8C37	25.7717	0.2981	0.2308	C. 2967	0.2490	139
0.4323		5044 0.940				35 					140
0.9323	9486	9220	0.8379	C. 7888	0.69 C-8036	0.7716		0.2308 9	C.2867 C.2867	83 0 0.24-1	4916
0.4321	9486	9323	C. 3396	6,7810	0.6036	35 C.7716	0.2991	°C. 2306 0. 731	0.2867	0.2491	142
0.9323		9323 0.920 9323	0.8397 1 0.	0.7888 6328 C.7887	7.66 C.8036	35 0.7716	0.744	0.2300 9.0.731 0.2360	0.2867	63 6	4916
0.	9486	9323 0.686 9323	C. 8 396 5 O.	6321	Us 0U36	0.7716			0.2867 0.2667	63 0. 2993	4915
0.9323	7486	9323 6.863 9323		0.7867 8327 C.7887	0.8034					63 2491 0. 2491	4915
	9486	0,687	9 0.	8328	0.8036	3.7715			1 0.65	03	4914
0.9323	9486	0.884	0. 8393	0330 0.7864	0. 8036 0. 8C36	0.7715	0.2961 0.2961	0.2308 6.2306 7 0.731	0.2468 0.65 0.2868	62 6. 2941	4914
	9486	9034	A ATAL	A 744	A 4	44	A VEAT	A 3124	0.2868	0.2991	149
0. 9323	9486 C.	0,907	0.6341	0.788		C. 7714	0.744 0.744	7 0.731 0.731 0.731	0.2868	9.5441	150
	9486	89 8Y	0.8391	0. 7884	0, 4	134	0.2081	0.2306	C. 2868	0.277	151
C.9323		9142	A 1100	0.798	0. 9035	0.7714			0.2468	C+3441	152
6.4323	9444	9290	0.8396	0.784	C. 8735	33	0.2980	6.2308 6.2308 6.2308	0.2868	0.2991	133
0.9321	C.	9323	0. 8 366	0,784		0.7714			0.2864	0.2991	134
-0.4323	7.	4323					-			0.244	
0.5373	9487 C.	9323	2.0363	0.768 6332 0.768 6333	C. 8035 D. 8036	0.7714			0.2866 0.5866 0.69	0.2991	156 0,4907
0.9323	9467	9323	G. 8 381	0,767	Q-4037	32 L: .Qe. 7714	0.2980 6.744	0.2308 6.2307 6.2307	0.2868	6.2991	137

0.9325 C.9289 C.8353 O.7849 O.68C8 O.2957 C.2285 O.2845 O.9489 O.8885 Ó.8405 C.5092 O.7751 O.7477 O.7351 O.658 O.9525 O.9171 O.8344 O.7950 O.68CF O.2957 C.2285 O.2844 O.9526 O.9489 O.9188 G.8408 O.8095 O.7753 O.7479 O.7333 O.658	0.2961 191
0.9325	0.2960 192
0.9323	7.2760 172 2 0,4886 0,2959 193
0.9323 0.9019 0.8555 0.7850 0.8098 0.7754 0.7480 0.7284 0.658 0.9489 0.9489 0.6409 0.8094 0.7754 0.7480 0.7534 0.658 0.9325 0.8696 0.6356 0.7850 0.6088 0.2956 0.2284 0.2284 0.9489 0.8489 0.8489 0.8640 0.8095 0.7754 0.7481 0.2284	0,4887
0.9489 0.9489 0.9489 0.8410 0.8099 0.7775 0.7756 0.7481 0.7835 0.458	4 0.4889
0.9489 0.9489 C.8469 0.8796 0.7757 0.7485 0.7556 0.658 0.9326 0.9113 0.8356 0.7850 0.6669 0.2956 0.2264 0.2841	0.2957 195 5 0.4891 0.2956 196 6 0.4892
0,9323	
0.9489 0.9489 0.9489 0.8355 0.7351 0.6809 0.7759 0.7684 0.2283 0.2740 0.658 0.9311 0.6385 0.7351 0.6809 0.7556 0.2283 0.2740 0.658 0.9489 0.9485 0.7358 0.658	0,2956 197 7 0,4896
0-4684 3-8407 C-C-00 Q-8100 U-761 U-7-07 U-7-90 U-838	0.2955 194 9 0.4896 0.2845 199
C.9326 C.9326 0.8554 0.7852 0.6810 0.22956 0.2283 0.2839	0,2455 199 0 0,4898 _
C.9326 C.9326 0.8554 0.7852 0.6810 0.2956 0.2283 0.2839 0.659 0.9489 0.8544 C.8406 C.6201 0.7762 0.7488 0.7341 0.659 0.9326 0.9326 0.9326 0.8554 0.7652 0.6610 0.2958 0.2283 0.2283 0.2839 0.659 0.9489 0.8383 C.8407 0.8101 0.7763 0.7763 0.7482 0.659	0.2954 200
	0.29*4 201 5 0.4902
0.9526	0.2954 201 5 0.4902 0.2953 202
0.9326 0.929C 0.8353 0.7553 0.6610 0.2936 0.7454 0.7451 0.7363 0.2838 0.9296 0.9286 0.9286 0.9286 0.9286 0.9286 0.8452 0.7453 0.6611 0.7765 0.7691 0.7363 0.6598 0.9325 0.9516 0.9516 0.76836 0.7833 0.6611 0.7765 0.7692 0.7546 0.2837 0.6592 0.9325 0.9516 0.9516 0.7633 0.8412 0.7833 0.6611 0.7765 0.7692 0.7692 0.7345 0.6592 0.9592 0	0.2953 203
0.9325 0.9016 0.8357 0.7853 0.6811 0.2957 0.2284 0.2837	0.2953 204
0.9325 0.8699 0.8358 0.7853 0.8611 0.2457 (.2284 0.2837	0.2953 205
0.9325	0.2953 206
0.9489 0.9489 0.8410 0.85101 0.7766 0.7495 0.7546 0.659 0.65	6.2953 207
0.0007 0.000 0.0007 0.0007 0.0007 0.0007 0.2008 0.2008 0.2007 0.2007 0.2007 0.2007 0.2007 0.2007 0.2007 0.2007	0.4914 0.2953 208
0.9489 0.8864 0.840) C.8100 D.7766 C.7494 0.7348 0.660	0.4917
0-2-63 (-4-64)	0.2953 211
A AND A BANK	
	9 0.4921
00,707 00,000 00,000 00,000 00,000	0.2974 213 06 0.4921 0.2954 214
0.9325	
0.9325 0.913Y 0.835Y 0.7855 0.6814 0.2460 0.2287 0.2839 0.9325 0.913 0.9376 0.8358 0.7855 0.6014 0.2764 0.7743 0.7548 0.661 0.9325 0.9489 0.9489 0.8358 0.7855 0.6014 0.7764 0.7453 0.7348 0.666 0.9489 0.9489 0.9489 0.6464 0.7855 0.6814 0.2666 0.2287 0.2839	0,2954 215
0.9325	0.2955 216 37 0.4923
0.9325 0.8993 0.8359 0.7555 0.6814 0.2861 0.2886 0.2860 0.9489 0.9489 0.8404 0.8094 0.7762 0.7692 0.7348 0.66	0.2455 217
0.9489 0.9489 0.8504 0.8094 0.7762 0.7692 0.7348 0.7860 0.9325 0.9156 0.8359 0.7853 0.6614 0.7961 0.2288 0.7260 0.9489 0.9489 0.8603 0.8093 0.7761 0.7347 0.7347	0.2955 218
0.9325 0.9156 0.8359 0.7855 0.8093 0.7761 0.2961 0.2268 0.7347 0.660 0.9325 0.9324 0.8356 0.7853 0.8093 0.7761 0.2961 0.2268 0.2060 0.660 0.9325 0.9324 0.8356 0.7347 0.660	0.2939 218 07 0.4923 0.2956 219 07 0.4929
0.9325 0.9324 0.8356 0.7855 0.6814 0.2961 0.2266 0.2266 0.2860 0.2860 0.666 0.9325 0.9328 0.8337 0.7855 0.7861 0.2961 0.2961 0.2861 0.2861 0.2961 0.2	0.2956 220
0.9128 0.9124 0.744 0.744 0.764 0.7744	A 3064 311
0.9325 0.9489 0.2289 0.8576 0.8576 0.8091 0.614 0.7759 0.2482 0.7546 0.2480 0.7546 0.2481 0.668 0.2481 0.24	0.2956 222
0.9325	0.4922
0.24690.8744 0.8198Q.80900.7757 <u>0.74670.7264</u>	Man 0.4921-

0.9325	825	9.9268	. 50.	0.6356	192	0.7654	10000	0.6613		0.2960		0.2207		0.2842		0.2951	
	D. 9489		0,9136		C. 5401		0.6091		Q.7.755		0.7463		0.7331		0.6594		0,4904
0.9325		0.9130		0.8357		0.7654		0,6413		0.2960		042287		0.2842		0.2951	
0.9325	0.9489		0.7407		0.8402		C. 8091		9.7755		0.7483		0,7331		0.6595		0,4904
0.9325		0.6964		0.6356		0.7554		0.6013		0.2960		0.2267	,	0.2642		0.2951	
	0.9489		0.9489		C. 84C3		C. 8090		C.7755	8	0.7483		0,7331		C. 4595		0.4901
0.9325	_	0.8892		0.4350		0.7854		0.4813		3.2940		0.2267	11	0.2842		0.2951	
0.9325	0.9489)	0.9489		C- 8403		C. 8090		0.7755		0.7483		0.7336	1	0.6599		0-4916
0.9325		0.9040		0.8358		0.7854		0.6613		0. 2969		0.2287	,	0.2842		0.295	
6.9325	0.9489	1	0.4469		C-8401		C-8090)	0.7755		C-7481) _	0.7339)	0.459	1	0.4910
4.9324		0-9204	:::	0. 1111		0. 7854		0.6613		0.2960	· · · · · ·	0.2244	- <u></u>	0. 28 42		0. 295	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
	0.9485	;	0.9489	,	C-A199		0. 8090	1	0.7749		0.7483	1	9.7339		0.6594		0. 491
0.9325		1. 9324		0. 8353		A. 7644	*****	C. AAT		5.2960		C-2286		0.3861	, , , , , , ,	A. 705	,
		,															
0.9325		A. 0158		A X		A. 9864		N. Kata		A. 2441		A > 5'44		W. 3444		A. 304	
007367	0.04.00			000330	104	40			A . 7756		A . 7484		A . 7334				0.401
0.9325	V0 7701		400.00	W. 444.4	V. 0.370	A 4862	U. 0070	X-1263	VA.: 133	A 1041	N	A 23784			0.6271	- 45 de	40.44
0.7325		0.4323		V-0333		00 1034		0.0013	A 7745	002701	. 74.04	V. 62 84	A 7330	V . Z 77Z		0.277	
0.9325	A . A . D .	A 0136	U. 8 70 1	A - 224	Ve 8 3 70	A 9464	0. 507	A 4313	967137	A 3041	V. 176	A - 134	0 6 1 3 3	0 1041	V . 07 74	A 468	0.471
0.4325		0.4353		0.0334		C. 1334		O 001 1		0.5461		U- 2286		0.60-4		V+277	
0.9325	U-748		0,0415		0.0397	1	C. 9040		U. 1.132	445.1			U. /33		A 624		U 0 471
0.4325		0.4312		0-4355		0.7854		0.0913		0.2961		0.2281		U. 2842		U. 275	
	0.748	<u> </u>	0.5744	,	C. 0394		C. 8090	,	0.7755	,	0.7484	•	0.733	,	0.057	7	0.471

APPENDIX VI COMPUTER LISTING

Unchoked Version

	SEY00236,01,RF212-42YA),W.C.MOGER,MSGLEVEL=1.CLASS=C.YIME=4		
//STE			
2	PROGRAM NO. SEROO238	A	2
		A	3
	UNCHOKED FLOW WITH FREE SUBSDNIC EXPANSION.	A	4
	COMPUTATION BASED ON LAX-WENDROFF METHOD.	-	5
:	TIME-DEPENDENT APPROACH TO STEADY STATE.	A .	7
	THE PERCONNECTION OF THE STATE	Ā	8
•	COMMON /PGMNO/ NPROG(5)	Ā	ğ
 •		Ā	10
	DATA KR/8/,K14/14/	A	11
,		A	72
	WRITE (6.1) NPROG	A	13
	WRITE (8.2) KB	A	14
	WRITE (14,2) K14	A	15
;		A	16
	CALL ERRSET (207,256,-1,1)	<u> </u>	17
	CALL ERRSET (208,256,-1,1)	A	16
	CALL ERRSET (209,256,-1,1)	A	19
	CALL CAROLN	-	20
	CALL CARDIN	A	21
	CALL MAINP	A	23
	CALL ENDJOB	-	24
	CALL EXIT	Ā	25
	STOP	A	26
		A	27
; 		A	28
		A	29
		7	-50
	FORMAT ('11',20X, 'PROGRAMME NO. ',5A4/'0',22X, 'REAL GAS TIME-DEPEND	A	31
	TENT UNCHOKED NOZZLE FLOW WITH FREE EXPANSION 1/1	A	32
	FORMAT ['1'+20X+'OUTPUT FROM DATA SET NO.'+13/'0']	A	33
	END	8	34
	FUNCTION BANDIT (X1.X2.X3.X4.X5)	B	- 1
•	CDMMON /FUBAR/ F1.F2.F3.F4.F5	8	3
	Comment of Comment of the Edit Str. Adv. Str.	В	4
	CENTRAL 4-POINT SMOOTHING	B	5
		8	6
	BAN=F1+X1+F2+X2	B	7
	D17=F3+X3+F5+X5	B	- 6
	BANDIT=BAN+DIT	В	•
	BAND[T=BAND[T+F4*X4	8	10
		A	11
	RETURN	8	12
	·	B	13
	END CULTIME REDUAL	B	-13
	SURROUTINE BEDLAM	C	1
	COMPUTE THE MAXIMUM MASS FLOW/AREA AT THE THROAT STATION.	C	3
	TTEDITIN, ACCIDEC CTATIC DECCINE IN CATICES AMAND & N		_
	ITERION, ASSUMES STATIC PRESSURE TO SATISFY DM/DP = 0	Ç	
	TIERIUM. ASSUMES STATIC PRESSURE TO SATISFY OM/DP = 0 USE 3-POINT PARABOLIC FIT	Č	5

•	COMMON /FLIGNR/ WEIGHT, PTHROT, PANIC	C	
	COMMON /COUNT/ L.LL	-č	•
	COMMON /EROS/ W(21,60,4),P(21,60)	ç	
	COMMON /NERO/ MF.NF.NT	č	
	COMMON /STAG/ AA(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21)		
	1,PZ(21),TZ(21),HZ(21),RHOZ(21)	č	-
		č	
	OIMENSION A(3), X(3), Y(3)	C	
;		C	
	ZERO=0.0	C	
;		_C	
	CALL PMIN (PANIC)	C	
<u>:</u>		C	
	XLOW=0.34PANIC	C	
	DELX=0.005000001*PANIC	C.	
	•	C	
	JERK=0	C	
•	COMPUTE FIRST THREE POINTS	C	
	00 1 K=1.3	C	
	X(K)=XLOW+(K-1)+DELX	C	
	CALL SETHP (X(K),NT)	C	
	Y(K)=XMASS(NT)	Ç	
	CONTINUE	<u> </u>	
•		C	
		Č	
	JERK=K CALL PARAR (X,Y,A) JF (A(3).EQ.ZERQ) A(3)=1.0D+69 XTEST=-0.5*A(2)/A(3) 1F (A(3).GE.ZERQ) GO TO 3 1F (A(3).EQ.ZERQ) GO TO 3	C	
	GALL PARAM (X,Y,A)	. <u>C</u>	
	JF (A(3).EU.ZERU) A(3)=1.0D+69	Č	
	AIC31=-0.074(21/A(3)		
	IF ((X(1)-LE-XTEST)-AND-(X(3)-GE-XTEST)) GO TO 4	Č	
	10 11A11/3LE3A1E31/3AND.TA13/3DE3A7E31/1 GU TU 4		•
•	X(1)=X(2)		
	X(1)=X(2) Y(1)=Y(2)	č	
	X(2)=X(3)	č	
		Č	-
	X(3)=X(3)+DELX '	č	
-		č	
	CALL SETWP (X(3),NT)	č	
	Y(3)=XMASS(NT)	Č	
!	CONT INDE	Č	
_		C	_
3	CONTINUE	Č	
:	NA CALITAN	Č	
	CALL BOMBER ('BEDLAM', JERK)	C	
	RETURN	C	
<u>:</u>		C	
,	CONTINUE	C	_
:	SOLUTION FOUND	Č	
	CALL SETWP (XTEST,NT)	Č	
	WEIGHT=XMASS(NT)	C	
	DTMPNT=YTEST	•	
<u>: </u>	COMPUTE PRESSURES CORRESPONDING TO CHOKED FLOW.	L	_
	CALL PHINDU (1)	C	
	CALL PHINOU (NF)	C	

	PS[A]=P(1,1)/144.0	C	64
	PSIAL=P(1,NF)/144.0	_ C_	65
	PPOI=P(1,1)/PZ(21)	_ C _	66
	PPDL=P(1,NF)/PZ(21)	C	67
	POT=PTHROT/PZ(21)	C	6 B
	CALL HEAD6	C	69
	WRITE (6,5)	C	70
	WRITE (6,7) WEIGHT, PTHROT, PANIC	č.	71
	WRITE (6,6) POT, PSIAI, PPDI, PSIAL, PPOL	C	72
С		č	73
<u> </u>	RETURN	č	74
c	RETURN	č	75
ᠸ		-	76
=	CODMAT 1/20V I COMOTTIONS COD CHONED STOL AT MINIMUM ADEA ! / }	Č	77
<u> </u>	FORMAT (/20x, CONDITIONS FOR CHOKED FLOW AT MINIMUM AREA ' /)	_	
6	FORMAT (/20x, THROAT P/PO =1, F7.4, 3x, TINLET PRESSURE =1, F8.3, TP	Č	78
	_ ISIA) + -3x - + P/PO = + - + F9 - 4 - / - 20x - + EXIT PRESSURE = + - + F8 - 3 + + (PSIA) + - 3x - + P	Ç	79
	2/PD =1,F9.4 /)	С	80
7	FORMAT (/20x, "WEIGHT=",1PG15.6,3x, "PTHROT=",G15.6,3x, "PANIC=",G15	_ C_	81
	1.6 /)	C	B2
	END	C	B3
	SUBROUT INE BNDRY	D	1
C		D	2
	COMMON TOELTAST DX, DY, DT, DY2, DT2, DT4	D	3
	COMMON /SUPER/ R(21.60)	Ď	4
	COMMON /SPUR/ 5(60).50(60).50P(60).51(60).51P(60).AREA(60)	. p	5
			_
	_ COMMON /NERD/ MF.NF.NT.MUFF.LIMIT	D.	_ 6
	COMMON /EROS/ W(21,60,4),P(21,60)	D	7
		_ D	8
	COMMON /FRAN/ AT(60),AI(60),BD(60),BI(60)	D	9
	DIMENSION PP(100)	D	10
C	And the state of t	D	11
Č	COMPLITE OUTER BOUNDARY PRESSURES	D	12
	DD 1 K=1.60	Ð	13
1	PP(K)=P(MF,K)	D	14
1 C		D	15
•	DO 2 K=2.LIM(T	Ď	16
	X=W(MF,K,2)**2/W(MF,K,1)	0	Ť
	X=X/SD(K)	Ď	18
	DP=0.5*(PP(K+1)-PP(K-1))	Ď	19
		=	
	CORR=BO(K) *DP-AO(K) *X	D	20
	P(FF,K)=P(MF-1,K)+CORR	D	21
2	CONTINUE	D	22
	DD 3 K=2,LIMIT	ס	23
	\$OP<=\$OP(K)	D	24
	DINGLE=ONF+SOPK**2	D	25
	DANGLE=SORTF(ONE/OINGLE)	D	26
	CALL GRONK (ONE,P(MF,K),RHO,VEL,EASY)	D	27
	W(MF,K,1)=RHD+R(MF,K)	D	28
	W(PF.K.2)=RHO*R(MF.K)*VEL*DANGLE	- 5-	-29
	W(MF,K,3)=W(MF,K,2)*SOPK	Ď	3 D
_		Б	31
,	W(MF,K,4)=EASY*R(MF,K)	_	
	D0 4 K=1,60	D	32
•	PP(K)=P(1,K)	Đ	33
	DO 5 K=2.LIMIT	D	34
	X=W(1,K,2)**2/W(1,K,1)	D.	35
	X=X/SI(K)	D	36

	DP=0.5*(PP(K+1)-PP(K-1))	Ō	37
	CORR=BI(K)+OP-AI(K)+X	D	.38_
5	P(1,K)=P(2,K)+CORR	D	39
<u> </u>			40_
	DO 6 K=2.LIMIT		41
	SIPK=SIP(K)	0	42
	DINGLE=DNE+SIPK++2	D	43
	DANGLE=SQRTF(ONE/DINGLE)	0	44
	CALL GRONK (ZERD,P(1,K),RHO,VEL,EASY)	0	45
	W(1,K,1)=RHO+R(1,K)	0	46
	W11,K,2)=RHO*R(1,K)*VEL*OANGLE	0	47
	W(1,K,3)=W(1,K,2)*SIPK	0_	48
_6	W(1,K,4)=EASY*R(1,K)	0	49
С		D	50
	RETURN	`o `	51
	END	D	52-
	SUBROUTINE BOMBER (NAME, KODE)	Ε	1
C		Ē	2 .
	DIMENSION NAME(2)	Ē	3
C		Ě	4
	WRITE (6,1) NAME(1), NAME(2), KODE	Ē	- 5
	CALL EXDUDE	Ē	6
	CALL EXIT	-Ē.	~ ~ ~
	RETURN	Ē	8
	RETURN	ŧ	- a -
č		Ē	10
-ř	FORMAT (/20%, 'BOMB-OUT TN' ', 244, 3%, 'CODE=', 15/)	٠ .	- ii
	END	E	12-
	SUBROUTINE CAROTN	. 5	. =
		_	1
	COMMON /SPY/ KCLASS.KGROUP	<u>-</u> -	2
•	DIMENSION KARD(20)	ŗ	3
	CALL DEMON	. Է.	
	READ (5,3) KCLASS, KGROUP	F	5
	WRITE (6.8) KCLASS, KGRDUP	_F_	
	CALL PCLASS	F	7
	DD 2 K=1.6969	F	8
	READ (5,4,END=9) KARD	F	9
	JF (MDD(K-1,50).NE.0) GD TO 1		10
	CALL FULO	F	11
	WRITE (6,7)	F.	12
_i	WRITE (6,5) KARD,K	F	13
2	CONTINUE	F	14
	REWIND 5	F	15
-	WRITE (6.6)	F	16
	RETURN	F	· 17 -
C		F	18
<u>3</u>	FORMAT (1615)	F	19
4	FORMAT (20A4)	F	20
5	FORMAT (10X,20A4,3X,15)	É	21
6	FORMAT (2x,50('*'),' END OF INPUT DATA ',50('*'))	E	22
- }	FORMAT (18X, " INPUT DATA CARO IMAGE PROGRAM NO. SEROD142 7)	F	
-	FUNDAL 1/20A 15 COURT P 1/40 AND 1740 PRUBLAN NU. SERVUITZ" /)	Ē	23
	FORMAT (/20X, SECURITY CLASS AND GROUP CLASS=1,15, GROUP=1,15/)	F	24
	END	F	25-
	SUBROUTINE COVO (CLAP, VENUS, PUNTZ, NASTY)	Č	
C	A. A	G	2
<u>č</u>	AT A GIVEN X-STATION.	Ğ	3

C	COMPUTE DISCHARGE COEFFICIENT-CD AND THRUST COEFFICIENT-VO.	G	5
	COMMON /EROS/ H(21,60,4),P(21,60)	G	6
	GOMMON /DELTAS/ DX,OY,DT	G	_ 7
	COMMON /NERO/ M.N.NT.MUFF	G.	8
	COMMON /SPOR/ S(60)	G	9
	COMMON /SUPER/ R(21,60)	G	10
<u> </u>		G	11
	NX=NASTY	- G	12
<u>c</u>	•	Ğ	13
	CD=(W(M,NX,2)+W(1,NX,2))+0.5	Ğ	14
	VD=(W(M,NX,2)**2/W(M,NX,1)+W(1,NX,2)**2/W(1,NX,1))*0.5	Ğ	15
	PUNE=(P(M.NX)=R(M.NX)+P(1.NX)+R(1.NX))+0.5	G	16
С	PUNC=(P(M;NA)=R(M;NA)=P(1;NA)=R(1;NA)=U0-)	G	17
<u> </u>		G	18
		G	19
	CD=CD+W(K+NX+2)		_
_	VO=VD+W(K+NX+2)++2/W(K+NX+1)	G	20
1	PUNE=PUNE+P(K,NX)*R(K,NX)	G	21
C		G	55
	SEX=S(NX)+DY+2.0	G	23
	CLAP=SEX*CD	G	24
	VENIJS=SEX+VD	G	25
	PUNT Z = PUNE + SEX	G	26
Ç	•	Ğ	27
•	RETURN	Ğ	28
С	NE COMP	Ğ	29
<u> </u>	END .	Ğ	30-
	= 17	н	
c	SUBROUTINE CHECK	ਜ਼	2
	COMPART THE MARK COME STRUCKED AT THE SAME AND THE STATE		
<u>c </u>	COMPUTE THE MASS FLOW EITHER AT THE ENTRANCE OR EXIT-	H	3
<u>c · </u>	PANZY > O ENTRANCE PSIA GIVEN	н	-4
<u>C</u>	PANZY < O EXIT PSIA GIVEN	H_	_ 5
C	the state of the s	Н_	6
	READ (5,4) PANZY,PZ,GAMMA	н	7
	WRITE (6.2) PANZY.PZ.GAMMA	н	- 8
	IF (PZ.EQ.O.O) GO TO 1	н	9
	PANZY=SIGN(PZ*PRAT(PANZY,GAMMA),PANZY)	н	10
1	PS1A=PANZY	н	11
	PANZY=PS1A+144.0	н.	12
	WRITE (6.3) PSIA.PANZY	H	13
c		н	14
·	CALL FIRST (PANZY)	H	15
	CALL DOWN (-PANZY)	- ii	- 16
_	CALL DOWN (-PANZY)	H	17
<u>c</u>		_	
_	RETURN	H	18
ç		H	19
	51 52 63 63 63 63 63 63 63 63 63 63 63 63 63	H	20
2	FORMAT (/20x, PANZY=1, F10.4, 3x, PZ=1, F10.3, 2x, GAMMA=1, F7.3/)	Н	21
3	FORMAT (/20x, P(IN/DUT) = 1,F10,4, (PSIA) 3x,F10,2, (PSFA) /)	Н	22
4	FDRMAT (6E12.0)	н	23
	END	н	24-
	SUBROUTINE CIPORT (PO.TO.OEN.FUZZ.PSTAT.TEMP.VEL.EASY)	ī	1
c	INPUT COMPUTED	. 1	2
Č		i	3
c -	COMPUTE STATIC PROPERTIES FOR A GIVEN STATIC DENSITY.	—- і -	
			5

<u> </u>	PD = SYAGNATION PRESSURE	1 6
<u> </u>		T7
<u> </u>	DEN = STATIC DENSITY	1
	FUZZ = STREAMLINE	1 9
		1 10
<u>: </u>		I 11
	COMMON /LIMITS/ VMIN	1 12
	COMMON /THERMO/ CPX(3),CVX(3),RAG	1 13
;		1 14
	CONTINUE	I 15
	ZERO=0.0	1 16
		1 17
	P2=P0	1 18
	TZ=TO	1 19
	RHQ=DEN	1 20
	F=FUZZ	Į 21
-		1 22
	RRATIO=RHO*RAG*TZ/PZ	1 23
		7 24
	T = HANKY(CVX,RRATID,TZ,RAG) ++++++++++++++++++++++++++++++++++++	1 25
	AZ=CVX(1)	1 26
	A1=CVX(2)	1 27
	A2=CVX(3)	1 28
	X=RRATIO	1 29
	RGAS=RAG	I 30
	POWER=RGAS/AZ	1. 31
	FUNGE=X++POWER	1 32
		1 33
	TRAF=A2+0.5/AZ	1 34
:-	LET FIRST GUESS FOR T = TZ	36
•	T=T2	1 37
	.nq 2 K=1,5	1 38
	TTZ=T/TZ ·	1 39
	EPAR=(TZ-T)+(BARF+(TZ+T)+TRAF)	1 40
	XLAX=EXP(EPAR)	1 41
	TRAT=XLAX#FUDGE	1 42
	COMPARE "TRAT" WITH =TTZ"	1 43
	TCOMP=TRAT+TZ	1 44
	ERROR=TCOMP-T	45
	T=TCOMP	1 46
	CONTINUE	1 47
		1 48
-	PRES=T*RHO*RAG	1 49
		1 50
•	DH=HOTS (CPX+T+TZ)	1 51
	VELOC=SORTF(DH+OH)	i 52
	VELOC=AMAXI (VELOC,VMIN)	53
	HO=HZERO(F)	1 54
	E=HO*RHO→PRES	1 55
		1 56
•	PSTAT=PRES	i 57
	VEL=VELOC	58
	EASY=E	1 54
	TEMP= T	1 60
:		1 61

	RETURN	1	62
<u> </u>	END	. 1	63_
	2.12	1	64-
- <u>c</u> -	SUBROUTINE CPEVAL .	- 1-	- 1
C	COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8)	Ĵ	3
C	COMMING TOPPATAT CP (1240) YMTH (074 MANGE (07	Ť	4
•	DATA KRUD/'PERF'/	J	5
	DIMENSION X(8). Y(8)	J	6
C	CP ARRAY	J	7
Č	1 - AIR 5 - 02	·- j ·	8 -
C	2 - CO2 6 - N2	J	9
С	3 - CO 7 - ARGON	J	10
c	4 - H2O 8 - H2	J	11
C		J	12
	INTEGER+4 LBMASS(4)/'CP(B','TU/L','BMAS','S-R)'/	_ 3	13
	* LBMOLE14)/'CP'(B', TU/L', 'BMOL', 'E-R)'/	J	14
	# , KGAMMA14)/'CP/C',"V GA","MHA "," '/	<u> 1</u>	15
Č		j	16 17
c	READ 15,10) NOMEN, ADDA	J	18
C	KEAD 13410) NUMENTADDA	J	19
`	IF (NOMEN.NE.KRUD) GO TO 3	J	20 -
	00 2 J=1,8	J	21
	DO 1 K=2,3	Ť	22
1	CP(K,J)=-0.0	J	23
· c -		j	24
ž	CONTINUE	Ĵ	25
_	CP(1,1)=0,24009	j	26
<u>C</u>	•	J	27
3	CONTINUE	J	2.9
	NC P= 19	J	_29
_	R=1.98726	J	³⁰
_ <u>c</u>		J	31
_	CALL HEADS	j	32
<u> </u>	WRITE (6,11)	J	33
C	MKILE (011)	J	35
	WRITE (6,12) (K,NAME(K),WTH(K), (CP(J,K),J=1,3),K=1,8)	"	36 -
_ <u>c</u>	MALLE LOGIES (MANAGELY) AMERICAN LOS	.i	37
	WRITE (6.14) NAME LBMASS	J	38
C		J	39
	DO 5 J=1.NCP	Ť	40
	A=J-1	J	41
	A=A+ADDA	J	42
	T=A+100.0	J	43
	00 4 K=1;8	J.	44 -
	X(K)=CP(1,K)+T+(CP(2,K)+CP(3,K)+T)	J	45
4	CONTINUE .	J	46
Ċ.		j	47
	WRITE (6,13) T,X,T	J	48 49
5 1	1F (MDD(J,5),EQ.0) WRITE (6.16) CONTINUE	7	50
Č	GUAL FUM.	J	51
<u> </u>	WRITE (6,15)		52
	WRITE (6.14) NAME I RING F	ŭ	53

C	DO 7 J=1.NCP	1	54 59
	A=J=1	- - j-	-5
			5
	A=A+AODA T=A+100.0	- <mark>J</mark> .	- 5
		_	_
	DD 6 K=1,8	ᆚ	5
	X(K)=CP(1,K)+T*(CP(2,K)+CP(3,K)*T)	ì	6
	X(K)=X(K)+WTM(K)	J	6
6	CONTINUE	J	4
<u>c</u>		J .	6
	WRITE (6,13) T,X,T	J	6
	IF (MOD(J,5).EQ.O) WRITE (6.16)	J	6
7	CONTINUE	J	6
С		J	6
Ċ		٠ آ	6
•	WRITE (6,14) NAME, KGAMMA	J	6
c	WAZIE TOULT NAME WORMAN	-j.	7
·			
	OD 9 J=1,NCP	-} -	-7
	A=J-1	_	7
	A=A+ADDA	٠,١	7
_	T=A*100.0	J.	. 7
<u>c</u>		J	7
	DO 6 K=1,8	J	7
	X(K)=CP(1,K)+T+(CP(2,K)+CP(3,K)+T)	<u> </u>	_7
	X(K)=X(K)+WTM(K)	J	7
	FUZZ=X(K)-R	J	7
	Y(K)=X(K)/FUZZ	J	8
8	CONT INUE	J	8
c —		J	8
_	WRITE (6,13) T,Y,T		8
	IF (MOD(J.5).EQ.Q) WRITE (6,16)	-3	8
С		J	8
9	CONTINUE	-j	8
ć	COVI INC.	ĭ	8
<u> </u>	RETURN		- 8
С	RETURN	j	
			8
<u>c</u>	•	_	9
<u>c</u>		J	9
10	FORMAT , (A4,E16.0)	J	9
11	_ FORMAT _ (! !,20x, 'CP DATA' _//20x, 'COEFFICIENTS FOR CP(BTU/LB.MASS)	J	9
	1= F(T-RANKINE)	J	9
12_	FORMAT (/10x.15.2x.A4.0PF10.3.1P3G15.6)	J	9
13	FORMAT (10x, F8.1, 5x, 8F9.4, 2x, F8.1)	Ĵ	9
14	FORMAT (/12X, 'RANKINE', 8X, 8(A4, 5X), 2X, 4A4/)	J	9
15	FORMAT ('1')	J	9
16	FORMAT ('')	J.	ģ
	END		10
	FUNCTION CSUBP (TEMP)	K	10
	COMMON /THERMO/ CP(3).CV(3)	ĸ	-
	T=TEMP	_	
		K	
	0-0-117-1-10-127-0-137-17	K	
	CSUBP=C	K	
_	RETURN	K	
C		_K	
C		K	-
	ENTRY CSUBV(TEMP)	K	

	COMPUTE CV AS A FUNCTION OF TEMPERATURE.	K
_	THEEMP	K
	C=CV(1)+T+(CV(2)+CV(3)+T)	K
_	CSUBY=C	K
	RETURN	K
	END	K
	SUBROUTINE CYCLE	Ĺ
_		Ī.
	COMMON /DELTAS/ DX,DY,DT,DY2,DT2,DT4	ī
	COMMON /DUPER/ HA(21)+HB(21)	ι
	COMMON /EROS/ W(21.60.4).P(21.60)	L
_	COMMON /FANG/ F(9,4),G(9,4)	T
	COMMON /FURD/ WNORTH(4).WSOUTH(4).WWEST(4).WEAST(4)	Ū
_	COMMON /NAVIER/ DTDX,0TDX2.DTDX4.DTDX8.DTDY.DTDY2.DTDY4.DTDY8	L
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT	L
	COMMON /STOKES/ A(60),8(60),H(60)	L
	COMMON /STUP(D/ FUZZ(2),60)	L
		L
	9-POINT GRID COMPUTATION SCHEME 4-POINT AT DT/2	Ł
		L
	78 9	L
		L
	NORTH 2	L
	5. 700	L
	4 WEST 5 EAST 6 3 X 4	L
		L
	SOUTH 1	L
•		L.
	1 2 3	L
		L
		Ļ
	00 4 M=2,MUFF	L
_	Y=HB(M)	
	on a way a sure	
	DO 3 N=2,LIMIT	
	HN=H(N)	
_	EAST=A(N+1)*Y+B(N+1)	
	WEST=A(N-1)+Y+B(N-1)	-
_	ANYB=A(N)+Y+B(N)	-
	YANKEE=ANYB+FUDGE	
_	REBEL = ANYB-FUNGE	┷
	**************************************	ì
	CALL SNAFU (M.N)	1
	CALL STATUS STATES	ř
	00 1 K=1.4	ì
	IN T W-FEA	1
_	F64=F(6,K)-F(4,K)	-
	GR2=(G(R,K)-G(2,K))+HN	ì
	F82=(F(B,K)-F(2,K))*ANYB	
	F04-1F10442-F144417-4410	
-	COMPUTE NORTH POINT	
	WRAR={W(M,N,K)+W(M+1,N,K))+0.5	
_	FX=(F64+F(9-K)-F(7-K))*DYDXB	
	FA=1FQ=+F 70A/=F 10A/J+U UAO	

	Y={G(8,X)-G(5,K))+HN	L :	50
	NORTH(K)=WBAR+FX+GY-FY	! L_ _!	51
		<u>-</u> :	52
	DMPUTE SOUTH POINT	ֈ _ !	53
-	BAR=(H(M,N,K)+H(M-1,N,K))+0.5		54
F	X=(F64+F(3,K)-F{1,K))+DTDX8		55
	Y=(F(5,K)-F(2,K))*REBEL	L	56
	V-ICIE VI.CIO VIIALLE	i i	57
	SOUTH(K)=WBAR+FX+GY-FY	_ [.]	58
		1. 3	59
	OMPUTE EAST POINT		60
	BAR=(W(M,N+1,K)+W(M,N,K))+0.5	-	61
	X=(F(6,K)-F(5,K))*DTDX2		<u>62</u>
	Y=(F(9,K)-F(3,K))*EAST	_	63
	Y=(G(9,K)-G(3,K))*H(N+1)	-	64
		_	
:	EAST(K)=HBAR+FX+(GY+G82-FY-F82)+0.25		65
		_	66
	OMPUTE WEST POINT		<u>67</u>
	BAR=(W(M,N-1,K)+W(M,N,K))+0.5	-	68
	X=(F(5,K)-F(4,K))+DTDX2	_ ~	69
	Y=(F(7,K)-F(1,K))*WEST	į į	70
	Y=(G(7-K)-Ġ(1-K))+H(N-1)	L	71
	WEST(K)=WBAR+FX+(GY+G82-FY-F82)+0.25	- i	72
·			73
	NORTH(3)=WNORTH(3)+DT4*(P(M,N)+P(M+1,N))		74
·	SOUTH(3)=WSOUTH(3)+DT4+(P(M,N)+P(M-1,N))		75
 :	30010137-8300101374014-1619774-161977		76
	EAST(3)=WEAST(3)+DT4*(P(M,N)+P(M,N+1))	_	
	<u>WEST(3)=WKEST(3)+DT4*(P(M,N)+P(M,N-L))</u>		77
			78
	ALL EVAL (WNORTH-2,(FUZZ(M-N)+FUZZ(M+1,N))+0.5)		<u>79</u>
	ALL EVAL (WSOUTH,1,(FUZZ(M,N)+FUZZ(M-1,N))+0.5}		RÖ
	ALL_EVAL_(HEAST,4,(FUZZ(M,N)+FDZZ(M,N+1))#^.5)		31
(ALL_EVAL_(WEAST,4,(FUZZ(M,N)+FUZZ(M,N+1))*^.5) ALL_EVAL_(WHEST,3,(FUZZ(M,N)+FUZZ(M,N-1))*0.5)	L .	82
	•	L	83
	00 2 K=1.4	∃ ا	84
	X=(F(4,K)-F(3,K))*DTDX	L	85
	Y=(F(2,K)-F(1,K))*ANYB		86
		_	87
· ·	Y= G(2,K)-G(1,K))+HN (M-1,N-1,K)=W(M,N,K)+FX+2.0+(GY-FY) (M-1,N-1,3)=W(M-1,N-1,3)+P(M,N)+DT	— : ·≬	88
			89
	(M-1,N-1,3)=K(M-1,N-1,3)+P(M,N)*DT		90
		_	
	ONTINUE		91
	ONT (NUE	-	92
	ALL WEIRDO		93
		L .	94
	ETURN	[[95
	NO The state of th	ַ װּ	96
	UBROUTINE DEMON	Ä	1
	MPLICIT REAL+8(A-H,O-Z)	M	7
,	OMMON /APE/ D(10) ARONUM WEEKDY KOATE(3)	M	3
··}	EAL+8 THTES(7)	n	4
'	CALTO INITALIA		100
	/ TUESDAY . " WEDNSOY THURSDY FRIDAY	M	5
	, 'SATURDY', SUNDAY ', MONDAY '	19	0
	NTEGER MONTH(13)/ ' JAN', ' FER', ' MAR', ' APR', ' MAY', ' JUN'	<u> </u>	. ?
	' JUL', ' AUG', ' SEP', ' DCT', ' NDV', ' DEC'/	M.	8
	NTEGER JERK(12)/31,28,31,30,31,30,31,30,31,30,31/	м	ç

	INTEGER LUSH/*1900*/ , LULU/* 00.*/	- 14	•	
	The state of the s	M	10	
	CALL GETWHO (ARONUM, KYEAR)	II -	. 1	
	KDAY=MOD(KYEAR,1000)	M	1	
	KYEAR=KYEAR/1000 IF(MDD(KYEAR-4) .EQ. 0) JERK(2)=29	M	.13	_
•		M	-14	
	L = KYEAR - 69 J = L/4 + L + KDAY	M	1	
	J = L/4 + L + KDAY L = MOD(J.7) + 1	Ä	14	
			1	
	WEEKDY=TWTFS(L)	H	1	
	K=KDAY	M	19	
	00 1 J=1+12 ·		20	
	N=J	<u> </u>	2	
	IF (K.LE.JERK(J)) GO TO 2	M	2	
1	K=K-JERK(J) .	. "A	2	
	K=0		24	
2	M=13	. M	2:	
~	MUNTH=MONTH(M)		2	
	KOATE (1)=MUNTH	M	2	
	KDATE(2)=LULU+256+([K/10)+256+MOD(K,10))	M	21	
	KOATE(3) = LUSH + 256+(KYEAR/10) + MOD(KYEAR+10)	-	.29	
	RETURN	M	3(
	END	_ M	3	
•	SUBROUTINE DOOOLE	N		1
	COMMON /EROS/ W(21,60,4),P(21,60)	N N		2
•	COMMON /FLIGHT			3
	COMMON /NERD/ MF.NF.NT.HUFF.LIMIT	_ N_		
	COMMON /STUPIDA F(21,60)	N	-	5
	COMMON /SUPER/ R(21,60)	N		<u>.</u>
	DATA ZERD/0.0/, ONE/1.0/, BIGGY/0.01/, SMALL/-0.01/, HUGE/1.69E+12/	N		7
	DD 2 J=2,CIMIT .	N_		<u> </u>
•	REL=(WEIGHT-XMASS(J))/WEIGHT	- N		9
	00 1 K=1,MF	_ <u>K</u>	- 10	
	FACTER=RIDDLE(K.J)	N	1	_
	IF (FACTER.EO.ZERO) FACTER=HUGE	N	_ 13	
	EPAR=REL/FACTER	N	1.	
	IF (EPAR.GT.BIGGY) EPAR=BIGGY	N	_14	
	IF (SMALL.GT.EPAR) EPAR=SMALL	N	1	_
1	W(K,J,1)=W(K,J,1)+(DNE+EPAR)	. N	. 14	
2	CONT I NUE	N	1	
	CALL ROGUE	. N	11	_
	DD 4 K=1, MF	N	1	
	00 3 J=2.LIMIT	N	- 21	
			-	
	FUZZ=F(K,J)	N	2	Ι
	FUZZ=F(K,J) RHO=W(K,J,1)	N	2	2
	FUZZ=F(K,J) RHO=W(K,J,1) RMAX=D.995*RHOMAX(FUZZ)	N N	. 2	1 2 3
	FUZZ=F(K,J) RHO=W(K,J,1) RMAX=D.995*RHOMAX(FUZZ) RHO=DUMDUM(RHO,RMAX)	. N N	. 2:	2 3
	FUZZ=F(K,J) RHO=W(K,J,1) RHAX=D.995*RHOMAX(FUZZ) RHO=DUMDUM(RHO,RMAX) CALL FONKY (FUZZ,RHO,PSTAT,VEC,EASY,TANG)	- N	2.2	1 2 3 4 5
	FUZZ=F(K,J) RHD=W(K,J,1) RMAx=D,995*RHOMAX(FUZZ) RHD=DUMDUH(RHD,RMAX) CALL FONKY (FUZZ,RHD,PSTAT,VEE,EASY,TANG) TANG=W(K,J,3)/W(K,J,2)	. N N	2:	1 2 3 4 5 6
	FUZZ=F(K,J) RHD=W(K,J,1) RMAx=D,995*RHOMAX(FUZZ) RHD=DUMDUM(RHD,RMAX) CALL FONKY (FUZZ,RHD,PSTAT,VEC,EASY,TANG) TANG=W(K,J,3)/W(K,J,2) CUSN=DNE/SORTF(UNE+TANG**Z)	N N N N N N N N N N N N N N N N N N N	2: 2: 2: 2: 2: 2:	2 3 4 5 6 7
	FUZZ=F(K,J) RHO=W(K,J,1) RMAx=O.995*RHOMAX(FUZZ) RHO=DUMDUM(RHO.RMAX) CALL FONKY (FUZZ.RHO.PSTAT.VEC.EASY.TANG) TANG=W(K,J,3)/W(K,J,2) CUSN=UNE/SORTF(UNE+TANG**Z) W(K,J,1)=RHO*R(K,J)	N N N N N	2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2: 2	1 2 3 4 5 6 7 8
	FUZZ=F(K,J) RHO=M(K,J,1) RMAX=D.995*RHOMAX(FUZZ) RHO=DUMDUM(RHO,RMAX) CALL FONKY (FUZZ,RHO,PSTAT,VEC,EASY,TANG) TANG=M(K,J,3)/M(K,J,2) CUSN=UMP/SORTF(UME+TANG**Z) M(K,J,1)=RHO*R(K,J) W(K,J,2)=W(K,J,1)*VEL*COSN	N N N N N N N N N N N N N N N N N N N	2: 2: 2: 2: 2: 2: 2: 2:	1 2 3 4 5 6 7 8 9
	FUZZ=F(K,J) RHD=W(K,J,1) RMAx=D,995*PHOMAX(FUZZ) RHD=DUMDUM(RHD,RMAX) CALL FDNKY (FUZZ,RHD,PSTAT,VEC,EASY,TANG) TANG=W(K,J,3)/W(K,J,2) CUSN=UNE/SDRTF(UNE+TANG**Z) W(K,J,1)=RHO*R(K,J) W(K,J,2)=W(K,J,1)*VEL*COSN W(K,J,3)=W(K,J,2)*TANG	N N N N N N N N N N N N N N N N N N N	2: 2: 2: 2: 2: 3:	234567890
	FUZZ=F(K,J) RHD=W(K,J,1) RMAX=D.995*RHOMAX(FUZZ) RHD=DUMDUM(RHD.RMAX) CALL FONKY (FUZZ,RHD.PSTAT,VEC,EASY,TANG) TANG=W(K,J,3)/W(K,J,2) CUSN=DNF/SOXTF(DNE+TANG**Z) W(K,J,1)=RHO*R(K,J) W(K,J,2)=W(K,J,1)*VEC+COSN W(K,J,2)=W(K,J,2)*TANG W(K,J,4)=EASY*R(K,J)	N N N N N N N N N N N N N N N N N N N	2: 2: 2: 2: 2: 3: 3:	1 2 3 4 5 6 7 8 9 0 1
3	FUZZ=F(K,J) RHD=W(K,J,1) RMAx=D,995*RHOMAX(FUZZ) RHD=DUMDUH(RHD,RMAX) CALL FDNKY (FUZZ,RHD,PSTAT,VEC,EASY,TANG) TANG=W(K,J,3)/W(K,J,2) CUSN=DNE/SDRTF(UNE+TANG**Z) W(K,J,1)=RHO*R(K,J) W(K,J,2)=W(K,J,1)*VEL*COSN W(K,J,3)*W(K,J,2)*TANG W(K,J,3)*W(K,J,2)*TANG W(K,J,3)*W(K,J,2)*RANG W(K,J,3)*PSTAT	N N N N N N N N N N N N N N N N N N N	2: 2: 2: 2: 3: 3: 3:	23456789012
3 4	FUZZ=F(K,J) RHD=W(K,J,1) RMAX=D.995*RHOMAX(FUZZ) RHD=DUMDUM(RHD.RMAX) CALL FONKY (FUZZ,RHD.PSTAT,VEC,EASY,TANG) TANG=W(K,J,3)/W(K,J,2) CUSN=DNF/SOXTF(DNE+TANG**Z) W(K,J,1)=RHO*R(K,J) W(K,J,2)=W(K,J,1)*VEC+COSN W(K,J,2)=W(K,J,2)*TANG W(K,J,4)=EASY*R(K,J)	N N N N N N N N N N N N N N N N N N N	2: 2: 2: 2: 2: 3: 3:	234567890123

		N 35-
_		<u>0 1</u> 0 2
•		
		. .
_		n 5 0 6
		0 7
		0 8
		0 9
_	WRITE (14)57	0 - 10 -
		0 11
		0 12
		0 13
		0 14
	DETUDN	0 15
		0 16
		0 17
		Ö 18
		0 19
-		0 20
		0 21
		0 22
		0 23
		0 24
		0 25
		0 26
		0 27-
		P 1
	•	P 2
	CHMMON /COUNT/ L,LL	3
		P 4
		P 5
	CALL HEADS	P 6
	BRITE (A.A)	P 7
		P 8
	WRITE (6.5)	P 9
		P 10
	CALL CDVD (CDT, VDT, PUNTZ, NT) IF (L.NE.O) GO TO 1	P 11
		P 12
		P 13
	DD 2 KE1.4F	P 14
		P 15
	AX=A/CDT	P 16
		P' 17
	8X=8/VDT	P 18
		P 19
	· · · · · · · · · · · · · · · · · · ·	P 20
	THRUST=\$UM+3.141593	P 21
		P 22
	DOTE 14.41 MC AV AVV. B. BV. BVV DIMITT THORICT V	P 23
	IF (K.EQ.NT) WRITE (6,7)	P 24 P 25
		P 26

	INTS ¹ /)	1151	29
		_	_
	FORMAT (10X,1PG14.5,0PF10.5,4X,F10.5,4X,1P5G14.5,1X,12)	P.	30
7	FORMAT (/16x, 'WF', 11x, 'WF/WF*', 6x, 'WF/WF1', 9x, 'VO', 11x, 'VD/VD+', 7	P	31
	1X,'VO/VD-1',9X,'PD',11X'THRUST(LBF)'/}		32
6	FORMAT (/20X, ITERATION NO.=",15/)	P	33
7	FORMAT ('+',5X,*THROAT')	P	34
	END	P	35-
	SURROUTINE EQUATE (K,J.NERD)	0	1
	DIMENSION K(1), J(1)	õ	2
	N=NERD	- 7	3
		Ö	_
	00 1 L=1+N	Q	4
1	K(1)=J(L)	0	5
-	RETURN	۵	6
	END	0	7-
	"SUBROUTINE EVAL"(A.ISW.ATE)"	R	1
<u>: </u>	SWIND THE CIRC CHILDREN	R	Ž
<u> </u>	COMMON / FANCY F (9.4) 6 (9.4)		3
_	CUMMON FRANCE F19449, G1944)	~	_
	VASS 1,3VF3M44	R	4
	DIMENSION A(4)	R	5
C		R	6
	ZERO=0.0	R	7
	ETA=ATE .	R	8
c		R	9
L	15 4444 NG 1550 AG 75 i		
	IF (A(1).NE.ZERO) GO TO 1	R	10
	22=2ERO	R	11
	23=2ERO '	R	12
	PR=ZERO	R	13
	GO TO 2	R	14
c		R	15
_	CONTINUE		
<u> </u>	CONTINUE	R	16
	22=A(2)/A(1)	R	17
	23=A(3)/A(1)	R	18
	HO=HZERO(ETÁ)	R	19
	PR=HN+A(1)-A(4)	R	20
Z	CONTINUÉ	R	21
•	F(1SW,1)=-A(2).	R	22
	FIISH,2)=-(Z2*A(2)+PR)	K	23
	F(ISW,3)=-Z2*A(3)	R	24
	F(1SW,4)=-{Z2+(A(4)+PR)}	R	25
	G(ISW.1)=-A(3)	R	26
	G(15W,2)=F(15W,3)	R	27
	G(15W,3)=-(23*A(3)+PR)	R	28
	G[[SN,4]=-(Z3*(A(4)+PR))	R	29
	RETURN	R	30
	END	R	31-
	SURROUTINE FIASCO	S	1
		S	2
-	CDMMON /EROS/ W(21,60,4),P(21,60)	Š	3
_			- 4
	COMMON /NERD/ MF,NF,NY,MUFF,LIMIT,NASTY	2	
	COMMON /SPOR/ S(60),SO(60),SOP(60),SI(60),SIP(60),AREA(60)	S	5
	COMMON"/\$EXX/ NASTIE, IDIOT	- \$	6
	DIMENSION X(21)	5	7
c		S	8
-	DATA DNE/1.D/	Š	9
		3	7
	DATA DISCIENCE	-	14
-	IF (NASTIE-LE-O) RETURN	5	10 11

		2 12
C		13
		14
		15
		ió
•		17
Ċ		
L		18
		19
Ċ		20
		5 21
	TN=x(K)	5 22
	RWR=SORTF(W(K,J,2)++2+W(K,J,3)++2)	5 23
~	CN=SURTF(ONE/(TN++2+ONE))	24
		25
		26
		5 27
2 C		5 28
<u> </u>		5 29
3	CONTINUE	
C		31
	RETURN	32
_C		\$ 33
	END	34-
		i
Č	SUBROUTINE PIRST TP7	2
•	CONNON 140151 AVIOL 31 BV131 31	
		4
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY	<u> </u>
· c	5. 15 A STATES	7 6
_	P=PP	7_
	IF (P) 1,2,4	7 8
ı	RETURN	9
-1	CALL BOMBER (*-FIRST+.98)	10
3	CALL BOMBER ("-FIRST",97)	T 11
3 4		12 -
č	= 0 =	13
6		14
č		15
-5	*: -: *******************************	
2		16
		[17
		7 18
		T 19
6	CALL HUNTZ (K.JX.X.SLOPE)	7 20
<u>C</u>		7 21
	BLIVET=XHASS(JX)	7 22
		7 23
-c		24 -
U		7 25
-		
C		7 26
<u></u>		T 27 _
		7 28
		T 29
	XLOW=PTHROT	T 30
		T 31
<u> </u>		32
-		T 33

_	X=(XLOW+XHIG)*0.5	~	34
С	x-(x50#+x114)+08>	Ť	35
	00 8 K=1,MF	T	36
	PIDDLE=X+AX(K+LUSH)	T	37
dest	SLOPE=BX(K, LUSH)	T	38
8	CALL HUNTZ (K.JX.PIDDLE,SLOPE)	T	39
Č		T	40
	SEX=XMASS(JX)	T	41
	ERROR=SEX-BLIVET	Ţ	42
		Ţ	43
Ċ	•	Ţ	44
9	XHIG=X	Ţ.	45
10	CO TO 11	Ť	47
10	CONTINUE	Ť	48
	CHATTAGE	Ť	49
Ç	TEST FOR MASS	Ť	50
•	RELERR=ERROR/BLIVET	Ť	51
	WRITE (6.14) JX.SEX.ERROR.RELERR	Ť	52
<u>c</u>		T	53
	RETURN	T.	54
<u>c</u>		T	55
	ENTRY DOWN (PP)	T	56
_	P=PP	_T	57
	IF (P) 1,2,12	T	- 5B
12	JX=NF	. <u>T</u> .	59
_	ĠÒ TÒ 5	Ţ	60
C		. [61
	CONMIT ALONG THE MARKET FOR A DISTRICT STATES HAD IN A DISTRICT OF THE PARTY OF THE	Ţ	62
13	FORMAT (/20x, 7H MASS =,E15.6,2x,15HAT STATION NO.=,13 /) FORMAT (/20x,15H AT X-STATION =,13,2x, 6H MASS=,E15.6//20x, ABSO	÷	63
17	1LUTE ERROR=', E15.6,3x,17H RELATIVE ERROR =,2PF8.4,2H %/1	Ť	65
	END ENDA-14612904284110 KECKATIVE ERROR -42PF04412H 471	i	66-
	SUBROUTINE FONKY (FUZZ,RHO,PSTAT,VEL,EASY,TEMP)	ů	1
Ċ	INPUT COMPUTED	ŭ	· 2
č	1	ŭ	3
Č	COMPUTE PROPERTIES AS A FUNCTION OF:	Ū	4
Č	F = STREAMLINE VALUE	u	5
. C	RHO = STATIC DENSITY	U	6
<u>C</u>		U	7
	COMMON /STAG/.A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21),	U	8
	1PZ(21),TZ(21),HZ(21)	U	9
_	COMMON /THERMO/ CPX(3),CVX(3),RAG	U	10
<u>c</u>		U	11
1	TONY INVE	Ų	12
	ONE=1.0	U	13
c	ZERO=0.D	U	14
<u>c</u>	F=FUZZ	- U	16
	Darho	U	17
·	N=0110	u	18
•	IF (F.EQ.ZERO) GO TO 3	Ü	19
	T'16 (F.EG.DNE) GO TO 5	ŭ	20
	IF (F*(ONE-F).LE.ZERO) CALL BOMBER ("FONKY",1)	ŭ	21
C	The second second second and second as second are	Ŭ	22
-	X=F+20.0	ŭ	23

	NEMKA=X	Ü	54
	DIGIT=NEHKY	<u>u</u> .	25
_	F2=X-OIGIT	U.	26
	F1=0NE-F2		27
	J=NEWKY+1	U	
	K=J+1	U	29
C		U	30
	PO=F1+PZ(J)+F2+PZ(K)	U	31
	TO=F1+TZ(J)+F2+TZ(K)	บ	32
C	•	Ü	33
	00 2 L=1.3	Ū	34
	CPX(L)=F1+CP(L,J)+F2+CP(L,K)	U	35
	CVX(L)=F1*CV(L,J)+F2*CV(L,K)	Ū	36
2	CONTINUE	ŭ	37
c	- CONT 170C	ŭ	38
·	BAC-5140CAF4 1345240CAF443	ŭ	
	RAG=F1*RGAS(J)+F2*RGAS(K) GO TO 7		39
_	60 10 7	U	40
<u>c</u>		<u> </u>	41
3	CONTINUE	U	42
	PO=PZ(1)	U	43
	TO=TZ(1)	- υ	44
	00 4 L=1.3	U_	45
-	CPX(L)=CP(L,1)	υ-	46
	CVX{L ⁰ =CV{L,1}	U	47
4	CONTINUE	U	48
C	•	U	49
	RAG*RGAS(1)	ŭ	50
	GD TO 7	ŭ	51
C		— ŭ	52
š .	CONTINUE	ŭ	53
-	P0=P2(21)	- 5	59
		-	
	TO=TZ(21)	U	- 55
	00 6 L=1.3	U	56
	CPX(L)=CP(L.21)	U.	57
	CVX(L)=CV(L,21)	U	58
6	CONTINUE	U	59
	RAG=RGAS(21)	U	60
	GO TO 7	U	61
C		··- u	62
7	CONTINUE	Ü	63
C		Ū	64
	CALL CIPORT (PD.TO.D.F.PRES.TRANK.VELOC,E)	Ŭ	65
<u> </u>		- ŏ	66
-	PSTAT=PRES	ű.	67
	TEMPETRANK		68
	EASY=E	Ü	69
	VÉL=VELOC	"	70
_	AET-AEFOR	_	
<u>C</u>		Ų	71
_	RETURN	U	72
<u>C</u>		U	73
	END	U	74
	SUBROUTINE FREAK (PRES, RHO, UU, VV, HY, NX, PO, TO, DEG, T, XM, VEL, GAM)	V	1
C	INPUT COMPUTED		2
č	-	V	3
	COMMON /COLINT/ L.LL	V	- 4

	COMMON /STUPID/ FZ(21,60)	V	
	COMMON /THERMO/ CPX(3),CVX(3),RAG	. <u>Y</u>	
	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21)	- V	
		٧	
		٧	1
<u> </u>	77.000	. V	1
	ZERO=0.0	٧	
		٧	1
	P=PRES	V	- 1
	R=RHD	٧	1
	U=UU	٧	:
	V=VV	٧	1
	M=MY	٧	_
	N=NX	٧	1
-		٧	- 2
	FUZZ=FZ(M.N)	v	- 2
	Q=V**2+U**2	v	7
		v	- 2
	COMPUTE STREAMLINE PARAMETERS	Ť	-
•	DO 1 K=2.MF	v	- 2
	J=K	v	- 2
	J=K F2=FU2Z~F2(K-1,1)	v	:
	F1=F2(K-1)-FUZZ	ŭ	:
		v	:
	IF (F1*F2.GE.ZERO) GO TO 2' CONTINUE	- <u>v</u> -	-
	CONTINUE	V	•
		V	
,	FAIL TO FIND STREAMLINE	•	3
	CALL BOMBER ('FREAK'.1)	_ V	3
	•	- v	3
	CONTINUE	<u>v</u>	_3
	SUM=F1+F2	V	
	F1=F1/SUM	٧	:
	F2=F2/SUH	٧	:
	RAG=F1*RGAS(J-1)+F2*RGAS(J)	٧	3
,		٧	4
	DO 3 K=1,3	V	4
	CPX(K)=F1*CP(K,J-1)+F2*CP(K,J)	V	-
	CVX(K)=F1*CV(K,J-1)+F2*CV(K,J)	٧	4
,	CONTINUE	٧	4
		V	4
	TEMP=P/(R*RAG)	٧	4
	TZ=TSTAG(CPX.TEMP.O)	٧	4
	PZ=PSTAG(CPX.TEMP.YZ.P.RAG)	-v-	_
		v	4
	TANG=V/U	v	9
	RAD=ATANF(TANG)	v	
	DEGREE=RAD+57,29578	·	
	SEX=CSUBP(TEMP)	v	
	HEX=CSUBV(TEMP)	Ť	-
		V	3
	GAMMA=SEX/HEX		_
	SONIC=SORTF (GAMMA#RAG+TEMP)	V	:
	VELOC=SQRTF(Q)	٧	- 5
	XMACH=VELOC/SONIC	٧	
<u>:</u>		٧	- 5

DEG-DEGREE		10=12	·	62
THEMP Y MAXHACH V 6			ŭ	
XM=XMACH				
VEL-VELOC GAM-GAMMA C RETURN V SUBROUTINE GRONK TFUZZ, PP, RHO, VEL, EASY) C COMPUTE GAS PROPERTIES AS A FUNCTION OF: W C C C TOMPUTE GAS PROPERTIES AS A FUNCTION OF: W C C TIPUT C FUZZ = STREAMLINE INDEX W C C PUZZ = STREAMLINE INDEX W C PP = STATIC PRESSURE W C C RHO = STATIC DENSITY W C C RHO = STATIC DENSITY W C C COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21),W 11 PZ(21),TZ(21) C COMMON /THERMO/ CPX(3),CVX(3),RAG W C C C C C C C C C C C C C C C C C C			•	
GAM=GAMMA C RETURN V 6 RETURN V 7 END SUBROUTINE GRONK (FU22, PP, RHOL, VEL, EASY) C COMPUTE GAS PROPERTIES AS A FUNCTION OF: F = STREAMLINE VALUE AND PP = STATIC PRESSURE N C INPUT C FU22 = STREAMLINE INDEX C RHO = STATIC PRESSIRE N C CALCULATED C COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), W 11 IPZ(21),TZ(21) C COMMON /THERMO/ CPX(3),CVX(3),RAG C C F=FU22 P=PP C C ONE=[_0 C C ONE=[_0 C C TF (F.EO.DNE) GO TO 2 IF (F.EO.DNE) GO TO 2 IF (F.EO.DNE) GO TO 4 IF (F			-	
C			•	
RETURN		Gan-Ganna		
END SUBROUTINE GRONK (FUZZ, PP, RHQ, VEL, EASY) C COMPUTE GAS PROPERTIES AS A FUNCTION OF: C FUZZ = STREAMLINE VALUE AND PP = STATIC PRESSURE C INPUT C FUZZ = STREAMLINE INDEX C PP = STATIC PRESSURE C CALCULATED C RHO = STATIC DENSITY C VEL = VELOCITY M 1 1PZ(21),TZ(21) C COMMON / THERMO/ CPX(3),CV(3,21),MTM(21),GAMZ(21),RGAS(21), M 1 1PZ(21),TZ(22) C COMMON / THERMO/ CPX(3),CVX(3),RAG C C M 1 F=FUZZ F=FUZZ P=PP C ONE=1.0 ZERO=0.0 C IF (F=CO.ONE) GO TO 2 IF (F=CO.ONE) GO TO 3 NEMXY=X DIGIT=NEMXY N 3 NEMXY=X DIGIT=NEMXY N 3 TO=F1=TZ(J)+FZ=PZ(K) N 3 CC C C DO 1 L=1.3 C CVX(L)=F1=CPY(L,J)+FZ=CPY(L,K) C C C CVX(L)=F1=CPY(L,J)+FZ=CPY(L,K) C C C C C C C C C C C C C C C C C C C	L	DETION	-	
END SUBROUTINE GRONK (FUZZ, PP, RHO, VEL, EASY) C C COMPUTE GAS PROPERTIES AS A FUNCTION OF: N C F = STREAMLINE VALUE AND PP = STATIC PRESSURE N C INPUT C FUZZ = STREAMLINE INDEX C CPP = STATIC PRESSURE N C CALCULATED N C RHO = STATIC DENSITY N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), CV(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), MTM(21), GAMZ(21), RGAS(21), N IPZ(21), TTAGA A(0,21), CP(3,21), TTAGA A(0,21), TTAG	-2	RETORA		
C COMPUTE GAS PROPERTIES AS A FUNCTION OFF C COMPUTE GAS PROPERTIES AS A FUNCTION OFF C FUZZ = STREAMLINE VALUE AND PP = STATIC PRESSURE C INPUT C FUZZ = STREAMLINE INDEX C PP = STATIC PRESSURE C CALCULATED C RHO = STATIC DENSITY C VEL = VELOCITY C COMMON / STAG/ A(0.21).CP(3.21).CV(3.21).MTM(21).GAMZ(21).RGAS(21). M 11 1PZ(21).TZ(21) C COMMON / THERMO/ CPX(3).CVX(3).RAG C L COMMON / THERMO/ CPX(3).CVX(3).RAG C M 11 C C C M 12 F=FUZZ P=PP C C M 2 C C M 2 IF (F.EO.JDE) GO TO 2 IF (F.EO.JDE) GO TO 2 IF (F.EO.JDE) GO TO 4 IF (F.EO.JDE) GO TO 5 IF (F.EO.JDE) GO TO 4 IF (F.EO.JDE) GO TO 5 IF (F.EO.JDE) GO TO 6 IF (F.EO.JDE) GO TO 7 IF (F.EO.JDE) GO TO 8 IF (F.EO.JDE) GO TO 9 IF	L	FND '		
C COMPUTE GAS PROPERTIES AS A FUNCTION OF: C F = STREAMLINE VALUE AND PP = STATIC PRESSURE N C INPUT C FUZZ = STREAMLINE INDEX C PP = STATIC PRESSIRE C CALCULATED C RNO = STATIC DENSITY N 11 C VEL = VELOCITY N 12 C COMMON /STAG/ A(8.21),CP(3.21),CV(3.21),MTM(21),GAMZ(21),RGAS(21), N 11 PZ(21),TZ(21) C COMMON /THERMO/ CPX(3),CVX(3),RAG N 11 C			-	71-
C C COMPUTE GAS PROPERTIES AS A FUNCTION OF 1 C F = STREAMLINE VALUE AND PP = STATIC PRESSURE C INPUT C FUZZ = STREAMLINE INDEX C PP = STATIC PRESSIRE C CALCULATED C RHO = STATIC DENSITY W 1 10 C RHO = STATIC DENSITY W 1 10 C COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),MTM(21),GAMZ(21),RGAS(21), W 1 1 1PZ(21),TZ(21) C COMMON /THERMO/ 'CPX(3),CVX(3),RAG W 1 10 C C W 1 10 C W 1	_	SUBROUTINE GRUNK (FUZZ)PPORMUNYELOERSYT		1
C F = STREAMLINE VALUE AND PP = STATIC PRESSURE C INPUT C FUZZ = STREAMLINE INDEX C PP = STATIC PRESSIRE W C C CALCULATED C RHO = STATIC DENSITY W 11 C VEL = VELOCITY W 11 C COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),MTM(21),GAMZ(21),RGAS(21), W 11 LPZ(21),TZ(21) C COMMON /THERMO/ CPX(3),CVX(3),RAG W 1 C C W 1 C W 1 C C W 1	-	ADUBLIEF PLP BEAREN VIPE AF A PURE VIOLENCE		2
C	Č			
C	<u></u>	" - 2 INFAMÉTUE ANTOE WAD NA = 21411C AME220ME		4
C FUZZ = STREAMLINE INDEX C PP = STATIC PRESSURE C CALCULATED W 10 C RNO = STATIC DENSITY W 11 C CUMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21),W 11 C CUMMON /THERMO/ CPX(3),CVX(3),RAG W 11 C CUMMON /THERMO/ CPX(3),CVX(3),RAG W 11 C C F=FUZZ W 12 C C W 12 C C W 12 C C W 14 F (F=FUZZ) W 12 C C W 15 F = FUZZ W 12 C C W 16 F (F,EO,DE) GO TO 2 F (F,EO,DE) GO TO 2 F (F,EO,DE) GO TO 4 F (F,EO,DE) GO TO 5 N 22 C X=F*20.0 NEW(Y=X DIGIT=NEWKY W 33 NEWKY=X DIGIT=NEWKY W 33 FZ=X-DIGIT F (F,EO,DE) GO TO 4 F (F,EO,DE) GO TO 5 N 22 C X=F*20.0 N 34 NEWKY=X N 35 NEWKY=X N 36 NEWKY=X N 37 DPG=F1=FZ(J)+F2*PZ(K) N 36 C NEWKY=X N 37 TO=F1=TZ(J)+F2*PZ(K) N 37 TO=F1=TZ(J)+F2*PZ(K) N 36 C NEWKY=T N 37 TO=F1=TZ(J)+F2*PZ(K) N 37 TO=F1=TZ(J)+F2*PZ(K) N 36 C NEWKY=T N 37 TO=F1=TZ(J)+F2*PZ(K) N 37 TO=F1=TZ(J)+F2*PZ(K) N 37 TO=F1=TZ(J)+F2*PZ(K) N 37 TO=F1=TZ(J)+F2*PZ(K) N 44 COX(L)=F1*CCY(L,J)+F2*PZ(L,K) N 44 COX(L)=F1*CCY(L,J)+F2*PZ(L,K) N 44 COX(L)=F1*PCCY(L,J)+F2*PZ(L,K) N 44	۲	******		5
C PP = STATIC PRESSIRE C CALCULATED C RHO = STATIC DENSITY W 11 C VEL = VELOCITY C COMMON / STAG/ A(8,21), CP(3,21), WTM(21), GAM2(21), RGAS(21), W 11 PZ(21), TZ(21) C COMMON / THERMO/ 'CPX(3), CVX(3), RAG W 11 C	ᇫ			6.
C CALCULATED C RID = STATIC DENSITY C VEL = VELOCITY W 11 C COMMON /STAG/ A(8.21),CP(3.21),CV(3.21),WTM(21),GAM2(21),RGAS(21), W 11 PZ(21),TZ(21) C COMMON /THERMO/ 'CPX(3),CVX(3),RAG W 11 C W 11 C W 11 C W 11 C W 12 C W 12 C W 12 C W 12 C W 14 C W 15 C W 17 C W 17 C W 17 C W 18 C W 19 C W	Č			7
C RHO = STATIC DENSITY C VEL = VELOCITY C VEL = VELOCITY C VEL = VELOCITY C COMMON /STAG/ A(8.21).CP(3.21).CV(3.21).WTM(21).GAMZ(21).RGAS(21), W 11 PZ(21).TZ(21) C COMMON /THERMO/ 'CPX(3).CVX(3).RAG C W 1' C				<u> </u>
C VEL = VELOCITY C COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), W 11				9
COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAM2(21),RGAS(21), W 11 PZ(21),TZ(21) COMMON /THERMO/ CPX(3),CVX(3),RAG	<u> </u>			10
COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),MTM(21),GAMZ(21),RGAS(21), W 12 COMMON /THERMO/ 'CPX(3),CVX(3),RAG	C	VEL = VELOCITY .	••	11
PZ(21),TZ(21)	<u> </u>		W	12
C COMMON / THERMO / CPX (3) , CVX (3) , RAG				13
COMMON / THERMO/ 'CPX(3) * CVX(3) * RAG C C C C F=FU22 P=PP C C C C C C C C C C C C C C C C C		1PZ(21),TZ(21)		14
C	C		W	15
C		COMMON /THERMO/ 'CPX(3),CVX(3),RAG	W	16
C F=FUZZ M 10 F=FUZZ M 20 P=PP M 20 C ONE=1.0 M 20 ZERO=0.0 M 20 C IF (F.EQ.ZERO) GO TO 2 M 20 IF (F.EQ.ZERO) GO TO 2 M 20 IF (F.EQ.DNE) GO TO 4 IF (F*(ONE-F).LE.ZERO) CALL BOMBER (*GRONK*.1) M 20 C X=F*20.0 M 30 NEMKY=X M 30 NEMKY=X M 30 DIGIT=NEMKY M 30 F2=X-DIGIT M 30 CPX(L)=F1*F2*FZ(K) M 30 CPX(L)=F1*CP(L,J)*F2*CP(L,K) M 30 CPX(L)=F1*CP(L,J)*F2*CP(L,K) M 40 CVX(L)=F1*CP(L,J)*F2*CV(L,K) M 40 CONTINUE M 40 CONTINUE	·c		W	17
F=FU22 P=PP C ONE=1.0 ZERD=0.0 IF (F.EQ.ZERD) GO TO 2 IF (F.EQ.DNE) GO TO 4 IF (F*(ONE-F).LE.ZERD) CALL BOMBER (*GRONK*.1) C X=F*20.0 NEHKY=X DIGIT=NEMKY F1=ONE-F2 J=NEMKY+1 K=J+1 PD=F1*PZ(J)*F2*PZ(K) TO=F1*TZ(J)*F2*PZ(K) C OO 1 L=1.3 CPX(L)=F1*CP(L,J)*F2*CP(L,K) CVX(L)=F1*CP(L,J)*F2*CV(L,K) CONTINUE W 20 # 20 # 20 # 20 # 30 # 4			W	10
F=FU2Z P=PP C C C C C C C C C TF (F.EQ.ZERD) GO TO 2 TF (F.EQ.DNE) GO TO 2 TF (F.EQ.DNE) GO TO 4 TF (F.EQ.DNE) GO TO 2 TF (F.EQ.DNE	·č. —			19
P=PP C ONE=1.0 ZERO=0.0 W 22 ZERO=0.0 W 22 IF (F.EO.ZERO) GO TO 2 IF (F.EO.DNE) GO TO 3 IF (F.EO.DNE) GO TO 4 IF (F*(ONE-F*).LE.ZERO) CALL BOMBER (*GRONK*.1) W 22 C X=F*20.0 NEWKY=X D1G1T=NEWKY W 33 P2=X-D1G1T F1=ONE-F2 J=NEMKY+1 K=J+1 PO=F1*PZ(J)*F2*PZ(K) T0=F1*PZ(J)*F2*PZ(K) W 33 C C O0 1 L=1.3 CPX(L)*=F1*CP(L,J)*F2*CP(L,K) CVX(L)*=F1*CPY(L,J)*F2*CPY(L,K) W 44 CONTINUE	•	F=F1177	ŭ	20
C ONE=1.0 M 2:				21
ONE=1.0	C			22
ZERO=0.0 C IF (F.EO.ZERO) GO TO 2 IF (F.EO.DNE) GO TO 4 IF (F.EO.DNE) GO TO 2 IF (F.EO.DNE) GO TO 3 IF (F.EO.DNE) GO TO 2 IF (F.EO.DNE) GO TO 3 IF (F.EO.DNE) GO TO 3 IF (F.EO.DNE) GO TO 4 IF (F.EO.DNE) GO TO 3 IF (F.EO		ONE=1.0		23
C				24
IF (F.EQ.ZERD) GO TO 2	·-		••	25
IF (F.EQ.DNE) GO YO 4	•	'IE IE EO ZERDA GO TO 2		
IF (F*(ONE-F).LE.ZERO) CALL BOMBER (*GRONK*,1)				27
C				
X=F*20.0 W 36 NEWKY=X W 33 D1G1T=NEWKY W 33 F2=X-D1G1T W 33 F1=0NE-F2 W 36 J=NEWKY+1 W 35 K=J+1 W 35 P0=F1*PZ(J)+F2*PZ(K) W 35 T0=F1*TZ(J)+F2*TZ(K) W 35 C W 36 CPX(L)=F1*CP(L,J)+F2*CP(L,K) W 46 CVX(L)=F1*CP(L,J)+F2*CP(L,K) W 46 CVX(L)=F1*CP(L,J)+F2*CP(L,K) W 46 CONTINUE W 46	_	IF IF TONE-PARCESZENDA CALC BONDER 3 GROWN 11		
NEWKY=X	L	V-E-20 0		
DIGIT=NEWKY				
F2=X-DIGIT F1=ONE-F2 J=NEMKY+1 K=J+1 P0=F1*PZ(J)+F2*PZ(K) T0=F1*TZ(J)+F2*TZ(K) C OO 1 L=1.3 CPX(L)=F1*CP(L.J)+F2*CP(L.K) CVX(L)=F1*CY(L.J)+F2*CV(L.K) 1 CONTINUE W 33 W 44 W 44 W 44 W 45 W 45 W 46				
F1=ONE-F2				32
J=NEWKY+1 K=J+1 P(J=F1*PZ(J)*F2*PZ(K) T(J=F1*TZ(J)*F2*TZ(K) C D(J) L=1,3 CPX(L)=F1*CP(L,J)*F2*CP(L,K) CVX(L)=F1*CP(L,J)*F2*CP(L,K) 1 CONTINUE W 33 W 44			-	33
K=J+1 PQ=F1*PZ(J)*F2*PZ(K) TQ=F1*TZ(J)*F2*TZ(K) M 3 C DO 1 L=1,3 CPX(L)=F1*CP(L,J)*F2*CP(L,K) CVX(L)=F1*CY(L,J)*F2*CV(L,K) 1 CONTINUE W 44			W	34
PG=F1=PZ(J)+F2=PZ(K) TG=F1=TZ(J)+F2=TZ(K) C DO 1 L=1.3 CPX(L)=F1+CP(L,J)+F2=CP(L,K) CVX(L)=F1+CP(L,J)+F2=CV(L,K) 1 CONTINUE W 4			W	35
TO=F1*TZ(J)+F2*TZ(K) C DO 1 L=1.3 GPX(L)=F1*CP(L,J)+F2*CP(L,K) CVX(L)=F1*CY(L,J)+F2*CV(L,K) 1 CONTINUE M 4			W	36
C			W	37
C		TO=F1+T2(J)+F2+T2(K)	W	38
CPX(L)=F1*CP(L,J)+F2*CP(L,K) W 4 CVX(L)=F1*CV(L,J)+F2*CV(L,K) W 4 1 CONTINUE W 4	C	,	W	39
CPX(L)=F1*CP(L,J)+F2*CP(L,K) W 4 CVX(L)=F1*CY(L,J)+F2*CV(L,K) W 4 1 CONTINUE W 4		00 1 L=1.3	W	40
CVX(L)=F1*CV(L+J)+F2*CV(L+K) W 4:	·	GPX(I,)=F1*GP(1,)+F2*GP(1,.K)		41
1 CONTINUE W 4		CVX(1) 1 = F1 + CV(1 = .1) + F2 + CV(1 = K)		42
	1	CONTINUE	•••	43
ペート・アルリーフ に アイドル・ファイル スター・スター・スター・スター・スター・スター・スター・スター・スター・スター・	•		W	44
				45
	•			46

	PO=PZ(1)	W	41
	T0=T2(1)	_ W	48
		W	49
	CPX(L)=CP(L,1)	W	_50
	CVX(L)=CV(L,1)	W	51
3	CONTINUE	W	52
	RAG=RGAS(1)	W	53
	GO TO 6		54
4	CONTINCE	W	55
	PO=PZ(21)	_ ₩	>6
	10-121217	W	57
	00 5 L=1.3	W	58
	CPX(L)=CP(L,21)		59
	CVX(L)=CV(L,21)	W	60
5	CONTINUE	W	61
	RAG=RGAS (21)		62
	GO TO 6	W	63
5	**	W	64
6	CONTINUE	W	65
_	CALL TROPIC (PD.TO.P.F.OEN.VELOC.E)	Ä	66
C	RHO=DEN .	W	67
	VEL=VELOC	W	69
	EASY=E	W.	70
	RETURN	- W-	71
С	RETURN	W	72
<u> </u>	END	- ü	73-
	CHARTION MANUA IN DANAA TO CACRE	X	1
-c	FUNCTION HANKY (A.PANKY.TO.SAGR)	î	. 2
•	D(MENSION A(1)	â	3
C	Direction star	-	- 4
•	AZ=A(1)	Ŷ	5
	A1=A(2)	- ;;	- 6
	A2=A(3)	x	7
C		x	8
•	X=DANK Y	x	9
	X=PANKY TZ=TO RGAS=SAGR	 ÿ-	10
	RGAS=SAGR	x	ii
-c			12
Č		X	13
	POWER=RGAS/AZ	- · X	14
	FUDGE=X**PDWER	X	15
	FUDGE=X**POWER RARF=A1/AZ	X	16
	TRAF=A2*0.5/A2	X	17
J		x	18
Č	LET FIRST GUESS FOR T = TZ	X	19
	7=72	- X	20
	DO 1 K=1,5	X	21
	112=1/12	X	22
	EPAR=(TZ-T)+(BARF+(TZ+T)+TRAF)	X	23
	XLAX=EXP(EPAR)	X	24
	TRAT=XLAX*FUNGE	X	25
. C.—-	COMPARE "TRAT" WITH "TYZ" " " " " " " " " " " " " " " " " " "	X	26
-	TCOMP=TRAT+TZ	X	27
	ERROR=TCOMP=T	- x	29
	T=TCOMP	X	29

r	CONTINUE HANKY=T	X	30 31
<u>c</u>		· 🛣	- 32
L .	DETURM	×	
	RETURN		33
	END	X	34-
	SURROUTINE HORNY	- Y	
C C		A	5
Ç	ANNULAR NOZZLE	. Y	3
C	COMPUTE THE STREAM FRACTION BASED ON 1-D GEOMETRY.	Y	•
<u>c</u>		Y	5
	COMMON INERDI MININT MUFFISTUPIDIF (21.60)/SUPER/R(21.60)	Y	6
	COMMON /SPOR/ S(60),SO(60).SOP(60).SI(60),SIP(60),AREA(60)	Y	7
C		Α.	8
	CALL DREZ (F,1260)	Y	9
c		Y	10
	CALL HEAD6	Y	11
	DO 2 J=1.N	Y	12
	F(M, J)=1.0	Ÿ	13
	ROGER=1.0/AREA(J)	Y	14
	DO 1 K=2, MUFF	Ÿ	15
ī	F(K,J)=(R(K,J)+R(1,J))+(R(K,J)-R(1,J))+ROGER	·Ý	16
•		Ÿ	17
2	WR(TE (6,3) J.(F(K,J).K=1,M)	÷	18
2		٧,	
	RETURN	<u> </u>	19
<u>c</u>		¥	20
<u>c</u>		Y	21
3	FORMAT (10X, 15, 2X, 11F10.4/17X, 10F10.4/)	Y	22
	END .	Y	23
	FUNCTION HOTS (CP.TSTAT.TZERO)	2	1
C		Z	2
C	COMPUTE THE ENTHALPY DIFFERENCES	7.	1
С	H(TZERO) - H(TSTAT) = HOTS	Z	4
C	WHERE CP = CP(1) + CP(2)+T + CP(3)+T++2	2	. 5
C		2	6
	DIMENSION CP(1)	—· <u>z</u>	·,
С		Ž	8
	A=CP(1)	Ž	9
	B=CP(2) +0.5	ž	10
	C=CP(3)*0.3333333	···· ž	- ii
С	0-07(37)(05333333	ž	12
-	Y=TSTAT	ź	13
	X=TZERO	. 2	14
	H=(X-Y)+(A+B+(X+Y)+C+(X++2+X+Y+Y++2))	- 2	15
·	HOTS=H	_ Z	16
C		Z	17
	RETURN	Z	18
C		Z	19
	END	Z	20
	SUBROUTINE HUNT	AA	1
	COMMON /SPOR/ S(60).SO(60).SOP(60).SI[60].SIP(60).AREA(60)	44	2
	COMMON /NERD/ MF.NF.NT	- 44	3
	DO 1 K=1,NF	AA	4
	S(K)=SO(K)-SI(K)	AA	5
	AREA(K)=S(K)*(SO(K)+SI(K))	3.4	Ŀ
	LITTLE=!	AA	7
	SMALL=AREA(1)	AA	8

	DO 2 K=2,NF	AA	9
	IF (SMALL.LE.AREA(K)) GO TO 2	AA	_ 10
	SMALL=AREA(K)	AA	11
	LITTLE=K	AA	12
5	CONTINUE	AA	13
	AGGNY=SORTF(SMALL)	AA	14
	CALL HEADS	AA	15
	WRITE (6,4) LITTLE, SMALL, AGONY	AA	16
	WRITE (6,5)	AA	17
	DO 3 K=1,NF	AA	18
	AGONY=AREA(K)/SHALL	AA	19
	SNAFU=SQRTF (AGDNY-)	AA	20
	WRITE (6.6) K.AREA(K).AGONY.SNAFU	AA	21
3	CONTINUE	AA	22
	NT=LITTLE	AA	23
	RETURN	AA	24
:		AA	25
	•	AA	26
	FORMAY 1/20x . MIN X-STA = 14, 3X, MIN AREA = F9.4, 3X, EFFECTIVE	AA	27
•	1RADIUS ='.F10.4 /)	44	28
	FORMAT (/33X, AREA . 12X, A/A++ . 11x, R/R+1 /)	AA	29
	FORMAT (20X+15-3F15-4)	AA	30
<u> </u>	END .	AA	. 31
	SUBROUTINE HUNTZ (NY.NX.PRES.SLOPE)	AB	· i
-	SUBMIDITINE HUNTE 141 INAPPRESTATED	AB	
	GIVEN THE INDICIES (NY.NX) COMPUTE THE "H" AND "P" ARRAY VALUES.		3
	NY = ORDINATE INDEX	AB	4
	NX = ABSCISSA INDEX	AB	5
•	500000 15000 C 1120 CO (C) 0100 CO	AB	
	COMMON /EROS/ W(21,60,4),P(21,60)	AB	- 7
	COMMON THERDY ME, NE, NY, MUFF, LIMIT	AB	H
	COMMON /STUPIO/ F(21,60)	48	9
	COMMON /SUPER/ R(21,60)	AB	10
	COMMON /SPOR/ \$160),\$0160),\$09(60),\$1(60),\$19(60),AREA(60)	AB	11
	COMMON /NUPER/ HA(21)+HB(21)	AR	12
_		AB	13
		AB	14
:		AB	15
	J=N4	AB	16
	K=NX	48	17
	PP=PRES	AR	18
	FUZZ=F(J,K)	AB	19
_		AB	20
	COSIN=SQRTF(1,0/(1.0+SL0PE++2))	AB	21
_		AB	22
		AB	23
	CALL GRONK (FUZZ,PP,RHO, VEL, EASY)	AB	24
:		AR	25
	WI=RHD+R(J.K)	AB	25
	WV=W1*VEL	AB	27
	W2=WV*COSIN	AB	28
	W3=W2+SLOPE	AB	29
	W4=EASY+R(J-K)	AB	30
:	NATIONAL INTEGRAL	AB	31
	₩(J.K.1)=WI	AB	32
	W(JaK-2)=W2	AB	33
	# 1 U # N # E 7 T M E	M D	

MIJ,K,3)=M3	34 35 36 37 38 39 40 1 2 3 4 5 6 7 8 9
P(J,K)=PP	36 37 38 39 40 1 2 3 4 5
C RETURN AB C	37 38 39 40 1 2 3 4 5 6 7 8
RETURN	38 39 40 1 2 3 4 5 6 7 8
END	39 40 1 2 3 4 5 6 7 8
END FUNCTION HZERO (ETA) C C C COMPUTE STAGNATION ENTHALPY FOR STREAMLINE VALUE ETA AC C C COMMON /STAG/ A(8.21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC 1PZ(21),TZ(21),HZ(21) AC C C C C C C C C C C C C C C C C C C	40 1 2 3 4 5 6 7 8 9
FUNCTION HZERO (ETA) C COMPUTE STAGNATION ENTHALPY FOR STREAMLINE VALUE ETA C COMMON /STAG/ A(8.21),CP(13,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC IPZ(21),TZ(21),HZ(21) C ONE=1.0 ZERO=0.0 HZERO=0.0 HZERO=HZ(21) AC IF (X.CT.CONE) RETURN IF (X.CT.CONE) RETURN AC IF (X.CT.CONE) CALL BOMBER ("HZERO",1) AC R=N R=X-R FZ=R AC F1=ONE=F2 HOHO)=HZ(N+1)*F1+HZ(N+2)*F2 HZERO=HOHO) C RETURN C COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTY COMMON /TYME/ T,FLIT COMMON /TYME/ T,FLIT COMMON /TYME/ T,FLIT COMMON /TYME/ T,FLIT COMMON /FUBBAR/ F1,F2,F3,F4,F5 AD T=0.0 FLITEL ZERO=0.0 AD T=0.0 FLITEL ZERO=0.0	1 2 3 4 5 6 7 8 9
COMPUTE STAGNATION ENTHALPY FOR STREAMLINE VALUE ETA AC COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC IPZ(21),YZ(21),HZ(21) AC ONE=1.0 CERC=0.0 AC HZERD=0.0 AC HZERD=HZ(21) AC IF (x.EC.ONE) RETURN AC IF (x.GT.ONE) CALL BOMBER ('HZERO',1) AC IF (x.GT.ONE) CALL BOMBER ('HZERO',2) AC R=N R=N R=N R=N AC F1=DNE-F2 HOHD=HZ(N+1)*F1+HZ(N+2)*F2 HZERD=HOHD AC SUBROUTINE INITAL COMMON /COUNT/ L.LL COMMON /TYME/ T,FLIT COMMON /TYME/ T,FLIT COMMON /TYME/ T,FLIT COMMON /TYME/ T1,FZ,F3,F4,F5 AD L=0 L=0 T=0.0 FLIT=L ZERO=0.0 AD	2 3 4 5 6 7 8 9
COMPUTE STAGNATION ENTHALPY FOR STREAMLINE VALUE ETA AC COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC IPZ(21),YZ(21),HZ(21) AC ONE=1.0 AC ONE=1.0 AC M2ERD=0.0 M2ERD=HZ(21) AC X=ETA AC IF (X.EO.ONE) RETURN AC IF (X.G.ONE) CALL BOMBER ('MZERO',1) AC N=X R=N R=N R=X-R F2=R H2ERD=H0HD AC RETURN AC RETURN AC RETURN AC COMMON /CDUNT/ L,LL COMMON /CDUNT/ L,LL COMMON /FUBAR/ F1,FZ,F3,F4,F5 AD L=0 L=0 L=0 T=0,0 FL1T=L ZERD=0.0 AD AD AD AD AD AD AD AD AD A	3 4 5 6 7 8 9
COMMON /STAG/ A(8.21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC TP2(21),YZ(2)),HZ(21)	3 4 5 6 7 8 9
COMMON /STAG/ A(8.21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC IPZ(21),TZ(21),HZ(21)	4 5 6 7 8 9
COMMON /STAG/ A(8.21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), AC P2[21),TZ(21),HZ(21)	5 6 7 8 9
TPZ[21],TZ(21),HZ[21]	6 7 8 9
AC	7 8 9
ONE=1.0	9
ZERO=0.0	9
M2ERD=HZ(21)	•
X=ETA	10
	11
IF (X.LT.ZERD) CALL BOMBER ('HZERD',1) AC IF (X.GT.ONE) CALL BOMBER ('HZERD',2) AC X=X*20.0 AC AC AC AC AC AC AC A	12
IF (X.GT.ONE) CALL BOMBER ('HZERO', 2)	13
X = X + 20.0	14
N=X	15
R=N R=x-R F2=R AC F1=DNE-F2 HNHD=H2(N+1)*F1+H2(N+2)*F2 AC HZERO=HOHD AC RETURN AC END SUBROUTINE INITAL AD COMMON /COUNT/ L.LL COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTY COMMON /TYME/ T,FLIT COMMON /FUBAR/ F1,F2,F3,F4,F5 AD L=0 L=0 AD ZERO=0.0 AD ZERO=0.0	
R=X-R F2=R AC F1=DNE-F2 HDHD=H2(N+1)*F1+H2(N+2)*F2 AC HZERO=HOHD AC RETURN AC END SUBROUTINE INITAL AD COMMON /COUNT/ L.LL COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTY AD COMMON /FUBAR/ F1,F2,F3,F4,F5 AD L=0 L=0 T=0.0 FL)T=L ZERO=0.0 AC	16
# # # # # # # # # # # # # # # # # # #	17
# # 1 = ONE - F 2	18
HOHO=H2(N+1)*F1+H2(N+2)*F2 HZERO=HOHO AC RETURN AC END SUBROUTINE INITAL AD COMMON /COUNT/ L.LL COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTY COMMON /TYME/ T,FLIT COMMON /FUBAR/ F1,F2,F3,F4,F5 AD L=0 L=0 AD T=0.0 FLIT=L ZERO=0.0	19
HZERD=HOHD AC AC AC AC AC AC AC A	20
HZERO=HOHO	21
RETURN AC RETURN AC END AC SUBROUTINE INITAL AD COMMON /COUNT/ L.LL AD COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTY AD COMMON /TYME/ T,FLIT AD COMMON /FUBAR/ F1,F2,F3,F4,F5 AD L=0 AD L=0 AD T=0.0 AD T=0.0 AD ZERO=0.0 AD	22
RETURN AC END SUBROUTINE INITAL AD COMMON /COUNT/ L.LL AD COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY AD COMMON /TYME/ T.FLIT AD COMMON /FUBAR/ F1.F2.F3.F4.F5 AD L=0 AD L=0 AD T=0.0 FLIT=L AD ZERO=0.0	23
END AC SUBROUTINE INITAL AD COMMON /COUNT/ L.LL AD COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTY AD COMMON /TYME/ T,FLIT AD COMMON /FUBAR/ F1,F2,F3,F4,F5 AD L=0 AD L=0 AD T=0.0 AD T=0.0 AD ZERO=0.0 AD	74
END SUBROUTINE INITAL COMMON /COUNT/ L.LL COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY COMMON /TYME/ T.FLIT COMMON /FUBAR/ F1.F2.F3.F4.F5 L=0 L=0 AD T=0.0 FLIT=L ZERO=0.0 AD AD ZERO=0.0	25
SUBROUTINE INITAL AD AD COMMON /COUNT/ L.LL AD COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY AD COMMON /TYME/ T.FLIT AD COMMON /FUBAR/ F1.F2.F3.F4.F5 AD L=0 AD L=0 AD L=0 AD L=0 AD T=0.0 AD T=0.0 AD T=0.0 AD AD ZERO=0.0 AD AD AD AD AD AD AD A	26
COMMON /COUNT/ L.LL . AD COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY . AD COMMON /TYME/ T.FLIT . AD COMMON /FUBAR/ F1.F2.F3.F4.F5 . AD L=0 . AD L=0 . AD T=0.0 . AD FLIT=L . AD ZERO=0.0 . AD	
COMMON / COUNT / L.LL	1
COMMON /NERD/ MF,NF,NT,MUFF,LIMIT,NASTV COMMUN /TYME/ T,FLIT COMMON /FUBAR/ F1,F2,F3,F4,F5 AD L=0 L=0 AD T=0.0 FLIT=L ZERO=0.0 AD	2
COMMON / TYME/ T, FLIT COMMON / FUBAR/ F1, F2, F3, F4, F5 L=0 L=0 AD L=0 AD T=0,0 FLIT=L AD ZERO=0.0 AD	3
COMMON /FUBAR/ F1,F2,F3,F4,F5 L=0 L=0 AD T=0.0 FL)T=L AD ZERO=0.0 AD	4
L=0 AD LL=0 AD T=0.0 AD FLIT=L AD ZERO=0.0 AD	5
L=0 AD LL=0 AD T=0.0 AD FL)T=L AD ZERO=0.0 AD	6
L=0 AD LL=0 AD T=0.0 AD FL)T=L AD ZERO=0.0 AD	7
LL=0 AD T=0.0 AD FLIT=L AD ZERO=0.0 AD	8
T=0.0 AD FLIT=L AD ZERO=0.0 AD	9
FL)T=L AD ZERO=0.0	10
ZERO=0.0 AD	11
96AN (6.71 KI.K7.K3.K4.K6	12
	13
WRITE (6,3) KI,K2,K3,K4,K5	14
F1=K1 AD	-
F2=K2 AD	15
F3=K3 AD	15
F4=K4	16
F5=K5 AD	16
	16 17
AD	16 17 18
SUM=F1+F2+F3+F4+F5 AD	16 17 18 19
IF (SUM_EG.ZERO) CALL BOMBER ('FRITO'.1) AD AD	16 17 18

_	WRITE (6,4) F1,F2,F3,F4,F5,SUN	AD	24
<u>c</u>	F1=F1/SUM	AD-	_25
	F1=F1/SUM F2=F2/SUM	AD AD	26 27
	F3=F3/SUM	AD.	28
	F4-F4/SUM	AĐ	29
	F5=F5/SUM	AD	30
c	, , , , , , , , , , , , , , , , , , , ,	AD.	31
. <u>~</u>	WRITE (6.4) F1.F2.F3.F4.F5	AD	32
<u>c</u>		AD	33
	CALL NAVSEA	AD	34
	CALL STAGG .	AD	35
	CALL STATIC	ΔD	36
	CALL HDRNY	AD	37
	CALL BEDLAM	AD	38
	CALL CHECK	AD	39
	DO L K=2,LIMIT	AD.	40
1	CALL PHINOI (K)	AD	41
	CALL TRICKY	AD	
	CALL OUTPUT	_ AD	. 43
Ċ		AD	44
	RETURN	40	45
C		AD	46
<u>c</u>	20000	AD	47
2	FORMAT (1615)	AD.	48
3	FORMAT (/20X, INTERPOLATION FACTORS //20X, 515)	AD	
•	FORMAT (/20X,1P6G15.6) END	AD	50 51
	FUNCTION LIBARY (SDRFT)	AE	1
	SDRFT=0.0	AE	2
	LIBARY=O	ĀĒ	- 5
•	RETURN	ĀĒ	4
<u> </u>	ACTOMY	AE	5
•	ENTRY COSRF(X)	AE	6
-	COSRF=COS(X)	AE	7
	RETURN	4E	8
<u> </u>	4	AE	9
_	ENTRY SINRF(X)	4E	10
	SINRF=SIN(X)	AE	~ I1
	RETURN	AE	12
-c		AE	13
	ENTRY COSF(X)	AE	14
	COSF=COS(X)	AE	15
	RETURN	٩E	16
c		AE	17
	ENTRY SINF(X)	AE	18
	SINF=SINIX)	AE	19
	RETURN	AE	50
C	PUTRU TANGANA	AE	51
	ENTRY TANF(X)	AE	22
	TANF=TAN(X)	AE	23
	RETURN	AE	24
<u> </u>	ENTRY CORTE/YA	AE	25
	ENTRY SORTF(X) SORTF=0.0	AE.	26
	IF (X.LE.D.OD+O) RETURN	AE AE	28
	II INGLEGUOVUTUI NEIUNN	ac	20

	SORTF=SORT(X) RETURN	AE AE	29 30
	NE LONG	ÃÈ-	31
C	ENTRY ATABELY.		_
	ENTRY ATANE (X)	_ AE	32
	ATANFATAN(X)	_	
	RETURN	AE.	34
C		AE	35
	ENTRY DUMDUM(X,Y)	AE	34
	DUMDUH=Y	AE	37
	IF (X.LT.Y) DUMDUM=X	ΔE	38
	RETURN	AE	39
C		AE	40
<u>~</u>	ENTRY TANDE(X)	AE	41
		_	
	WDRGH=X/57.29578	. AE	42
	TANDF=TAN(WDRGH) ·	AE	43
	RETURN	AE	44
	ENO	AE	45-
	SUBROUTINE LINEAR (TARGET, X, NASTY, F1, F2, J1, J2, NOCON)	AF	1
C		AF	2
Č	TARGET = INPUT VALUE	AF	3
Č	X · = MONOTONIC ARRAY	- AF	4
Č	NASTY = NO. OF "X'S"	AF	5
Č	FI & F2 = THE LINEAR INTERPOLATION FACTOR AND.	AF	6
-			
<u>c</u>	ST G SZ - INC " INDICES SUCH INATA	AF	7
C	TARGET = F1+X(J1) + F2+X(J2)	AF	8
C	NOCON = NO SOLUTION CODE	AF	9
2		AF	10
	DIMENSION X(1)	AF	11
C		AF	12
-	ZERO=0.0	AF	13
	NX=NASTY	AF	14
	NOCON#1	ĀF	15
	IF (NX.LT.2) RETURN	AF	16
	NÜCQN=5	AF .	17
	IF (NX.GT.21) RETURN	AF	18
C	•	AF	19
	NOCON=3	AF	20
	Gl=TARGET-X(l)	AF	21
	G2=X(NX)-TARGET	AF	22
	SUM=G2*G1	ĀF	23
	IF (SUM-LT-ZERO) RETURN	ĀF	24
		7.75	
	00 1 K=2+NX	AF	25
	J=K	AF	26
	G2=TARGET-X(K-1)	AF	27
	G1=x(K)-TARGET	AF	28
	IF ({G1+G2).GE.ZERO) GO TO 2	AF	29
1	CONTINUE	AF	30
•	NDC DN=4	AF	31
	RETURN	AF	32
C	DE LODA	AF	
_	This on Ta		33
2	NOCON=5	AF	34
	SUM=G1+G2	AF	35
	IF (SUN.EO.ZERO) RETURN	AF	36
	NOCON=0	AF	37
	AOCHA-O	A.	
	F1=G1/SUM	AF	3.8

	AF	40
	AF	4
RETURN	AF	4
END	AF	4
SURROUTINE MAINP	AG	
	AG	- 1
COMMON /DELTAS/ DX, DY.DY, DY2, DY2, DY4	ΔĞ	
COMMON /COUNT/ L.LL	AG	4
COMMON /MERD/ MF.NF.NT	AG	
COMMON /TYME/ T.FLIT	AG	
	- AG	
READ (5.4) NDSEG.NDIT.K.KREEP	AG	9
IF (K.LE.O) CALL INITAL	AG	
IF (K.GT.D) CALL RESTOR	46	10
	AG	i
IF (K.LT.0) GO TO 3	_	-
IF (KREEP.NE.O) CALL MEYER	AG	1
	ΔG	1
CALL HEADS	AG	_14
	AG	1
K=NOSEG#ND1T ·	AG	1
WRITE (6.5) NOSEG.NOIT.K	AG	1
IF (K.LE.O) CALL BOMBER [MAINPROG +K)	AG	٦,
	AG.	1
CALL SAVEHP	AG	2
	AG	2
CALL PLOTP	AG	2
CALL JINX	AG	2
	AG	2
On 2 K=1,NOSEG	- AG	2
NO 1 J=1.NOIT	AG	2
TETHOT	AG	-7
L=L+1	AG	2
FLITTEL	- AG	2
CALL RESET	AG	3
	AG	3
- CALL TOUCH	AG	_
CALL CYCLE	40	3
CALL CYCLE CALL RESET		
CALL CYCLE CALL RESET CALL BNDRY	AG	_
CALL CYCLE CALL RESET CALL BNDRY CALL DOODLE	AG	3
CALL CYCLE CALL RESET CALL BNDRY CALL DODDLE CALL RESET	AG AG	3
CALL CYCLE CAUL RESET CALL BNDRY CAUL DODDLE CALL RESET CALL FIASCO	AG AG	3
CALL CYCLE CALL RESET CALL RNDRY CALL DUODLE CALL FIASCO CALL STREAM	AG AG AG AG	3 3 3
CALL CYCLE CALL RESET CALL BNDRY CALL DODDLE CALL FIASCO CALL FIASCO CALL STREAM CALL RESET	AG AG AG AG	3 3 3
CALL CYCLE CALL RESET CALL RNDRY CALL DUODLE CALL FIASCO CALL STREAM	AG AG AG AG	3 3 3
CALL CYCLE CALL RESET CALL RIDRY CALL DUODLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL TRICKY	AG AG AG AG	3 3 3 3
CALL CYCLE CALL RESET CALL BNDRY CALL DODDLE CALL FIASCO CALL FIASCO CALL STREAM CALL RESET	AG AG AG AG	3:3:3:4:
CALL CYCLE CALL RESET CALL RESET CALL DUDDLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT	AG AG AG AG AG AG	3 3 3 3 4 4
CALL CYCLE CALL RESET CALL RESET CALL DUDDLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL RESET CALL RESET	AG AG AG AG AG AG	3 3 3 3 4 4 4 4
CALL CYCLE CALL RESET CALL RESET CALL DOODLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX	AG AG AG AG AG AG AG	3 3 3 3 3 4 4 4 4
CALL CYCLE CALL RESET CALL RESET CALL DUDDLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT	AG AG AG AG AG AG AG AG	3 3 3 3 4 4 4 4 4
CALL CYCLE CAU RESET CALL RESET CALL DUDDUE CALL DUDDUE CALL FIASCO CALL STREAM CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX CALL STORE	AG AG AG AG AG AG AG AG	3 3 3 3 3 4 4 4 4 4 4 4
CALL CYCLE CALL RESET CALL RESET CALL DOODLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX	AG AG AG AG AG AG AG AG AG	333333444444444444444444444444444444444
CALL CYCLE CAU RESET CALL RESET CALL DUDDUE CALL DUDDUE CALL FIASCO CALL STREAM CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX CALL STORE	AG AG AG AG AG AG AG AG AG AG	333333444444444444444444444444444444444
CALL CYCLE CAU RESET CALL RESET CALL DUDDUE CALL DUDDUE CALL FIASCO CALL STREAM CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX CALL STORE	AG AG AG AG AG AG AG AG AG AG	3 3 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
CALL CYCLE CALL RESET CALL RESET CALL DUDDLE CALL RESET CALL FIASCO CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX CALL STORE RETURN	AG AG AG AG AG AG AG AG AG AG AG AG	34 31 31 31 41 4 4 4 4 4 4 4 4 4 4 4 4 4
CALL CYCLE CAU RESET CALL RESET CALL DUDDUE CALL DUDDUE CALL FIASCO CALL STREAM CALL STREAM CALL RESET CALL TRICKY CALL OUTPUT CALL JINX CALL STORE	AG AG AG AG AG AG AG AG AG AG AG AG AG	333333333333333333333333333333333333333

	ENO SUBROUTINE MAXIE (X.NDEX)	AG AH	53- 1
<u> </u>	FINO THE INDEX OF THE LARGEST VALUE OF ARRAY "X".	AH	ž
·	OTHENSION X(1)	AH	3
	N=NDEX	AH	4
	J=1 ·	AH	5
	IF (N.LE.1) RETURN	AH	6
	BIG=X(1)	AH	7
	00 1 K=2,N	AH	B
	_ IF (BIG.GT.X(K)) GO TO 1	ΔH	g.
		Ali	1å "
	BIG=X(K)	ÄH	iĭ
1	CONTINUE	AH	12
•	NOEX=1	AH	13
	RETURN	AH	14
С	NE LUNA	AH	15
-č		AH	
·	ENTRY MINITERY NICES		16
	ENTRY MINNIE(X,NDEX)	AH	17
L	FIND THE INDEX OF THE SMALLEST VALUE OF ARRAY "X".	HA	18
		AH	19
	N=NDEX	AH	20
	IF (N.LE.1) RETURN	AH	21
	SMALL=X(1)	AH	22
	DD 2 K=2.N	AH	23
	IF (SMALL.LT.X(N)) GO TO 2	AH	24
	J=K	AH	25
	SMALL=X(N)	AH	26
.2	CONT INUE	AH	27
	NDEX=J	AH	28
C		AH	29
	RETURN	AH	30
	END	AH	31-
	SLIBROUTINE MEYER	AI	- i
С	THIS SUBROUTINE RESERVED FOR COMPUTING A FREE PRESSURE BOUNDARY.	AI	ż
	RETURN	ΑÏ	3 ~
	END	AI	4-
	SUBROUTINE MONO (X1NX)	- ÂĴ	1
	DIMENSION X(1)	AJ	ž
· · ·	N=MX		
	N=NX ,	AJ	3
	00 4 M-0 N-m-111 T T T-1-m	AJ	4
	DO 1 K=2+N	LA	5
. 1	X(K)=DUMDUM(X(K-1)+X(K)) .	AJ	6
	RETURN	AJ	7
	_ END	LA	8-
	SUBROUTINE NAVSEA	AK	1
_C		AK	2 _
	COMMON /FRAN/ AD160),A1(60),BD(60),B1(60)	AK	3
	COMMON /DELTAS/ DX.DY.DY.DY2.0T2.0T4	AK	4
	COPMON /DUPER/ HA(21), HB(21)	AK	5
	COMMON /EROS/ D(60,4),MAT(20),KODE(4),SDYDX(60)	AK	6
	COMMON /FLEX/ NFLX	AK	7
	COMMON /NDEX/ INDEX(9)	AK	8
	www.niwit gitmant gitMunt ff		
	COMMON ANERDA ME NE NE NE NIEE I INTELLE	AK	
	COMMON /VERD/ MF,NF,NT,MUFF,LIMIT,NEWKY	AK	9
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NEWKY COMMON /SPOR/ \$(60).SO(60).SOP(60).\$I(60).\$IP(60).AREA(60) COMMON /SUPER/ R(21.60)	AK AK	10

_	DATA ZERO/O.O/,ONE/1.O/,ZUBER/57.Z9578/	AK AK	1
	CALL OREX (\$,360)	AK	-1
			_
	CALL DREZ (D,264)	AK.	_!
	READ (5,18) MF,NF	AK	_1
	READ (5,20) DX,DT	AK	_1
	WRITE (6,19) MF,NF	AK	i
		AK	2
	LIMIT=NF-1	AK	2
	MUFF=MF-1	AK .	_
	NEWKY=MIJFF-1	AK	2
	DY=MUFF	AK	2
	DY=ONE/DY	AK	-2
	DY2=DY+0.5	AK	2
_	DT2=DT+0.5	AK	. 5
	DT4=DT2*0.5	AK	2
	WRITE (6,12) DT.DX.DY	AK	2
	READ (5.23) ((D(K.J).J=1.4).K=1.NF)	AK	3
	CALL EQUATE (SO.0.240)	AK	-3
		AK	3
	ENTRY HOAX	AK	3
	HOTTE 14 101	AK	3
	WRITE (6.13)	AK	3
		AK	3
	WRITE (6,14) (K,SO(K),SOP(K),SI(K),SIP(K),K,K=1,NF)	AK	-3
	DU37-MC-3	AK	3
	BUZZ=MF-1	_	_
	FUZZ=ONE/BUZZ	AK	3
	DD 2 K=1,MF	AK	. 4
	F1=MF-K	AK	4
	HA(K)=F1/BUZZ	AK	4
	F2=K-1	AK	4
	HB(K)=F2/BUZZ	AK	4
	DO 1 J=1.NF	AK	4
	R(K,J)=(F1+SI(J)+F2+SD(J))+FUZZ -	AK	4
	CONTINUE	AK	4
		AK	4
	CALL HEAD6	AK	4
	WRITE (6.15)	AK	5
	DO 3 J=1.NF	ΔK	5
	WRITE (6,21) J. (R(K,J),K=1,MF)	AK	5
		AK	Ś
	CALL HUNT	AK	5
		AK	-5
	READ (5,18) NASTIE, IDIOT	AK	5
	··· IDIOT=MINO(IDIOT=NT)	AK	5
			_
	IF (NASTIE-LT-0) NASTIE=NT	AK	5
	WRITE (6,16) NT, NASTIE, IDIOT	AK	5
	CALL HEAD6	AK	6
		AK	- 6
	WRITE (6,10)	AK	6
	WRITE (6,17)	AK	6
	K=1	AK	6
		AK	6
	D1K=0.0	AK	6
_	DEGIK=0.0	AK	-6
	DEGOK=0.0 .	AK	6

	X=ZERO	AK	69
	WRITE 16,22) K.X.AREAIK),SIK),SOIK),DOK,SOPIKI,DEGOK,SIIKI,DIK,SIP	AK	70
	1(K) DEGIK	AK	71
С		AK	72
	EPAR=0.5/DX FPARDY=EPAR=DY	AK	73
	EPARDY=EPAR*DY	AK	74
	DO 4 K=2,LIMIT	AK	75
	SDYDX(K)=S(K)*EPARDY	AK	76
	DIK=(SI(K+1)-SI(K-1))+EPAR	AK	77
	DOK=(SO(K+1)-SO(K-1))*EPAR	AK	78
	DEGIK=ZUBER*ATANF(SIP(K))	AK	79
	DEGOK=ZUBER*ATANE(SOP(K))	AK	80
	X=(K-1)+0X	AK	81
	WRITE (6,22) K.X.AREA(K).S(K).SO(K).DOK.SOP(KI.DEGOK.SI(KI.DIK.SIP	AK	82
	1(K) -DEGIK	AK	83
4	CONTINUE	AK	84
	K=NF	AK	85
	X={K-1}+DX	AK	86
	DΠK=0.0	AK	87
	DIK=0.0	AK	88
	DEGIK=0.0	AK	89
	DEGOK=0.0	AK	90
	WRITE (6,22) K,X,AREA(K),SIK),SO(K),DOK,SOP(K),DEGOK,SI(K),DIK,SIP		91
	I(K).DEGIK	AK	92
-	11K/J//EGIR	AK	93
•	DO 5 K=2.NT	AK	94
			95
	NFL X=K-1	AK	
	IF (SDP(K)-SDP(K-1)) 5,5,6	AK.	96
5	CONTINUE	AK	97
<u>6</u>	WRITE (6-11) NFLX	AK	98
C -		AK	99
	CALL NAVSTO	AF	100
Č		AK	101
	INDEX(1)=1	AK	102
	INDEX(2)=4	AK	103
	INDEX(3)=NT-5	AK	104
	INDEX(4)=NT-3		105
	INDEX(5)=NT-1		106
	INDEX(6)=NT		107
	INDEX(7)=NT+1		108
	INDEX(8)=NT+3		
			109
	INDEX (9)=NT+5	_	110
	COMPUTE ANGLES	AK	111
	COMPUTE ANGLES.		112
	NO 1 Walfield.		113
	BD(K)=ATANF(SOP(K))		114
	BI(K)=ATANF(SIP(K))	AK	115
7	CONTINUE	AK	116
<u></u>		AK	117
	DO 8 K=2,LIMIT	AK	118
	AO(K)=SDYDX(K)+180(K+1)-80(K-1))		119
	AI(K)=-SDYDX(K)+(BI(K+1)-BI(K-1))		120
8	CONTINUE		
9			121
	DO 9 K=2,LIMIT		122
	BO(K)=SDYDX(K)+SINRF(BO(K)+BO(K))		123
	8I(K)=-SDYDX(K)+SINRF(BI(K)+BI(K))	AK	124

9	CONTINUE		125
<u>c</u>			156
_	RETURN		127
Ç -			128
			129
10	FORMAT 1/20X, MOZZLE GEDHETRY ' /)		130 -
11	FORMAT (/20x, INFLECTION POINT NO. = 1,13)		131
15	FORMAT (/20x, DT = , 3PFID.4. (MILLISECONDS) ,5x, DX = , OPF9.5.3x.	AK	132
	1'DY =',F9.5)		133
13	FORMAT (/36x,'SD',13x,'SOP',13x,'S[',13x,'S[P'/)		134
14	FORMAT (5(20x, 15, 2x, 4F15.6, 5x, 15/))		135
15	FORMAT (/20X, ""R" ARRAY"/)		136
16	FORMAT (/20x, THROAT INDEX(NT) = 1,13,4x, LAST FLOW SHOOTH = 1,13,		
	14x. LAST PRESSURE SMOOTH STATION =*,13)		138
17	FORMAT" (26x, 'X', 8X, 'AREA', 7x, 'S', 8X, 'SO', 6x, 'DSO/DX', 5x, 3HSO', 6x,	AK	139
	16HSD'(D),7x.'S1',5x,'DSI/Dx',4x,3HSI',6x,6HSI'(D) /)	AK	140
18	FORMAT (1615)	AK	141
19	FORMAT (/20x. 'NO. POINTS ON VERTICAL LINE(MF)=".13.5x, 'NO. OF WAL	AK	142
	1L POINTS(NF) =*, [3/)		143
20	FORMAT (2812.0)	AK	144
Żĺ	FORMAT (10x, 15,2x, 12F9,4/17x, 12F9,4)	AK	145
22	FORMAT (5(10x, 15, 5x, 11F10, 4/))	AK	146
23	FORMAT (4G15.0)		147
	END		148-
	SUBROUTINE NAVSTO	AL	
C	·	AL	2
-	COMMON THERD! ME NE	AL	3.
	COMMON /DELTAS/ DK,DY.DT	AL	4
	COMMON /NAVIER/ DTOX, DTDX2, DTDX4, DTDX8, DTDY, DTDY2, DTDY4, OTOY8	AL	5-
•	COMMON /STOKES/ A(60).B(60).H(60)	AL	6
	COMMON /SPOR/ \$160),50160),509160),\$[160],\$[160],\$[160],AREA(60)	ĀL	Ť
C		AL	8
	ONE=[.0	ÄL	· - ğ-
C	JAC-110	AL	10
- <u>-</u> -	DTDX=DT/DX	AL	ii -
	DTDX2=DTDX+0.5	AL	12
	DTDX4=DTDX2*0.5	ĀĽ	- 13
	DTOXR=OTDX4+0.5	AL	14
	DTOX=-DT/DY	AL	15
	DTDY2=DTDY+0.5	AL	16
	DTDY4=DTDY2+0.5	AL	17
	DTDY8=0TDY4+0.5	AL	18
_	U1010-0101-0101	AL	19
۲.	DO 1 K=1.NF	AL	20
	A(K)=(SOP(K)+SIP(K))/S(K)	AL	21
	B(K)=SIP(K)/S(K)	AL	22
	H(K)=0NE/S(K)	AL	23
		AL	24
1	CONTINUE		_
C .	DO 2 K-1 190	AU	25
	DO 2 K=1,180	AL	26
2	A(K)=A(K)+DTDYZ	AL	27
Č		AL	28
	RETURN	AL	29
C		AL	30
	END	AL	31-
	SUBROUTINE NORMAL (X, NERD)	AH	1

DIMENSION X(1) N=NERD SUM=0.0 DO 1 K=1.N	MA — Ma Ma Ma	3
SUN=0.0 DD 1 K=1.N	AM	
DO 1 K=1.N		
	A 14	5
	A11	6
1 SUM=SUM+X(K)	MA	7
IF (SUM.LE.O.O) RETURN	AM	. 6
DO 2 K=1.N	AM	9
2 x(K)=x(K)/SUM	MA	10
RETURN	AM	11
END	AM	12-
SUBSOUTINE OREZ (X.NERD)	AN	ī
E	ĀN	- 2
DIMENSION X(1)	AN	3
DIMENSION XII)	AN	4
	AN	5
N=NERD	ĀN	6
E 10 40	AN	7
DO 1 K=1.N		
1 X(K)=-0.0	AN	8
<u> </u>	AN	9
RETURN	AN	10
C END	AN	11
END	AN	12-
SUBROUTINE OUTPUT	- 40	1
C	AO	2
COMMON /COUNT/ L.LL	AO	3
COMMON /NERD/ MF.NF.NT	AD	4
	AO	5
N6=6	ÃO	6
NO-0	ÃO	ž
C No=6	ÃO	- 8
	40	0
T	AO	10
DO 2 K=1+NF	AD	11.
CALL HEADS	AO	12
CALL GROG 1K)	AO	13
	AD	14
DO 1 J=1, MF	40	15
1 CALL PLINE (J.K.N6)	AO	16
C	AO	17
2 CONTINUE .	- AO	18
C se	AO	19
CALL ENIGMA	AÜ	20
C .	AO	21
C WRITE OUT AXIS.	AO	22
CALL HEADS	ÃO	23
WRITE (A.5) L	AO	24
C	40	25
CALL FROG	AO AO	26
<u></u>	40	27
DO 3 K=1.NF	AD	28
3 CALL PLINE (1.K.NB)	40	29
C .	AD	30
C WRITE DUT WALL.	AO	31
C	AO	34
CALL HEADS	AD	33

	WRITE (8,6) L	AO AO	3
	CALL FROG	AU	. 3
	DO 4 K=1.NF	AQ.	3
•	CALL PLINE (MF,K,NB)	AO	3
			3
	RETURN	AO	4
		_ AO	4
		AD	4
	FORMAT (/20X, AXIS ITERATION NO=1, 15 / 1	AO	4
	FORMAT (/20x, WALL ITERATION NO=',15 /)	AD	4
	END ·	AO	4
	SUBROUTINE PARAB(\$X,\$Y,\$)	AP	
	IMPLICIT REAL+8(A-H,O-Z)	AP	
	DIMENSION \$X(1),\$Y(1),\$(1)	AP	
	\$(1) = -0.0	AP	
	s(2) = - 0.0	AP	
	\$(3) = -0.0	AP	
	X1 = SX(1)	AP	_
	X2 = \$X(2)	AP	
	x3 = \$x(3)	· AP	
	F1 = X1 - X2	AP	_ l
	F2 = X2 - X3	AP	1
_	F3 = X3 - X1	AP	1
	D = F1*F2*F3	AP	7
	IF (D .EQ. 0.0D+O) RETURN	AP	1
	D = -1.0/D .	AP	1
	Y1 = 5Y(1)	AP	1
	Y2 = \$Y(2)	AP	1
	$y3 = yy(3) \qquad \cdot .$	AP	1
	VI = VI*F2	AP	Ť
	Y2 = Y2 + F3	AP	Ž
	V3 - V2+C1	AP	· 2
	S(1) = D*(Y1*X2*X3 + Y2*X1*X3 + Y3*X1*X2)	AP	ž
	s(2) = -0*(Y!*(X2+X3) + Y2*(X!+X3) + Y3*(X!+X2!)	AP	- 2
	\$(3) = 0*(Y1+Y2+Y3)	AP	2
	RETURN	AP	- 2
	END	AP	
			2
	SUBROUTINE PCLASS	AO	
	COMMON /SPY/ KCLASS, KGROUP	QA	_
	INTEGER*4 JERK(3.3) /	AO	2
	* 'UNCL', 'ASS1', 'F1ED'	AO	2
	*, 'CONF', IDEN', 'TIAL'	YO	7
	*, 'S', 'ECRE', 'T' /	AQ	2
	DIMENSION M(3)	AO	
	CALL EQUATE (M,JERK(1,KCLASS+1),3)	AO	
_	CALL DATE (KDAY+KYR)	- AO	
	RETURN	AO	
	ENTRY PCL6	AU	_
		AQ	
	WRITE (6.1) M	AQ AQ	
	WRITE (6,1) M WRITE (6,2) KDAY,KYR,KGROUP,M	0A - A0	
-	WRITE (6,1) M WRITE (6,2) KOAY,KYR,KGROUP,M RETURN	0A 0A 0A	1
	WRITE (6,1) M WRITE (6,2) KOAY,KYR,KGROUP,M RETURN ENTRY FCLB	OA	1
	WRITE (6,1) M WRITE (6,2) KOAY,KYR,KGROUP,M RETURN	0A 0A 0A	1 1 1

	ENTRY PCL14	AO	15
	WRITE (14,1) M	AQ	16
	WRITE (14,2) RDAY,KYR,KGROUP,M	AQ"	717
	RETURN	AQ	18
7		AO	19
1	FORMAT ('2',T58,18('4')/T58,'4',T75,'4'/T58,'4 ',3A4,T75,'4'/	AO	20
	1758.***,?75.***/T58,18(***))	AO	21
2	FORMAT ('0'/' DATE=',13,'/',12,T58,18('+')/' GROUP',12,T58,'+', T	AO	22
-	175, 4*'/' ARO INC.", 158, 1* ', 344, 1 4'/' ARNOLD AIR FORCE STATION,	AO	23
	2TENN.*,T58,***,T75,***/T58,18(***) /)	AO	24
	END	AO	25
	SUBROUTINE PHINGU (NXSTA)	AR	1
c	SAUGONING MILLON THYSINA	AR	- 2
	COMMITTE THE ORESPOND CORRESPONDING TO A CINEN MASS ELON		3
č	COMPUTE THE PRESSURE CORRESPONDING TO A GIVEN MASS FLOW	AR .	
c	SUBSONIC REGIME	AR	- 3
<u>c</u>		AR	5
	COMMON /NERD/ MF,NF,NT,MUFF,LIMIT	AR	6
	COMMON /FLIGNR/ WEIGHT.PTHROT.PANIC	AR	_ 7
C		AR	8
	TARGET=WEIGHT	AR	9
	NX=NXSTA	AR	10
	IF ((NX.LE.O).OR.(NX.GT.NF)) CALL BOMBER ("PHINOU", NX)	AR	11
	XLOW=PTHROT	AR	12
	XHIG=PAN)C	AR	13
		AR	14
•	DN 3 KOUNT=1,20	AR	15
	X=(XLON+XHIG)+0.5	AR	16
	CALL SETHP (X+NX)	AR_	17
_		AR	18
1	XH1G=X	AR	19
_	GO TO 3	AR	20
2	XFOH=X	AR	21
3	CONTINUE	AR	22
C		AR	23
	RETURN	AR	24
	ENO	AR	25
	SUBROUTINE PLINE (MY, NX, NUNIT)	AS	ī
	COMMON /COUNT/ L.LL	AS	Ž
		.~•	
	COMMON /FROS/ W/21.40.5)	AC	- 2
	COMMON /EROS/ W(21,60,5) COMMON /SPOR/ S(60) SO(60) SO(60) SI(60) SI(60) AREA(60)	AS	_
	COMMON /SPOR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60)	AS	4
	COMMON /SPOR/ S(60),SO(60),SOP(60),SI(60),SIP(60),AREA(60),	AS AS	5
	COMMON /SPOR/ S(60),SO(60),SOP(60),SI(60),SIP(60),AREA(60), COMMON /STUPIO/ F(21,60) COMMON /SUPER/ R(21,60)	AS AS AS	5
	COMMON /SPQR/ S(60),SO(60),SDP(60),SIP(60),AREA(60), COMMON /STUPIO/ F(21,60) COMMON /SUPER/ R(21,60) H=MY	AS AS AS	4 5 6 7
	COMMON /SPQR/ S(60),SD(60),SDP(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX	AS AS AS AS	5 6 7 8
	COMMON /SPOR/ S(60),SD(60),SDP(60),SIF(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT	AS AS AS AS AS	5 6 7 8 9
	COMMON /SPOR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=HY N=NX NU=NUNIT P=W(M,N,5)	AS AS AS AS AS	5 6 7 8 9
	COMMON /SPOR/ S(60),SD(60),SDP(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) W1=W(M,N,1)	AS AS AS AS AS AS	4 5 6 7 8 9 10
	COMMON /SPQR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) M1=W(M,N,1) W2=W(M,N,2)	AS AS AS AS AS AS	4 5 6 7 8 9 10 11 12
	COMMON /SPOR/ S(60),SD(60),SDP(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) W1=W(M,N,1)	AS AS AS AS AS AS	4 5 6 7 8 9 10
	COMMON /SPQR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) M1=W(M,N,1) W2=W(M,N,2)	AS AS AS AS AS AS	6 7 8 9 10 11 12
	COMMON /SPQR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) W1=W(M,N,1) W2=W(M,N,2) W3=W(M,N,3)	AS AS AS AS AS AS AS	5 6 7 8 9 10 11 12 13
	COMMON /SPQR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) H=MY N=NX NU=NUNIT P=W(M,N,5) W1=W(M,N,1) W2=W(M,N,2) W3=W(M,N,3) W4=W(M,N,4)	AS AS AS AS AS AS AS	5 6 7 8 9 10 11 12 13 14 15
	COMMON /SPQR/ S(60),SD(60),SDP(60),SI(60),SIP(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=HY N=NX NU=NUNIT P=H(M,N,5) W1=H(M,N,1) H2=H(M,N,2) H3=H(M,N,3) H4=H(M,N,4) RHO=HI/R(M,N)	AS AS AS AS AS AS AS AS	5 6 7 8 9 10 11 12 13 14 15 16
	COMMON /SPQR/ S(60),SD(60),SDP(60),SIF(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) W1=W(M,N,5) W2=W(M,N,2) W3=W(M,N,2) W3=W(M,N,4) RHO=WI/R(M,N,4) U=W2/H1 V=W3/WI	AS AS AS AS AS AS AS AS AS	5 6 7 8 9 10 11 12 13 14 15 16
	COMMON /SPQR/ S(60),SD(60),SDP(60),SIF(60),AREA(60) COMMON /STUPID/ F(21,60) COMMON /SUPER/ R(21,60) M=MY N=NX NU=NUNIT P=W(M,N,5) W1=W(M,N,1) W2=W(M,N,2) W3=W(M,N,3) W4=W(M,N,3) W4=W(M,N,4) RHO=WI/R(M,N,4) U=W2/H1	AS AS AS AS AS AS AS AS	3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18

WRITE (6,2) M.FUZZ.WI.WZ.W3.W4.P.T.XM.GAM.RHO.U.V.DEGRE.PZERO.	TZER AS	2
RETURN	AS	- z
L CONTINUE	AS	2
		_
IF (NU.NE.8) CALL BOMBER ('PLINE',1)	AS	2
WRITE (8.2) N.FUZZ.WI.WZ.W3.W4.P.T.XM.GAM.RHO.U.V.DEGRE.PZERO.		2
10.VEL	AS	2
RETURN	AS	2
	AS	2
ENTRY GROG(NASTY)	AS	3
N=NASTY .	AS	3
	_	_
WRITE (6,3) L,N,SI(N),SO(N),LL	AS	3
WRITE (6,4)	AS	3
RETURN	AS	3
ENTRY FROG	AS	3
78122 1977.	AS	3
WRITE (8,4) RETURN	AS	3
esees and executed executed executed must be look of companying the lateral and	45	3
FORMAT (3X,15,2X,2PF12.2,3X,1P7G15.5/10X,1P8G15.5/)	AS	3
FORMAT (/20x, ITERATION NO.= 1, 14, 3x, 1x-STATION NO.= 1, 13, 3x, 1	Y-INN AS	4
1ER =*.F9.4.3X,*Y-OUTER =*.F9.4.5X,*OUTPUT NO. =*.15 /)	AS	4
FORMAT (11X, 'STREAMLINE % '.8X, 'WL', 14X, 'W2', 12X, 'W3', 14X, 'W		4
1x, P-STAT , 10x, TEMP(R) , 7x, MACH NO / /15x, CP/CV , 9x, DENSIT		4
2x, U', 13x, 'V', 10x, 'FLOW ANG(D)', 7x, 'P-STAG', 10x, 'T-STAG', 7x, '		4
3174. \)	AS	4
END	AS	4
SUBROUTINE PLOTP	AT	
	ĀT	
OUTPUT PLOT PRESSURE DATA DN UNIT 10.	ĀŤ	•
	AT	
COMMON /APE/ LURID(27)	AT	
COMMON /COUNT/ L.LL	AT	
COMMON /DELTAS/ DX"	AT	
COMMON /EROS/ W(21,60,4).P(21,60)	AT	
COMMON /NERDY HY.NX	ĀŤ	
COMMON /SPOR/ \$(60),\$0(60),\$0P(60),\$1(60),\$1P(60),AREA(60)	AT	1
COMMON /SUPER/ R(21,60)	, AT	\neg
	· AT	- 1
DOITE 2101 CHOID	AT	- 1
WRITE (10) R,SO,SI,DX,MY,NX	ĀŤ	1
RETURN	· · · AT	1
		_
0+4-000cc00000cc00000	AT	1
ENTRY JINX	AT	1
	AT	1
WRITE (10) L.P	AT	1
RETURN	AT	2
	ĀŤ	2
	AT	2
END		
ENO SUBROUTINE PHIN (PH)	AU	
END SUBROUTINE PHIN (PM)	AU	
END SURROUTINE PHIN (PM)	AU	
END SUBROUTINE PHIN (PM) **PZ" "ARRAY" SEARCH FOR "MINIMUN" VALUE" = PM	AU AU	
END SUBROUTINE PHIN (PM) "PZ" "ARRAY" SEARCH FOR "MINIMUN VALUE" PM	UA	
END SURROUTINE PHIN (PM) "PZ" "ARRAY" SEARCH FOR "MINIMUN" VALUE = PM COMMON /NERDY MF NF NT	UA	-
END SURROUTINE PMIN (PM) "PZ" "ARRAY" SEARCH FOR "MINIMUN" VALUE" = PM COMMON /NERD/ MF.NF.NT COMMON /STAG/ A(8.21).CP(3.21).CV(3.21).WTM(21).GAM2(21).RGAS	AU AU AU AU (21)+ AU	-
END SURROUTINE PHIN (PM) "PZ" "ARRAY" SEARCH FOR "MINIMUN" VALUE = PM COMMON /NERD/ MF.NF.NT	UA	-

L		ΔU	9
	X=PZ(1)	_AU	.10
	DO 1 K=2,MF	AU	11
	IF (X.GT.PZ(K)) X=PZ(K)	AU	12
1	CONTINUE	AU	13
C		AU	14
	PM=X	AU	15
C		ΑU	16
	RETURN	AU	17
C		AU	is
<u></u>	END	AU	19-
			_
	FUNCTION PRAT (XMACH, GAMMA)	AV	1_
C	P/PT = F(MACH NO.)	AV	2
	X=GAMMA/(1.Q-GAMMA)	AV	3
	PRAT=(1.0+0.5+(GAMNA-1.0)+XMACH++21++X	AV	4
	RETURN	AV	5
	END	AV	6-
	FUNCTION PSTAG (CP.TSTAT.TZERO.PSTAT.SAGR)	AW	1
	DIMENSION CP(3) .	AW	2
C	Difficultion CV (3)	AW	3
	Tensent in the second of the s		-
	CPZ=CP(1)	AW	4
	CPA=CP(2)	AW	5
	CPB=CP(3)	AW	6
:		AW	7
	T=TSTAT	AW	8
	TZ=TZERO	AH	9
_	PEPSTAT	AW	10
	RGAS=SAGR	AW	ii
		AW	12
_	BADE-FDA / F 07	AW	13
	RARF=CPA/CPZ	AW	13
_	TRAF=0.5*CPB/CPZ		-
		AW	15
	TRAI=TZ/T	AW	16
	POWER=CPZ/RGAS	AW	17
	PAR=(TZ-T)+(BARF+(TZ+T)+TRAF)	AW	18
	XLAX=EXP(EPAR)	AW	19
	PRAT=(TRAT=XLAX)**POWER	· A 9	20
	PZERD=PRATOP	AW	21
_	227.0	AW	22
	PSTAG=PZERO	AW	23
C	The second of	AW	24
	RETURN	AW	25
	END	AW	26-
	SUBROUT (NE PUNTZ (NY.NX.PRES)	AX	1
	TCOMMON /EROS/ W(21.60.4).P(21.60)	AX	2
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT	AX	3
	COMMON /STUP(D/ F(21,60)	ĀX	4
			-
	COMMON /SUPER/ R(21,60)	AX	_ 5
	COMMUN /SPOR/ S(60), SD(60), SDP(60), ST(60), STP(60), AREA(60)	AX	6
	COMMON /DUPER/ HA(21)+HB(21)	AX	7
	J=NY .	AX	8
	K=NX	AX	9
	PP=PRES'	AX	10
	FUZZ=F(J,K)	AX	ii
	SLOPE=HA(J) *S[P(K)+HB(J) *SOP(K)	AX	12

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	CALL GRONK (FUZZ, PP, RHD, VEL, EASY)	AX		14
	W1=RHO+R(J,K)	AX.		15
	WY=W1+VEL	AX		16
	W2=WV*COSIN	AX		1.
	W3=W2*SLOPE	AX		1
	W4=EASY*R(J,K)	AX		1
	W(J,K,1)=W1	AX		2
	W(J,K,2)=W2	AX	- :	2
_	W(J,K,3)=W3	AX		:
	W(J,K,4)=114	AX		2
_	P(J,K)=PP	AX		2
	RETURN	AX		ž
	END	AX		2
	7.67	AY		_
_	FUNCTION PYNTS (WONE, WFOUR, WAMA, NERK)	AY		
	COMPUTE STATIC PRESSURE AS A FUNCTION OF (W1+W4+STREAMLINE)			
		AY		
	COMMON /STUPID/ F(21,60)	AY		4
	COMMON /SUPER/ R(21,60)	AY		
		AY		7
	W1=WONE	AY		. 1
	W4=WFDUR	AY		
	M=MA HA	AY		1
	N=NERK	AY		ı
	·	AY		1
_	FUZZ=F(M.W)	AY		Ī
	HO=HZERO(FUZZ)	AY		1
_	P=(HD+W1-W4)/R(M,N)	AY		1
	PVNTS=P	AY		i
-		ÂY		i
	RETURN	AY		i
_	RETURN	ÂY		i
	END			-
		AY		1
	FUNCTION RHOMAX (FUZZ)	ΑZ		
		AZ		
	"RHONAX" COMPUTES THE STAGNATION DENSITY	AZ		
	AS A FUNCTION OF THE STREAMLINE VALUE.	AZ		•
		ΑZ		-
	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTH(21),GAMZ(21),RGAS(21),	AZ		-
_	T1P2(21),T2(21),H2(21),RH02(21)	AZ		
	·	AZ		3
_	ONE=1.0	AZ		•
	ZERO=0.0	AZ		1
		AZ	_	ī
	F=FUZZ	AZ	1	ī
_	IF (F.EO.ONE) GO TO 3	AZ		i
	IF (F.EQ.ZERO) GO TO Z	ΑŽ		ī
_	F (F+(ONE-F).LE.ZERO) CALL BOMBER (**RHOMAX**,1)	AZ		i
	X=F*20.0	AZ		i
_	NEWKY=X	AZ		İ
				-
_	DIGIT=NEWKY	AZ		1
	F2=X-DIGIT	AZ		1
	F1=0NE-F2	ΑZ		2
	J=NEWKY+1	AZ		2
	K=J+1	AZ		2
	RZ=F1*RHOZ(JJ*FZ*RHOZ(K)	AZ		2
	RHOMAX=RZ	AZ		2

С	RETURN .	AZ	2:
2	RZ=RHDZ(1)	-AZ-	-2
L	MENINGER EVEN	AZ	2
c—	GO TO 1	AZ.	2
3	RZ=RHOZ(21)	AZ	3
	GO YO 1	AZ	-3
С	60 10 1	AZ	3
·	PAIR TO THE PAIR T		_
	END	AZ	3
	FUNCTION RIDDLE (NY.NX)	BA	_
Ç	COMPUTE THE DESIGNATION OF FREEDRICK FOR	BA	-
<u>c</u>	COMPUTE THE DENSITY "DIDDLE" FACTOR FOR	BA	
<u> </u>	MASS CONSERVATION	BA	
<u>c</u>		BA	!
	COMMON /STUPID/ F(21,60)	BA	
	COMMON /EROS/ W(21,60,4),P(21,60)	BA	
	CDMMDN /SUPER/ R(21,60)	BA	- 1
	COMMON /THERMO/ CPX(3),CVX(3),RAG	BA	•
C		BA	1
	ONE=1.0	BA	1
	ZERÔ=0.0	BA	1.
	K=NY	BA	1
	J=NX	BA	1
	RIDOLE=ZERO .	BA	1
	FUZZ=F(K,J) ·	BA	1
	RHO=W(K,J,1)/R(K,J)	BA	1
c —	COMPUTE PROPERTIES AS A FUNCTION OF RHO.	BA	1
-	CALL FUNKY (FUZZ, RHO, PSTAT, VEL, EASY, T)	BA	1
c		BA	2
_	VV=VEL**2	BA	2
	IF (VV.En.ZERO) CALL BOMBER (**RIDDLE**,2)	BA	- 2
	GAMMA=CSIBP(T)/CSUBV(T)	BA	2
ć		BA	2
•	BETA=GAMMA*RAG*T/VV	BA	2
	XM=SORTF(ONE/BETA)	BA	2
		_	
	RID=ONE-BETA	BA	2
_	RIDDLE=RID	BA	2
<u>c </u>		BA	2
_	RETURN	BA	3
<u>c</u>	END .	BA	3
	To Thomas and the state of the	BA	3
	SUBROUTINE ROGUE	88	
C		88	
	COMMON /ERDS/ W(21,60,5)	88	
	COMMON /NERD/ MF.NF.NT	BB	
	COMMON /SUPER/ R(21,60)	BB	
c _		BB	
C .	SMOOTHING ROUTINE FOR DENSITY	88	
<u> </u>		86	
C	PRESERVE STATION 1.	BB	
	DO 1 J=1.5	BB	1
ı	CALL EQUATE (W(1,60,J),W(1,1,J),MF)	86	i
ċ		86	i
č	COMPUTE DENSITY AT EACH W(+.+.1)	88	i
<u> </u>	DO 3 K=1,MF	BB	-i
	UU 3 N-19MF	On	1

2	W(K,J,1)=W(K,J,1)/R(K,J)	58	16
3	CONTINUE	88	17
₫-	VOVI 1105	BB .	18
č	••	88	19
ç	SHIFT RHO UP + 2 FOR TEMPORARY STORAGE	88	20
•	DO 4 J=1.NF	BB	21
	K=NF+1-J	BB	22
4	CALL EQUATE (W(1,K+2,1),W(1,K,1),MF)	88	23
c-		BR	24
-	CALL SLICK	BB	25
C		BB	26
Č	RESTORE FIRST STATION	88	27
	00 5 J=1,5	BA	28
5	CALL EQUATE (W(1,1,J),W(1,60,J),MF)	BR	29
	RETURN	88	30 "
	END	BB	31-
	SUBBOUT INF SAM	BC	1
C		RC.	Ž
-	COMMON /EROS/ W(21,60,4),P(21,60)	BC	3
	COMMON /NERD/ MF.NF.NT.MUFF	8C	4
	COMMON /STUP(D/ F(21.60)	BC	- 5
	COMMON /SUPER/ R(21,60)	BC	6
	COMMON /WORK/ X(60)	BC	7
	COMMON /SEXX/ NAST(E.IDIOT	BC	8
-		BC	9
	IF (ID(OT.LE.2) RETURN	80	10
7		BC	11
C	PRESSURE SMOOTHING AT CONSTANT Y.	BC	12
	DO 3 K=2, MUFF	BC	13
С	10.12	BC	14
	PO 1 J=1,10101	BC	15
1	(L,) Y = (L) X	BC	16
C		BC	17
	CALL SMOOTH (X, IDIOT, 4)	BC	18
	HORON=IDIOT-1	BC	19
	DO 2 J=2,MORON	BC	20
	CALL GRONK (F(K,J),X(J),RHU,VEL,EASY)	BC	21
	RWR=SQRTF(W(K,J,2)**2+W(K,J,3)**2)	BC	22
	CSN=w(K,J,2)/RWR	BC	23
	SN=W(K,J,3)/RWR	BC	24
	W(K,J,1)=RHO+R(K,J)	AC	25
	W(K,J,2)=W(K,J,1)*VEL*CSN	BC	26
	W(K+J+3)=W(K+J+1)*VEL*SN	BC	27
	W(K,J,4)=EASY*R(K,J)	BC	28
	T P(K,J)=X(J)	BC	29
2	CONTINUE	BC	30
-c		BC	31
3	CONTINUE	AC	32
t		BC	33
	RETURN	AC	34
	END	BC	35-
	SUBROUTINE SAVEWP	80	1
	DIMENSION A(21,5,2)	BD	2
	COMMON /EROS/ W121.60.5)	BD	3
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY	BD	4
	DO 2 K=1,21	80	5
	 · · · · · · · · · · · · · · · ·		

	00 1 J=1,5	BD	6
	(L.f.) W=(f.L.)A	BD	7
1	A(K,J,2)=W(K,NF,J)	BD	8
2	CONTINUE	BD	9
	RETURN	BD	10
C		BD	11
Ċ		BD	12
	ENTRY RESET	9D	13
	DO 4 K=1.21	BD	14
	00 3 J=1.5	9C	15
	W(K,1,J)=A(K,J,1)	80	16
3	W(K,NF,J)=A(K,J,2)	BD	17
4	CONTINUE	BD	18
	RETURN	80	19
	END	80	20-
	SUBARRUTINE SETWP (PRES-NXSTA)	BE	1
	ENTRY ZETHP(PRES-NXSTA)	BE	2
C	ENINE ACTORIFICATION	BE	3
ᆫ	PHES = STATIC PRESSURE	BE	- 4-
Ğ	NXSTA = "X" STATION NO.	BE	· ·
C		BF.	0
č	"SETWO" AND "ZETWO" COMPUTES THE "W" AND "P" ARRAY FOR A GIVEN	RE	<u>.</u> .
Č	"X" STATION AT A CONSTANT STATIC PRESSURE.	BE	8
<u>c</u>		BE	9
	COMMON /NERD/ MF	BE	10
ι	NX=NXSTA	BE	11
	PP=PRES	ΒE	12
c _		BE	13
C		BE	14
	00 2 K=1.MF	BE	15
2	CALL PUNTZ (K,NX,PP)	BE	16
	RETURN	9 E	17
`c_		BΕ	18
	END	BE	19-
	SUBROUTINE SLICK	BF	1
С,		BF	2
	COMMON /ERDS/ W(21,60,4)	BF	3
	COMMON /NERO/ MF.NF.NT.MUFF.NEWKY	BF	4
ċ-:		BF	5
č	COMPUTE A SMOOTHING BASED ON 4-POINT NEIGHBORHOOD.	BF	6
č·–		BF	7
-	DO 2 J=2,NEHKY	BF	à
	00 C 0-277CM7.	8F	9
•	DO 1 K=2.MUFF	BF	10
	L=J+2	BF	ii
	RU=W(K+1.L.1)	BF	12
	RD=W(K-1,L,1)	BF	13 "
	RL=W(K,L-1,-1)	8F	14
	R=W(K,L,1) '	BF	15
,	RR=W(K,L+1,1)	8F	16
Ĭ	W(K,J,1)=BANDIT(RU+RD+RL+R+RR)	BF	17
2	CONTINUE	AF	18
		86	19
c_		BF	
c _	RESET AXIS AND HALL BOUNDARY.	BF	20
c C	RESET AXIS AND WALL BOUNDARY. DO 3 J=2.NF W(1.J.1)=W(1.J.2.1)		

_			100
3	W(MF,J,1)=W(MF,J+2,1)	BF	23
· · · · · · ·	Teeff . Act of tropic in the second control of the second control	8F	24 _
C	RESET LAST STATION	BF BF	25
·	DD 4 K=2,MUFF W(K,NF,1)=W(K,NF+2,1)	BF	26 27
4	RETURN	BF	28
Ċ.	RETURA	BF	29
L	END	BF	30-
	SURROUTINE SMOOTH (X.NX.NTIMES)	BG	1
•	SOURTION THE SHOULD TARMARATIMES!	BG	,
Ē	DIMENSION X(1) . Z(100)	BG	3
C	DIPENSION ACCOUNT	BG	4
<u> </u>	N=NX	86	- 3-
	NERD=N-1	BG	6
	LIMIT=NTIMES.	BG	7 -
	F=0.B125	BG	8
	F00=0,5-0,5*F	BG	9
С	1741-ABA 464-1	BG	10
<u> </u>	00 2 J=1.LIMIT	BG	11
	CALL EQUATE (Z,X,N)	BG	12
	00 1 K=2, NERO	BG	13
1	X(K)=F*Z(K)+F00*(Z(K+1)+Z(K-1))	BG	14
2 -	CONTINUE	BG	15
č		BG	16
<u> </u>	RETURN	BG	17
C		BG	ia .
	END	BG	19-
	SURROUTINE SNAFU (MM,NN)	BH	î
c -		BH	. 2
č	COMPUTE THE PARTIAL FUNCTIONS FOR A 3X3 SQUARE	BH	3
Č	WITH A CENTER POINT LOCATED AT Y=M . X=N .	BH	4
<u> </u>		BH	5
	COMMON / FROS / W(21,60.4)	BH	6
	COMMON /STUPID/ F(21,60)	BH	7
	DIMENSION A(4)	84	8
С		BH	ğ
	M=MM	BH	10
	N=NN	BH	11
		ВН	12
	KNUNT=0 ·	BH	13
Έ -		84	14
	00 2 KRUD=1,3	BH	15
	K=M+KRUD+2	BH	16
С		BH	17
	DO 1 JOLLY=1,3	BH	18
	J=N+J0LLY-2	BH	19
	KOUNT=KOU4T+1	" Вн	20
	A(1)=H(K,J,I)	ВН	21
	A(Z)=W(K,J,Z)	BH	22
		8H	23
	A(4)=W(K,J,4)	BH	24
	FUZZ=F(K,J)	BH	25
	CALL EVAL (A, KDUNT, FUZZ)	ВН	26
<u> </u>		ВН	27
T	CONTINUE	ВН	28
C		BH	29

2	CONTINUE	BH	30 31
<u>c</u>		BH	-32
·	RETURN	BH	33
c	REJURN	BH-	34
•	END	BH	35
	SUBROUTINE STAGG	81	-
:	Samorine Stage	61	ž
<u> </u>	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAH2;21),RGAS(21),		• 3
	1PZ(21),TZ(21),MZ(21),RHOZ(21)	AI	4
		BI	. 5
	COMMON /CPDATA/ CPSPEC(3,8),SPCHWT(8),NAME(8)	BI	ě
		BI	9
	COMMON /EROS/ 818,50),X(50),P(50),T(50),F(50),NSTAG	81	
	COMMON 7EIMITS? VMIN	BI.	٠,
	•	81	10
-		BI	11
	CALL CPEVAL	BI	12
,		BI	13
	CALL DREZ (A,420)	BI	14
		BI	1:
	GCJ=32.174#777.648	81	_14
	GRINCH=1.98726	BI	-1
	WENCH=GRINCH*GCJ	BI	- 11
		BI	ינ
	NS=21	81	20
	ÓNE=1.0 ·	BI	2
		81	22
	CALL HEAD6 .	81	2
:		BI	24
	READ (5,16) NSTAG	BI	2:
	WRITE (6,17) NSTAG	BI	20
	NX=NSTAG	BI	5.
:	INPUT DATA BASED ON FOLLOWING PARAMETERS:	81	21
	X - STREAMLINE FRACTION - 0.0 AXIS , 1.0 WALL	BI	2
:	P - PRESSURE (PSIA)	BI	30
	T, - TEMPERATURE (RANKINE)	BI	3
;	B - RELATIVE MASS	01	3
;		BI	3
	READ (5,18) (X(K),P(K),T(K),(B(J,K),J=1,8),K=1,NSTAG)	BI	34
	WRITE (6,11) NAME	BI	3
		BI	3
	WRITE (6,19) (K,X(K),P(K),T(K),(B(J,K),J=1,8),K=1,NSTAG)	BI	3
;		81	31
	CALL HEADS	BI	39
	المنظمة br>المنظمة المنظمة	BI	.40
;	NORMALIZE B'S AND CONVERT PSIA TO PSFA.	61	4
	ON 1 K=1.NSTAG	BI	42
•	P(K)=P(K)*144.0	BI	4
<u></u>	CALL NORMAL (B(1,K),8)	BI	44
;		BI	4
	WRITE (6,12) NAME	BI	4
	WRITE (6,19) (K,X(K),P(K),T(K),(B(J,K),J=1,B),K=1,NSTAG)	BI	4
;		61	41
	FURD=NS-1	BI	44
:	•	BI	50

	Dn 4 K=1.NS	BI	5
	TARGET=K-1	BI	5
	TARGET=TARGET/FURD	8 I	5
C		81	5
•	CALL LINEAR (TARGET, X, NX, F1, F2, J1, J2, NOCONI	81	5
C		BI	5
	IF (NOCON.NE.O) CALL BOMBER ('STAGG', NOCON)	BI	- 5
С		RI	5
-	PZ(K)=P(J1)*F1+P(J2)*F2	BI	5
	TZ(K)=T(J1)=F1+T(J2)=F2	81	6
•	FIK)=TARGET	BI	6
C		BI	6
Č		BT	6
~	SUM=0.0	BI	6
	DD 3 J=1,8	BI	6
		BI	6
c	Ÿ(J'K)=B(J'J])*EI+Ÿ(J'JS)*ES	BI	6
L	00.2 (-).2		
	DO 2 L=1.3	AI	<u>6</u>
2	CP(L,K)=CP(L,K)+A(J,K)*CPSPEC(L,J)	υī	-
c		91	7
_	SUM=SUM+A(J+K)/SPCMWT(J)	81	7
3	CONTINUE	8 [7
c		ВÍ	7
	HTM(K)=ONE/SUM	BI	7.
	RGASTK)=WENCH*SUM	81	7
4	CONTINUE	BŢ	7
C		BI	7
	DO 5 K=1.NS	BI	7
5 -	RHOZ(K)=PZ(K)/(TZ(K)*RGAS(K))	RI	7
C	CONVERT OF UNITS FROM BTU/LBM TO FT++2/SEC++2	A I	R
	DO 6 K=1,63	BT	B
6	CP(K+1)=CP(K+1)+GGJ	91	8
C —		6 I	8
	DO 7 K=1,NS	BI	B
	CV(1,K)=CP(1,K)-RGAS(K)	BI	8
	CV(2,K)=CP(2,K)	BI	8
	CV(3,K)=CP(3,K)	Br	-8
7	CONTINUE	BI	8
<u>;</u>		81	8
C .	MOTTE AC 121 NAME '		
	WRITE (6,12) NAME	81	9
L	Water 14 10 14 Flat 02141 72141 1114 41 1-2 01 4-1 No.	RI	9
	WRITE 16,19) [K,F(K),PZ(K),TZ(KI,(AIJ,KI,J=1,BI,K=1,NSI	<u> </u>	_9
C		RI	-9
	CALL HEAD6	91	9
	WRITE (6,13)	AI	9
	WRITE 16,20) [K,WTMIK),RGASIK),(CPIJ,KI,J=1,3I,(CVIJ,KI,J=1,3I,K=1		9
	1.NS) .	AI	9
<u> </u>		AI	_9
C	COMPUTE EFFECTIVE GAMMA AT STAGNATION	BI	-9
	WRITE (6,14)	BI	
c — -		BI	
	DO 8 K=1.NS	91	10
	HZ(K)=TZ(K)+(CP(ITK)+TZ(K)+(CP(2,K)+0.5+0.33333335+CP(3,K(+TZ(K(1)	BI	10
	G=CP(1,K)+TZ(K)*(CP(2,K)+TZ(K)*CP(3,K1)	91	10
	H=CV(1,K)+TZ(K)+(CV(Z,K)+TZ(K)+CV(3,K))	BI	10
	GAMMA=G/H		10

GAMZ (K)=GAMMA	BI	107
WRITE (6.15) K,GAMMA,G,H,HZ(K)	81	108
8 CONTINUE	81	109
C .	2111	110
C COMPUTE MAXIMUM SPEED OF SOUND		iii
DO 9 K=1.NS		112
X(K)=GAMZ(K)+RGAS(K)+TZ(K)		113
9 CONTINUE	_	114
C	-	115
K=21	8 [116
CALL MAXIE (X,K)	81	117
AMAX=SORTF(X(K))	B 1	118
VMIN=AMAX+0.15	BI	119
VMIN=AHAX+0.10		120
WRITE (6,10) K,AMAX,VMIN		121
RETURN	-	122
C - KETUKA		
		123
<u> </u>		124
C	BI	125
10 FORMAT (/20x, INDEX OF MAX. STAGNATION SOUND SPEED =1.13,3x, SPEE	BI	126
1D ='.F9.2, '(FT/SEC)'.5X, 'VM[N ='.F9.2, '(FT/SEC)' /)	81	127
11 FORMAT (/16x. STREAM FRACT 8x. STAGNATION 19x. RELATIVE MASS (BI	128
1F SPECIE 1/30X + PSIA 1 + 7X + T-R1 +8(5X + A4) /)		129
12 FORMAT (/30x · PSFA · •7x • 'T-R · •8(5x • A4)/)		130
13 FORMAT 1/20x, MOL WY., 5x, GAS CON. 17x, CP COEFFICIENTS, 22x, CV	BI	131
The state of the s		
	-	132
<pre>14 FORMAT (/20x, *STAGNATION EVALUATION* //32x, *GAMMA*, 10x, *CP*, 12x, *</pre>	BI	133
1CV*,10X,*ENTHAL* /)	91	134
15 FORMAT (20x,15,5x,F8,4,2x,1P3G15,6)	BI	135
16 FORMAT (1615)	BI	136
17 FORMAT (/20x. STAGNATION PARAMETERS ,5x, NO. INPUT POINTS= ,15/	BI	137
18 FORMAT (3E12.0.4X.8E5.0)		138
19 FORMAT (10x,15,F8.4,F12.3,F10.1,BF9.4)	_	134
20 FORMAT (10x,15,2X,1P8G13.4)		140
END		141
SURROUTINE START	BJ	1
COMMON /APE/ LINE(31)	BJ	2
DIMENSION LUSH(27) . KARD(20)	· BJ	3
EQUIVALENCE (LINE(1).LUSH(1).KARD(1))	BJ	4
DATA KRUD/'1 ***/,HUNG/******/,HUD/*%*<*/	BJ	5
1 READ (5.2.END=99) KARD	BJ	6
IF (KARDII).EQ.MUNG) CALL ENDJOB	BJ	7
IF [KARD(1) NE KRUD) GO TO 1	BJ	ė
		9
KARD(1)=MUO	81	_
LINE(31)=0	BJ	10
C	BJ	11
ENTRY HEADS	BJ	12
CALL PCL6	BJ	13
C	ŘJ	14
CALL TIME (IDIOT.NSECS)	BJ	15
MINUTE=NSECS/60	BJ	16
•		
NSEC=NSECS-MINUTE*60	BJ	17
KHOUR=MINUTE/60	BJ	18
	BJ	19
MINUTE=MINUTE-KHOUR#60		
MINUTE=MINUTE-KHOUR*60 Line(28)=Khour	BJ	20

	(INEI30)=NSEC	BJ	2
	LINE(31)=LINE(31)+1 WRITE (6,2) LINE	BJ	.2
	A # 7	BJ	2
"	RETURN		
44	CALL ENDJOB	BJ	3
	RETURN	83	3
L		BJ	2
-	ENTRY HEADB	AJ	2
	CALL PCLR	AJ	3
	WRITE (8.2) LUSH	BJ -	3
_	RETURN	BJ	3
<u>c</u>		RJ RJ	2
	ENTRY HEAD14	-	_
	CALL PCL14	. BJ	3
	WRITE (14,2) LUSH	BJ	
	RETURN .	BJ	3
ċ · ·		BJ	3
2	FORMAT (27A4,14,'1',12,'.',12,' PAGE',14/)	BJ	3
	END	BJ	4
	SUBROUTINE STATIC	BL .	
<u> </u>	COMMUNIC PRINCIPLE STATES BACKSHAP BLCT PARTIES	BL	
c	COMPUTE EXTREMALS STATIC PRESSURE DIST. FACTORS.	8L	
L	40000 440.54 4845 21 BUILD D.	BL	
	CN4MON /ARLE/ AX(21,2),BX(21,2)	BL	_
_	COMMON /EROS/ 8(8,50),X(50),P(50),T(50),F(50),S(50)	81.	
c	COHMON T/NERO/ ME.NE.NT.MUFF	BL	
_	COMMON /NERD/ MF.NF.NT.MUFF		
<u> </u>	PD 1 ' 1'. 2'	BL _	
	DO 1 K=1,42	BL	1
	BX(K,1)=0.0	BL BL	_
1	AX(K,1)=1.0 FURD=MUFF	BL	1
			. 1
	DO 2 K=1,MF TARGET=K-1	BL	1
	TARGET=TARGET/FURO	- AL BL	1
•	FIK)=TARGET	BL BL	1
2		BL.	i
	CALL HEADS	. BL	i
c	WRITE (6,11)	- BL	2
·	00 8 L=1.2	BL	2
	READ (5.14) NSTAT	- BL	1
	1F (NSTAT) 10.7.3	BL BL	ž
4	[F (NSTAT-21) 4,4,9	BL	÷
3 4	N=NSTAT	BL.	2
Ti.	READ (5,15) (X(K),P(K),S(K),K=1,N)	8L	2
	WRITE (6,12)	BL	2
	WRITE (6,16) (K,X(K),P(K),S(K),K=1,N)	8L	2
	MX=M	BL	ž
	DD 6 K=1,MF	BL	-
	TARGET=F(<)	BL	3
		BL	3
	CALL LINFAR (TARGET, X, NX, F1, F2, J1, J2, NOCON)	BL	3
5			1
7	Ax(K,L)=P(J1)=F1+P(J2)+F2	BL	_
	BX(K,L)=S(J1)*F1+S(J2)*F2 F(K)=TARGET	RL BL	-3

C WRIT	75 (4.12)	BL	38
THE WELL	TE (6,13) TE (6,16) (K,F(K),AX(K,L),BX(K,L),K=1,MF)	BL_	40
6 CONT	IC (D, LD) (K, P(K), AX(K, L), DX(K, L), K=L, MP)		41
CCON!	TINUE	BL	42
RETU	ION	BL	43
	BOMBER ('-STATIC-'.5)	BL	44
10 RETU		BL	45
c		BL	46
č		BL	47
	MAT TOZON FEXTREMAL STATIC PRESS. DIST. FACTORS " /)	BL	48
	MAT (18x,5HINPUT,6x,4HR/RW,6x,11HPRES, FACT,/)	BL	49
	MAT (/16X,8HCOMPUTEO,5X,4HR/RW,6X,11HPRES, FACT,/)	BL	50
	MAT (141E)	BL	51
L5 FORM		B)_	52
		BL	53
	MAT (20X,15,2X,3F10,5)		
END	DOUTING STORE	BL	54
SUBR	ROUTINE STORE	BM	$-\frac{1}{2}$
-	NOW JARY E. A. A. A.	AM	
	MON /ABLE/ AX(21,4)		3
	MON /APE/ KITLE, LABEL (19)	BM	4
	MON /COUNT/ L.LL	BM	5
	MDN /CPDATA/ TGFH(40)	BM	6
	MON /DELTAS/ OX,OY,DT,DY2,OT2,DT4	8M	_7
	MON /DUPFR/ HA(21) HB(21)	8H	- 8
	MON /EROS/ W121,60,4),P(21,60)	SM	9
	MON /FANG/ F(9,4),G(9,4)	BM	10
	MON /FLIGNR/ WEIGHT.PTHROT.PANIC	BM	. 11
	MON /FRAN/ AD(60), A1(60), BD(60), B1(60)	BM	12
	MON /FUBAR/ F1.F2.F3.F4.F5	BM	13
CONF	MON /FURD/ WMP(4),WMM(4),WMP(4),WMM(4),WMM(4)	BM	14
COMM	40N /LIMITS/ VMIN	RM	15
COMM	MON /NAVIER/ DTDx,OTDx2,DTDX4,DTDX8,DTOY,DTDY2,DTOY4,DTOY8 ¯¯¯ ˙	BM	16
	MON /NDEX/ INDEX(9)	BM	17
CUMP	MON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY	BM	18
COMM	MON /NITWIT/ CLOWN.VULGAR	BM	19
		.BM	20
	MON /SKALE/ SIMPLE(4)	BM	21
	MON /SPOR/ S(60).SO(60).SOP(60).SI(60).SIP(60).AREA(60)	BM	22
	MON /SPY/ KCLASS.KGROUP	BM	23
	MON /STAG/ AA(8,21),CP(3,21),CV(3,21),WTH(21),GAM2(21),RGAS(21)		24
	(21).TZ(21).HZ(21).RHOZ(21)	BM	25
	MON /STOKES/ A(60),B(60),H(60)	BM	26
	MON /STUPIO/ FOOL(21,60)	BM	27
	MON /SUPER/ R121,60)	BM	26
	MON /THERMO/ RHFJ(7)	BM	29
	MON /TYME/ T.FLIT	BH	30
	MON /WALL/ XWALL(100)	RM	31
	MIN /WARL/ XWALLING)	8M	- 31 32
CONF	MIN / FURN/ AIRALTTE TRIAT	BM	
CUMP	MON /SEXX/ NASTIE.IDIOT	-	33
5		BM	34
<u> </u>		BM	35
c****	102.2	BM	36
	IND 9	0/4	37
_up T1	TE (9) KITLE, LABEL, L, LL, TGFH, DX, DY, DT, DY2, DT2, DT4, HA, HB, W, P, F, G	RM	36

3 NEWS REAS AND AND SHOUL BY DUE ME ME MUTE I MATE MATERIAL		
2,DTDX4,DTDXA,DTDY,DTDY2,DTDY4,DTDY8,MF,NF,NT,MUFF,L1MIT,NASTY,CLD 3N,VULGAR,S,SO,SOP,SI,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,NTM,GAMZ,RGAS		40
4.PZ.TZ.HZ.RHDZ.A.B.H.FODL.R.RHFJ.T.FLIT.XTRA.PSIA.NPSIA.SIMPLE.XW		42
5LL.VMIN.AX.INDEX.AO.AI.BO.BI.NASTIE.IDIOT	BM	43
	BM	44
WRITE (14,1)	81	45
	BM	46
RETURN	BM	47
•	94	48
	BM	49
·	BM	50
ENTRY RESTOR	BH	51
READ (9) KITLE-LAREL-LILL-TGFH, DX.DY.DT, DYZ.DTZ.DTZ.HA, HB, W.P.F.G.	BM	32
LWEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WNP, WMM, WMN, OTDX, DTDX2,	RM	53
ZDTDX4.DTDX8.DTDY.DTDY2.DTDY4.DTDY8, MF.NF.NT.MUFF, LIMIT, NASTY.CLOWN	I BM	54
3.VILGAR,S.SO.SOP.SI.SIP.AREA,KCLASS,KGROUP.AA.CP,CV.WTM.GAMZ,RGAS,	BM	55
4PZ,TZ,HZ,RHOZ,A,B,H,FODL,R,RHFJ,T,FLIT,XTRA,PSIA,NPSIA,SIMPLE,XHAL	BM	56
5L,VMIN,AX,INDEX,AO,AI,BO,BI,NASTIE,IDIOT	BH	57
	RM	5 A
	BH	59
WRITE (6-2)	BH	60
	RM	61
RETURN TO THE TOTAL THE TOTAL TO AL TO THE T	BM	62
·	BH	63
	BM	64
FORMAT ('1',20x,'STORED ON NINE' /)	PМ	65
FORMAT ('1',20%, RESTORED FROM NINE'/)	BM	66
_ END	BM	67
SUBROUTINE STREAM	BN	1
	BN	2
COMPUTE THE STREAM FUNCTION "F" FOR EACH POINT IN THE FIELD.	BN	- 3
	RN	4
INTEGRATE THE MASS INTEGRAND W(+,+,2) = RHO+U+R	BN	5
THEN NORMALIZE THE RESULTS.	BN	6
	BN	?
CUMMIN /ESOS/ M(21,60,5)	BN	8
COMMON /NERD/ MF, NF, NT	BN	_ 9
COMMON /STUPIO/ F(21,60)	91	10
	AN	11
	RN	12
DO 3 NX=1,NF		13
F(1,NX)=0,0	BN	
F(l+NX)=0.0 DO 1 K=2,MF	BN	_
F(1,NX)=0,0	BN BN	75
F(l+NX)=0.0 DO 1 K=2,MF	BN BN BN	15
F(1.NX)=0.0 DO 1 K=2.MF F(K,NX)=F(K-1.NX)+0.5*(W(K-1.NX,2)+W(K,NX,2))	BN BN BN BN	15 16 17
F(l+NX)=0.0 DO 1 K=2,MF	BN BN BN BN BN	15 16 17 18
F(1.NX)=0.0 DO 1 K=2.MF F(K,NX)=F(K-1.NX)+0.5*(W(K-1.NX,Z)+W(K,NX,Z)) NORMAL1ZE	BN BN BN BN BN BN	15 16 17 18 19
F(1.NX)=0.0 DO 1 K=2.MF F(K,NX)=F(K-1.NX)+0.5*(W(K-1.NX,Z)+W(K,NX,Z)) NORMALIZE DO 2 K=1.MF	BN BN BN BN BN BN BN	15 16 17 18 19 20
F(1.NX)=0.0 DO 1 K=2.MF F(K,NX)=F(K-1.NX)+0.5*(W(K-1.NX,Z)+W(K,NX,Z)) NORMAL1ZE	BN BN BN BN BN BN BN BN	15 16 17 18 19 20
F(1,NX)=0.0 DO 1 K=2,MF F(K,NX)=F(K-1,NX)+0.5*(W(K-1,NX,Z)+W(K,NX,Z)) NORMALIZE DO 2 K=1,MF F(K,NX)=F(K,NX)/F(MF,NX)	BN BN BN BN BN BN BN BN BN	15 16 17 18 19 20 21
F(1.NX)=0.0 DO 1 K=2.MF F(K,NX)=F(K-1.NX)+0.5*(W(K-1.NX,Z)+W(K,NX,Z)) NORMALIZE DO 2 K=1.MF	BN BN BN BN BN BN BN BN BN	15 16 17 18 19 20 21 22 23
F(1,NX)=0.0 DO 1 K=2,MF F(K,NX)=F(K-1,NX)+0.5*(W(K-1,NX,Z)+W(K,NX,Z)) NORMAL 1ZE DO 2 K=1,MF F(K,NX)=F(K,NX)/F(MF,NX)	BN BN BN BN BN BN BN BN BN BN	15 16 17 18 19 20 21 22 23
F(1,NX)=0.0 DO 1 K=2,MF F(K,NX)=F(K-1,NX)+0.5*(W(K-1,NX,Z)+W(K,NX,Z)) NORMAL1ZE DO 2 K=1,MF F(K,NX)=F(K,NX)/F(MF,NX) CONTINUE	BN BN BN BN BN BN BN BN BN BN BN BN	14 15 16 17 18 19 20 21 22 23 24 25
F(1,NX)=0.0 DO 1 K=2,MF F(K,NX)=F(K-1,NX)+0.5*(W(K-1,NX,Z)+W(K,NX,Z)) NORMAL 1ZE DO 2 K=1,MF F(K,NX)=F(K,NX)/F(MF,NX)	BN BN BN BN BN BN BN BN BN BN	15 16 17 18 19 20 21 22 23 24

	COMMON /EROS/ W(21,60,4),P(21,60)	80	3
	COMMON /COUNT/ L.LL	80_	
	COMMON /NOEX/ INDEX(9)	BO	5
	COMMON /NERD/ MF.NF.NT	80	6
	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21), 1PZ(21),TZ(21),HZ[21),RHOZ(21)	BO	7
<u> </u>	1PC121741212174HZ12174HHDZ1217	BD	- 8
u	DIMENSION X(9), Y(9)	BO	10
c	DIMENSION X(9), Y(9)	BO	-iĭ
•	J=M∩D(L+1,25)	80	12
	J=M()0(L-1,25) [F (J.NE.O) GO TO 1	80	13
	CALL HEAD14	BD	14
	WRITE (14.5) INDEX	80	15
C		30	16
i	CONTINUE	BO	17
		50	18
	DO 2 K=1.9 J=[NDEX(K)	80	19
	MANA BANG ANAMANGA	90	20
	Y(K)=P(MF,J)/PZ(MF) Y(K)=P(1,J)/PZ(I)	BO	21
2		80	22
c—	CONTINUE	80	23
•	WRITE (14,3) X.L	BO	24
	WRITE (14.4) Y	BO	25
C	HOLIC 117477	80	26
	RETURN	BO	27
C	RETURN .	BO	28
<u>-</u>		BO	29
Č		80	30
3	FORMAT (1X,9F12.4,18)	BO	31
4	• FORMAT (7X,9F12.4)	BO	32
<u> </u>	FORMAT (/20X,30H(P/PO) WALL/AXIS RESPECTIVELY//1X,9112/)	BG	35
•	END	80	34-
	SUBROUTINE TROPIC (PO.TO.PSTAT.F.DEN. VEL. EASY)	BP	1
C	INPUT COMPUTED	90	2
ั้द		AP	3
č	COMPUTE STATIC DENSITY. VELOCITY. AND "E" INTEGRAL	BP	4
ट -	FOR AN ISENTROPIC EXPANSION FROM GIVEN	BP	
č	STAGNATION CONDITIONS FOR A REAL GAS OF THE FORM:	BP	6
č	CP = A0 + A1+T + A2+T++2 & P = RHO+R+T	BP.	- 7
č	CF - AU T AITH T AZTITUE & F - KNUTKYI	BP	B
Č	PO + STAGNATION PRESSURE	BP	9
č	TO - STAGNATION TEMPERATURE	BP	10
č	PSTAT - STATIC PRESSURE	BP	11
Č	F - STREAMLINE VALUE	BP	42
č	T. C. SINEMBLINE ANDRE	BP	13
Č	OEN - STATIC DENSITY	BP	14
č	VEL - VELOCITY	AP	15
-	EASY - SUM OF INTERNAL + KINETIC ENERGY PER UNIT VOLUME	BP	16
<u> </u>	LMSI - SUT UP INICHNAL Y NINCIIL CHERUT FER UNII VULUNC	BP	17
-	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21),		18
		BP	19
	COMMON /THERMO/ CPX(3).CVX(3).RAG	BP	20
	COMMON /LIMITS/ VMIN	BP	20
		0.5	
 c	Chillies (C11113) VIIII	80	22
 <u>C</u>	OWNER PETITION	BP	22

	PO=PO	BP	25
	TO=TO	BP	26
	P=PSTAT	BP	27
	FUZZ=F	AP	28
		BP	29
•	PRAT=P/PO	BP	30
-	PRATEFFE	BP	31
•	T-WANKY/CDY. DBAT. TO. BAC.	BP	32
	T=HANKY(CPX,PRAT,TO,RAG)	BP	33
	RHO=P/(T*RAG)	_	
	DEN=RHO	BP	34
ב" -		BP	35
	OH=HOTS (CPX,T,TO)	BP	36
	VELOC=SQRTF(DH+DH)	ВР	37
	VELOC=AMAXI (VELOC.VMIN)	BP	38
	VEL=VELOC	RP	39
5		BP	40
	HO=HZERO(FUZZ)	BP	41
	E=HD*RHD-P	BP	42
	EASY=E	BP	4
;		BP	44
	RETURN	BP"	45
	END	BP	46
	FUNCTION TSTAG (CP, TSTAT, VSOR)	80	1
	DIMENSION CP(3)	80	. :
	DIMENSION CP(3)	BQ	<u></u>
•	T_T(TAT		
	T=TSTAT	BQ	- 4
	H=VSOR+0.5	RΩ	
	A=CSUBP(TSTAT)	BO	-
C		BQ	- 7
	TZ=T+W/A	90	
	DO 1 K=1,5	AO	- 5
	H=HNTS(CP,T,TZ)	AU	10
	ERROR=N-H	BQ	11
	CPTZ=CSU8P(TZ)	BO	12
	DT=ERROR/CPTZ	80	13
	TZ=TZ+DT	80	14
	CONTINUE	BO	Ţ
	•	80	10
	TSTAG=T2	80	i
;	13.55=12	BQ	i
	RETURN	80	i
	END	80	20
	SUBROUTINE WEIRDO	BR	
<u>; </u>		RR	2
	COMMON /EROS/ W(21,6074),P(21,60)	BR	3
	COMMON /NERD/ M.N.NT.MUFF.LIMIT.NEWKY	BR	- 1
		BR	-
	ON 3 I=1.NEWKY	BR	
	K=M-I	BR	
;		BR	- (
	00 2 J=2,LIMIT	BR	•
	DQ 1 L=1,4	BR	10
_	₩(KŢJŢC)=₩(K-1,J-[ŢC)	BR	ī
4	CONTINUE	BR	i
		BP	-
3	CONTINUE	BR	14

DO 5 K=2,MUFF DO 4 J=2,LIMIT 4 P(K,J)=PVNTS(W(K,J,1)*W(K,J,4)*K,J) 5 CONTINUE C RETURN	BR BR BR	75
DO 4 J=2.LIMIT 4 P(K.J)=PVNTS(W(K.J.1).W(K.J.4).K.J) 5 CONTINUE C RETURN		16
4 P(K,J)=PVNTS(W(K,J,1),W(K,J,4),K,J) 5 CONTINUE C RETURN		17
5 CONTINUE CRETURN	BR	18
C RETURN		
RETURN	BR	19
	BR	20
END	BR	21
END	BR	22-
FUNCTION XMASS (NXSTA)	Be	1
C COMPUTE THE MASS FLOW AT A GIVEN **X* STATION NO.	BS	2
C . COMPUTE THE MASS FLOW AT A GIVEN "X" STATION NO.	BS	3
C TRAPEZOIDAL INTEGRATION OF THE RHO+U+R TERM.	BS	4
C TRAPEZOIDAL INTEGRATION OF THE RHO*U*R TERM.	85	- 5
		-
C NOTE: "W" ARRAY MUST BE PREVIOUSLY COMPUTED	BS	6
C T	BS	7
COMMON /EROS/ W(21.60,4).P(21.60)	BS	B
COMMON /NERD/ MF.NF.NT.MUFF	BS	9
COMMON (SPOR) S(60)	BS	10
C	85	11
K=NXSTA	85	12
SUM=(W(1,K,2)+W(MF,K,2))+0.5	BS	13
C	BS	14
00 1 J=2;40FF	BS	15
1 SUM=SUM+W(J.K.2)	AS	16
c	BS	17
XMASS=SIJM+S(K)	BS	18
C	BS	19
RETURN	AS	20
C	BS	21
END	95	22-
BLOCK DATA	81	
		-
C	BT	Ž,
	BT	
COMMON /CPDATA/ CP(3,8),WTH(8),NAME(8)		3
	BT	3
COMMON /CPDATA/ CP(3,8),WTH(8),NAME(8)	- 8T	3 4 5
COMMON /CPDATA/ CP(3,8).WTM(8).NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300)		3 - 4 - 5
COMMON /CPDATA/ CP(3,8).WTM(8).NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260)	BT BT	
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260)	BT BT	6
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260)	BT BT BT	6 7 8
COMMON /CPDATA/ CP(3.8), WTM(8), NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS	BT BT BT BT	6 7 8 9
COMMON /CPDATA/ CP(3.8).WTM(8).NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE ÜNITS OF BTU/LB.MASS C	BT BT BT BT BT	6 7 8 9
COMMON /CPDATA/ CP(3.8).WTM(8).NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04.	BT BT BT BT BT BT	6 7 8 9 10
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE ÜNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842	BT BT BT BT BT BT BT E ST	6 7 8 9
COMMON /CPDATA/ CP(3.8).WTM(8).NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04.	BT BT BT BT BT BT BT E ST	6 7 8 9 10
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842	BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12
COMMON /CPDATA/ CP(3.8).WTM(8).NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08.0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3.22600,1.757600E-04,1.0E	BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /PGMNO/ NPROG(5) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E-408/	87 87 87 87 87 87 87 87 87 87 87	6 7 8 9 10 11 12 13 14 15
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/	8T 8T 8T 8T 8T 8T 8 3T 5 8T 8 7 8 7	6 7 8 9 10 11 12 13 14 15 16
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE ÜNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04, 14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08.0.190481,5.646879E-05,-9.812500E-09,0.246445,-3. 364750E-06,1.251100E-08,0.124349,0.0,0.0,3.22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/	8T 8T 8T 8T 8T 8T 8 3T 5 8T 8T 8T 8T	6 7 8 9 10 11 12 13 14 15 16 17
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04, 14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3. 364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39,944,2.016/	8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T	6 7 8 9 10 11 12 13 14 15 16 17 18
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /PGMNO/ NPROG(5) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C OATA NAME/*AIR*,*CO2*,*CO*,*HZO*,*O2*,*N2*,*A*,*H2*/	8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T	6 7 8 9 10 11 12 13 14 15 16 17 18
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.24645,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C OATA NAME/*AIR*, 'CO2*, 'CO*, 'HZO*, 'OZ*, 'NZ*, 'A*, 'HZ*/	8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T	6 7 8 9 10 11 12 13 14 15 16 17 18
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /PGMNO/ NPROG(5) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C OATA NAME/*AIR*,*CO2*,*CO*,*HZO*,*O2*,*N2*,*A*,*H2*/	8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T 8T	6 7 8 9 10 11 12 13 14 15 16 17 18
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE ÜNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05.7.166000E-09.0.120765.1.720251E-04. 14.235305E-08.0.2615315.179134E-05.1.07508E-07.0.430062.1.676842 2-05.2.778587E-08.0.190481.5.646879E-059.812500E-09.0.2464453. 364750E-06.1.251100E-08.0.124349.0.0.0.0.3.22600.1.757600E-04.1.0E 408/ C DATA WTM/28.97.44.011.28.011.18.016.32.000.28.000.39.944.2.016/ C DATA NAME/*AIR*, 'CO2*, 'CO*, 'HZO*, 'O2*, 'N2*, 'A*, 'H2*/ C DATA NAME/*AIR*, 'CO2*, 'CO*, 'HZO*, 'O2*, 'N2*, 'A*, 'H2*/ C DATA KR71260+0/	BT BT BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12 13 14 15 16 17 18
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPRGG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04, 14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3. 364750E-06,1.251100E-08,0.124349,0.0,0.0,3.22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C DATA NAME/*AIR*,'CO2*,'CO*,'H2O*,'U2*,'N2*,'A*,'H2*/ C DATA NAME/*AIR*,'CO2*,'CO*,'H2O*,'U2*,'N2*,'A*,'H2*/ C DATA KR/IZ60+0/	BT BT BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C DATA NAME/*AIR*, "CO2*, "CO*, "HZO*, "OZ*, "NZ*, "A*, "HZ*/ C DATA KR/1260+0/ C DATA KW/6300+0/	BT BT BT BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /PGMNO/ NPROG(5) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE C UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.24645,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C DATA NAME/*AIR*,'CU2*,'CU*,'HZU*,'UZ*,'NZ*,'A*,'HZ*/ C DATA KW/3300+0/ INTEGER*4 NPROG/*SER00238 (08-18-72) */	BT BT BT BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24
COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8) COMMON /PGMNO/ NPROG(5) COMMON /EROS/ KW(6300) COMMON /SUPER/ KR(1260) C C CP COEFFICIENTS FOR EACH CHEMICAL SPECIE UNITS OF BTU/LB.MASS C DATA CP/0.231800,1.040000E-05,7.166000E-09,0.120765,1.720251E-04,14.235305E-08,0.261531,-5.179134E-05,1.07508E-07,0.430062,1.676842 2-05,2.778587E-08,0.190481,5.646879E-05,-9.812500E-09,0.246445,-3.364750E-06,1.251100E-08,0.124349,0.0,0.0,3,22600,1.757600E-04,1.0E 408/ C DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/ C DATA NAME/*AIR*, "CO2*, "CO*, "HZO*, "OZ*, "NZ*, "A*, "HZ*/ C DATA KR/1260+0/ C DATA KW/6300+0/	BT BT BT BT BT BT BT BT BT BT BT BT BT	6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23

Choked Version

	UDE SYSTFORT	-	-
CHIK	REAL GAS TIME-DEPENDENT ANNULAR NOZZLE FLOW.	A	
	RUN ON IRM 370/155 ARNOLD ENGINEERING DEVELOPMENT CENTER.	Ā	
	TULLAHOMA. TEMNESSEE.37389.	Ā	
	FOR INFORMATION CONCERNING THIS PROGRAM CAONTACT.	Â	
	ENGINEER SAM WEHNFER PHONE. 615-455-2611 EXT 533.	Ã	
	ANALYST W. C. MOGER PHONE. 615-455-2611 EXT 7131.	Ā	
	The second secon	Ã	
	DATA K8/8/-K14/14/	A	
	WRITF (6.1)	Ā	1
	WRITE (8.2) KB	-	٦
	WRITE (14,2) K14	A	ī
-	CALL SER142	A	i
	CALL ENDJOB	Ä	1
-	CALL EXIT	À	ī
	STOP	A	i
		A	٦
	FORMAT ('1',20x, PROGRAM NO. SEROO142 AUG 8,1972 1/)	A	i
•	FORMAT ('1'.20X. OUTPUT FROM DATA SET NO. 113/10')	A	i
	END	A	2
	FUNCTION RANDIT (X1.X2.X3.X4.X5)	В	
	CHMMON /FURAR/ F1.F2.F3.F4.F5	8	
	GAN=F1 *x1+F2*X2	В	_
	\(\bar{D}\)1T=F3+X3+F5+X5	В	
	RAND(T=RAN+DIT	В	
	RANDIT=RANDIT+F4=X4	8	
	RETURN	B	
	END	8	
	SURROUTINE REDEAM	C	_
	COMMON /FLIGHR/ WEIGHT.PTHROT.PANIC	С	
	COMMON /COUNT/ L.LL	С	
	COMMON /NERD/ ME.NE.NT	C	
	DIMENSIAN A(3), X(3), Y(3)	С	
_	ZERO=0.0	C	
	CALL PMIN (PANIC)	C	
	KLOH=0.3*PANIC	, C	
	DELX=0.005000001+PANIC	Ċ	
	JERK=0	C	- 1
	DD 1 K=1.3	C	
	X(K)=XLNW+(K-1)+DFLX	<u> </u>	_ 1
	CALL SETUP (XIK).NT)	<u> </u>	
	Y(K)=XMASS(NT)	C	1
	CONTINUE	C	1
	DO 2 K=1,69	Ç	1
	JERK=K	C	- 1
	CALL PARAS (X,Y+A)	<u> </u>	_ [
	IF (A(3),ED,ZERO) A(3)=1.00+69		
	XTEST=-0.5*A(2)/A(3)	C	- 3
	IF (A(3).GE.ZERO) GO TO 3	C	
-	IF ((X(1).LE.XTEST).AND.(X(3).GE.XTEST)) GO TO 4	Č	3
	X(1)=X(2)	Č	
	Y(1)=Y(2)	— ᡶ	-
	X(Z)=X(3)	Č	

	X(3)=X(3)+DELX	C	2
	CALL SETWP (X(3).NT)	č	2
	Y(3)=XMASS(NT)	<u>c</u> —	2
>	CONTINUE	č	3
<u>2</u> ,	CONTINUE	č	3
	CALL BOMBER ('BEDLAM', JERK)	č	3
	RETURN	C	3
	CONTINUE	č	3
<u></u>	CALL SETHP (XTEST, NT)	č	3
•	WEIGHT=XMASS(NT)	č	3
	PTHRDT=XTEST	Č	3
	WRITE (6.5) WEIGHT.PTHROT.PANIC	č	3
	RETURN	č	3
C	70.1004	č	4
<u> </u>	FORMAT (/20x, 'WEIGHT=",1PG15.6,3X, 'PTHROT=",G15.6,3X, 'PANIC=",G15		4
•	1.6 /)	-	4
	END		4
	- 12 /	D	7
	SUBROUTINE BNORY	8	-
6		_	
	COMMON /DELTAS! DX.DY.DT.DY2.DT2.DT4	D	
	COMMON /SUPER/ R(21.60)	D	
	COMMON /SPOR/ \$(60).50(60).50P(60).\$1(60).\$1P(60).AREA(60)	Ð	
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT	D	-
	COMMON /EROS/ W(21,60,4),P(21,60)	<u>D</u>	_
	DATA ZERD/O.O/.ONE/1.O/	D	
	COMMON /FRAN/ AD(60) +A1(60) +B0(60) +B1(60)	D.,	
_	DIMENSIAN PP(100)	D	1
<u></u> C			1
C	COMPUTE OUTER BOUNDARY PRESSURES	D	1
	DD 1 K=1,60	D	1
į.	PP(K)=P(MF.K)	D	1
<u> </u>		D	1
	DO 2 K=2,(1M17	0	1
	X=W(MF,K,2)+*2/W(MF,K,1)	Đ	1
	X=X/SUIK) .	D	1
	DP=0.5*(PP(K+1)-PP(K-1))	D	1
	CORR=BO(K) *DP-AD(K) *X	D	2
	P(MF,K)=P(MF-1,K)+CORR	D	2
2	CONTINUE	D	2
	DO 3 K=2.LIMIT	D	2
_	SOPK=SOP(K)	D	2
	DINGLE=NNE+SOPK**2	D	2
	DANGLE=SORTF (DNE/DINGLE)	D	ž
	CALL GRONK (ONE,P(MF,K),RHO,VEL,EASY)	D	ž
	W(MF.K.1)=RHO+R(MF.K)	ō	ž
	W(MF,K,2)=RH()*R(MF,K)*VEL*DANGLE	D	2
	W(MF.K.3)=W(MF.K.2)+SOPK	D	3
3	W(MF.K.4)=EASY*R(MF.K)	ŏ	3
		D	3
	DO 4 K=1,60	D	
4	PP(K)=P(1,K)		3
	DO 5 K=2+LIMIT	D	3
	X=W(1,K,2]**2/W(1,K,1)	D	3
	X=X/SI(K)	D	3
	DP=0.5*(PP(K+1)-PP(K-1))	D	3
	CDRR=BI(K)*DP-AI(K)*X	Ð	3

C		0	40
·	DD 6 K=2.LIMIT	D	41
	SIPK=SIP(K)	p	-42
	DINGLE=NNE+SIPK##2	Ď	43
·	DANGLE=SORTF (ONE/DINGLE)	Ď	44
	CALL GRONK (ZERO,P(1,K),RHO,VEL,EASY)	Ď	45
	W(1,K,1)=RHO*R(1,K)	'n	46
	W(1,K,2)=RHO+R(1,K)+VEL+DANGLE	Ď	47
	W(1,K,3)=W(1,K,2)*SIPK	ñ	40
6	W(1.K.4)=EASY+R(1.K)	D	49
č		Ď	50
•	RETURN	Ď	51
	END	D	52-
	SUBROUTINE BOMBER (NAME, KODE)	F	ĩ
	DIMENSION NAME(2)	Ė	2
	WRITE (6.1) NAME(1).NAME(2).KODE	Ē	3
	CALL ENDJOB	Ē	4-
	CALL EXIT	È	5
	RETURN	<u>−È</u>	-6
	RETURN	E	7
<u>C</u>	FORMAT 1/20X, BOMB-OUT IN 1,244, 3X, CODE=1, 15/)	Ē	8
	END	E	9-
	SUBROUTINE CARDIN	F	1
		F	2
	COMMON /SPY/ KCLASS-KGROUP	<u></u>	
	CALL DEMON		4
			-
	READ (5,3) KCLASS-KGROUP		5
	WRITE (6,8) KCLASS,KGROUP		_ 6.
	CALL FOLASS	F	7
	NO 2 K=1,6969	<u> </u>	- 8
	READ (5,4,END=9) KARD	-	•
	IF (MOD(K-1,50),NE.0) GO TO 1	F.	10
	CALL PCL6	F	11
	WRITE (6.7)	F.	12_
1	HALIE (047) KAKUAK	F	13
2	CONTINUE	F	14
	9 REWIND 5	_ F1	15
	WRITE (6,6)	F	16
_	RETURN	-	17
<u> </u>		-	18
3	FORMAT (1615)	-	19
4	FORMAT (20A4)	<u></u>	20
5	FORMAT (10X,20A4,3X,15)	-	51
6	FORMAT (2x,50('*'),' END OF INPUT DATA ',50('*'))	F	22
7 -	FORHAT (18x. INPUT DATA CARD IMAGE PROGRAM NO. SEROO142 /)	F	23
8	FORMAT (/20X, 'SECURITY CLASS AND GROUP CLASS=',15,' GROUP=',15/)	. F	24
	END	F.	25-
	SUBROUTINE COVO (CLAP, VENUS, PUNTZ, NASTY)	G	1
•	COMMON /EROS/ W(21,60,4),P(21,60)	G	Z
	COMMON /NELTAS/ DX.DY.DT	G	3
	COMMON /NERD/ M.N.NT.MUFF	G	4
	COMMON /SPOR/ \$(50)	G	5
	COMMON / SUPER/ R(21,60)	G	6
	NX=NASTY	G	7
	CD=(W(H,NX,Z)+W(1,NX,Z))+U.5	G	B
	VD=(H(M,NX,2)++2/H(M,NX,1)+H(1,NX,2)++2/H(1,NX,1))+0.5	G	9

	PUNE=(P(H,NX)+R(H,NX)+P(1,NX)+R(1,NX))+0.5	6 10
	DO 1 K=2, MUFF	G 10 G 11
	CD=CD+W(K,NX,2)	G-12
	VD=VD+W(K,NX,2)**2/W(K,NX,1)	G 13
	PUNE=PUNE+P(K,NX)+R(K,NX)	G 14
	SEX=S(NX)+DY+2.0	G 15
	CLAP=SEX*CD	G 16
	VENUS=SEX+UD	6 17
	PUNTZ=PUNE*SEX	G 18-
	RETURN	G 19
	END	G 20-
	SUBROUTINE CIPORT (PO, TO, DEN, FUZZ, PSTAT, TEMP, VEL, EASY)	H 1
	COMMON /LIMITS/ VMIN	· H 2
	COMMON /THERMO/ CPX(3),CVX(3),RAG	H 3
— 	CONTINUE	·· ;; 4
	* - - - - - - - - - -	
	ZERO=0.0 PZ=PO	H - 5
	72-70 TZ=TO	и н 7
	RHO=OEN	H 8
	F=FUZZ	H 9
	RRATIO=RHO+RAG+TZ/PZ	· ·- ·- H 10
-	AZ=CVX(1)	H 11
	A1=CVX(2)	H- 12
	A2=CVX(3)	H 13
	X=RRATIO	H 14
	RGAS=RAG	H 15
	POWER=RGAS/AZ	H 16
	FUDGE=X**PDWER	H 17
	BARF=A1/AZ	H-18
	TRAF=A2+0.5/AZ	H 19
	1217	H 20
	DO 2 K=1.5	H 21
	TTZ=T/TZ	
	EPAR=(T2-T)*(BARF+(TZ+T)*TRAF)	H 23
	XLAX=EXP(EPAR)	'H24
	TRAT=XL AX*FIJOGE	H 25
	TCOMP=7RAT+T2	H 26
	ERROR=TCOMP-T	H 27
	T=TCOMP	H 28
2	CONT INUE	H 29
_ 2	PRES=T*RHO*RAG	· · H 30
	DH=HOTS(CPX.T.TZ)	H 31
	VELCC=SORTF(DH+DH)	H 32
	VELOC=AMAX1(VELOC,VMIN)	H 33
	HO=HZERO(F)	H 34
	E=HO+RHO-PRES	H 35
	PSTAT=PRES	
	AFT=AFTOC	H 36 H 37
	VEL=VELUC EASY=E	H 38
•	TEMP=T	H 39
	RETURN	
	END	H 41-
	SUBROUTINE CPEVAL	1 1.
	COMMON /CPDATA/ CP(3,8),WTM(8),NAME(8)	1 2
	DATA KRUD/*PERF*/	
	DIMENSION X(8), Y(8)	i 4
	MINISTOR ALUTY TIOT	• • • • • • • • • • • • • • • • • • • •

-	INTEGER+4 LBMASS(4)/*CP(B*.*TU/L*.*BMAS*.*S-R1*/	40
	+ LBMOLE(4)/*CP(8*.*TU/L*,*BMOL*,*E-R)*/	41
	* . KGAMMA(4)/'CP/C','V GA','MMA ',' '/	42
	READ (5.10) NOMEN.ADDA	1 5
_	IF (NOMEN.NE.KRUD) GO TO 3	1 6
	00 2 J=1,8	1 7
	00 1 K=2,3	1 8
ı	CP(K+J)=+0.0	1 9
2	CONTINUE	1 10
	CP(1.1)=0.24009	1 11
3	CONTINUE	1 12
	NC P=19 .	1 13
	R=1.98726 .	7 74
	CALL HEAD6	1 15
	WR(TE (6.11)	I 16
	HRITE (6.12) (K.NAME(K).HTM(K).(CP(J.K).J=1.3).K=1.8)	I 17
	WRITE (6.14) NAME-LBMASS	1 18
	DO 5 J=1.NCP	1 19
	A=1-1	1 20
	A=A+ADDA	I 21
	T=A+100.0	1 22
	DO 4 K=1.8	1 23
_	X(K)=CP(1,K)+T*(CP(2,K)+CP(3,K)+T)	1 24
4	CONT INVE	1 25
	WRITE (6,13) Y,X,Y	26
	IF (MOD(J.5).EQ.O) WRITE (6.16)	1 27
5	CONTINUE	1 28
	WRITE (6.15)	1 29
	WRITE (6.14) NAME, L'BMOLE	1 30
	On 7 J=1.NCP	1 31
	,A=J-1	32
	A=A+ADDA	1 33
	T=A*100.0	1 34
	00 6 K=1.8	1 35
	X(K)=CP(1,K)+T+(CP(2,K)+CP(3,K)+T)	I 36
	X(K)=X(K)+WTM(K)	1 37
ठ	CONTINUE	1 38
	WRITE (6.13) T.X.T	1 39
	IF (MODIJ-5):E0.0) WRITE (6:16)	1 40
7	CONTINUE	I 41
-	WRITE (6-14) NAME-KGAMMA	1 42
	DN 9 J=1.NCP	1 43
	A=J-1	1 44
	A=A+ADDA	1 45
	T=A*100.0	1 46
	DO 8 K=1.8	1 47
	X(K)=CP(1,K)+T*(CP(2,K)+CP(3,K)+T)	1 48
	X{K}=X{K}+WTM(K)	1 49
-	FUZZ=X(K)-R	1 50
	Y(K)=X(K)/FUZZ	1 51
-8		1 52
	WRITE (6,13) T.Y.T	1 53
	TF (MOD(J;5),E0.0) RRITE (6,16)	1 54
9	CONT INUE •	1 55
_	RETURN	1 50
_		1 67

11	FORMAT (44.E16.0) FORMAT (* '.20x. CP DATA' //20x. CDEFFICIENTS FOR CP(BTU/LB.MASS)	1 58 1 59
	1= F(T-RANKINE): //23x,'MOL. HT.',5x,'AO',10x,'A1+T',13x,'A2+T++2')	60
12_		61
13	- MONOR	1 62
14	FIRMAT (/12x, 'RANKINE', RX, 8 (A4, 5X), 2x, 4A4/)	1 63
15	FORMAT (*1*)	1 64
16		1 65
	END) 66-
	FUNCTION CSUBP (TEMP)	j i
	COMMON /THERMO/ CP(3)+CV(3)	J 2
		J 3
	C=CP(1)+T=(CP(2)+CP(3)+T)	J 4
	CSURP=C	J 5
	RETURN	J 6
	ENTRY CSUBV(TEMP)	J7
	T=TEMP	J B
	C=CV(1)+T*(CV(2)+CV(3)*T)	J 9
		J 10
	RETURN	J .11
••		J 12-
		K 1
		K 2
		Ř -3
		\ 4
		_
		K 6
		K 7
		K B
		K 9
		K 10
	- 1.7.3.0 (0.7.10.1)	K 11
		K 12
		K 13
		K 14
	EAST=A(N+1)*Y+B(N+1)	K 15
	WEST=A(N-1)+Y+R(N-1)	K 16
	ANYR=A(N)=Y+B(N)	K 17
	FUDGE=A(N)+DY2	K 18
	MANAGE AND CHARGE	
	YANKEE=ANYB+FUDGE .	K 19
		K 19 K 20
	REBEL=ANYB-FUDGE	K 20
	REBEL=ANYB-FUDGE CALL SNAFD (M.N)	K 20 K 21
	REREL=ANYB-FUDGE CALL SNAFU (M.N) DD 1 K=1.4	K 20 K 21 K 22
	REREL=ANYB-FUDGE CALL SNAFD (M.N) DD 1 K=1.4 F64=F(6.K)-F(4.K)	K 20 K 21 K 22 K 23
	REREL=ANYB-FUDGE CALL SNAFD (M.N) DD 1 K=1.4 F64=F(6.K)-F(4.K) - G82=(G(8.K)-G(2.K))+HN	K 20 K 21 K 22 K 23 K 24
	REREL=ANYB-FUDGE CALL SNAF() (M.N) DD 1 K=1.4 F64=F(6,K)-F(4,K) - G82=(G(R,K)-F(2,K))*HN F82=(F(8,K)-F(2,K))*ANYB	K 20 K 21 K 22 K 23 K 24 K 25
	REREL=ANYA-FUDGE CALL SNAFI (M.N) DD 1 K=1.4 F64=F(6.K)-F(4.K) - G82=(G(R,K)-G(2.K))+HN FR2=(F(8.K)-F(2.K))+ANYB WBAR=(H(M.N.K)+W(M+1.N.K))+0.5	K 20 K 21 K 22 K 23 K 24 K 25 K 26
	REBEL=ANYB-FUDGE CALL SNAFI) (M.N) DD 1 K=1,4 F64=F(6,K)-F(4,K) ~ G82=(G(8,K)-G(2,K))*HN FR2=(F(8,K)-F(2,K))*ANYB WBAR=(W(M,N,K)+W(M+1,N,K))*0.5 FX=(F64+F(9,K)-F(7,K))*DTDX8	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27
	REBEL=ANYB-FUDGE CALL SNAFI) (M.N) DD 1 K=1.4 F64=F(6.K)-F(4.K) ~ G82=(G(R.K)-F(2.K))*HN FR2=(F(8.K)-F(2.K))*ANYB WBAR=(W(M.N.K)+W(M+1.N.K))*0.5 FX=(F64+F(9.K)-F(7.K))*DTDX8 FY=(F(8.K)-F(5.K))*YANKEE	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27
	REREL=ANYB-FUDGE CALL SNAFI) (M,N) DD 1 K=1,4 F64=F(6,K)-F(4,K) ~ G82=(G(R,K)-G(2,K))*HN FR2=(F(8,K)-F(2,K))*ANYB WBAR=(W(M,N,K)+W[M+1,N,K))*0.5 FX=(F64+F(9,K)-F(7,K))*DDDX8 FY=[F(8,K)-F(5,K))*YANKEE GY=(G(8,K)-G(5,K))*HN	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27 K 28 K 29
	REREL=ANYB-FUDGE CALL SNAF13 (M.N) DD 1 K=1.4 F64=F(6.K)-F(4.K) - G82=(G(R.K)-G(2.K))*HN F82=(F(8.K)-F(2.K))*ANYB WBAR=(H(M,N.K)+H(M+1.N.K))*0.5 FX=(F64+F(9.K)-F(7.K))*DTDX8 FY=(F(8.K)-F(5.K))*YANKEE GY=(G(8.K)-G(5.K))*HN WNDRTH(K)=HBAR+FX+GY-FY	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27 K 28 K 29 K 30
	REBEL=ANYB-FUDGE CALL SNAFI (M.N) DD 1 K=1.4 F64=F(6.K)-F(4.K) - G82=(G(R,K)-G(2.K))+HN FR2=(F(8.K)-F(2.K))+ANYB WBAR=(H(M.N.K)+H(M+1.N.K))+0.5 FX=(F64+F(9.K)-F(7.K))+DTDX8 FY=(F(8.K)-F(5.K))+YANKEE GY=(G(R.K)-G(5.K))+HN WNRRTH(K)=HBAR+FX+GY-FY WBAR=(H(M.N.K)+HGM-1.N.K))+0.5	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27 K 28 K 29 K 30 K 31
	REBEL=ANYB-FUDGE CALL SNAFI (M,N) DD 1 K=1,4 F64=F(6,K)-F(4,K) ~ G82=(G(R,K)-G(2,K))*HN FR2=(F(B,K)-F(2,K))*ANYB WBAR=(W(M,N,K)+W(M+1,N,K))*0.5 FX=(F64+F(9,K)-F(7,K))*DTDX8 FY=(F(R,K)-F(5,K))*YANKEE GY=(G(B,K)-G(5,K))*HN WNDRTH(K)=HBAR+FX+GY-FY WRAR=(W(M,N,K)+W(M-1,N,K))*0.5 FX=(F64+F(3,K)-F(1,K))*DTDX8	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27 K 28 K 29 K 30 K 31 K 32
	REREL=ANYB-FUDGE CALL SNAF1) (M,N) DD 1 K=1,4 F64=F(6,K)-F(4,K) ~ G82=(G(R,K)-G(2,K))*HN FR2=(F(8,K)-F(2,K))*ANYB HBAR=(W(M,N,K)+W(M+1,N,K))*0.5 FX=(F64+F(9,K)-F(7,K))*DTDX8 FY=(F(R,K)-F(5,K))*YANKEE GY=(G(R,K)-G(5,K))*HN HNRRTH(K)=HBAR*FX+GY-FY WRAR=(W(M,N,K)+W(M-1,N,K))*0.5 FX=(F64+F(3,K)-F(1,K))*DTDX8 FY=(F65+F(3,K)-F(1,K))*DTDX8 FY=(F65+F(3,K)-F(2,K))*REREL	K 20 K 21 K 22 K 23 K 24 K 25 K 26 K 27 K 28 K 29 K 30 K 31

		- 10	
	WBAR=(W(M,N+1,K)+W(M,N,K))+0.5	K	36
	FX=(F(6,K)-F(5,K))+OTDX2	K	37
	FY=(F(9,K)-F(3,K))+EAST	K	38
	GY=(G(9,K)-G(3,K))+H(N+1)	K	39
	WEAST(K)=HBAR+FX+(GY+GR2-FY-F82)+0,25	K	40
	WBAR=(W(M,N-1,K)+W(M,N,K))+0.5	K	41
	FX=(F(5,K)-F(4,K))*DTDX2	K	42
	FY=(F(7,K)-F(1,K))*WEST	K	43
	GY=(G(7,K)-G(1,K))+H(N-1)	K	44
ι	WWEST(K)=WB4R+FX+(GY+GA2-FY-FA2)*0.25	K	45
	WNORTH(3)=WAORTH(3)+DT4*(P(M,N)+P(M+1,N))	K	46
	WSDUTH(3)=WSDDTH(3)+DT4+(P(M,N)+P(M-1,N))	K	47
	WEAST(3)=WEAST(3)+DT4+(P(M,N)+P(M,N+1))	K	48
	WWEST(3)=WWEST(3)+DT4*(P(M.N)+P(M.N-1))	K	49
	CALL EVAL (NNORTH, 2. (FUZZ (M, N)+FUZZ (M+1, N))+0.5)	K	50
	CALL EVAL (HSOUTH, 1. (FUZZ (M.N)+FUZZ (M-1.N))+0.5)	K	51
	CALL EVAL (WEAST.4.(FUZZ(M.N)+FIJZZ(M.N+1))+0.5)	K	52
	CALL EVAL (WHEST.3.(FUZZ(M.N)+FI)ZZ(M.N-1))+0.5)	K	53
	DO 2 K=1.4	Ŕ	54
	FX=(F(4,K)-F(3,K))+DTDX	ĸ	55
	FY=(F(2,K)-F(1,K))*ANYB	K	56
	$GY = (G(2 \cdot K) - G(1 \cdot K)) *HN$	K	57
2	W(H-1.N-1.K)=W(M.N.K)+FX+2.O*(GY-FY)	ĸ	58
-	W1(4-1,N-1,3)=W(M-1,N-1,3)+P(M,N)*DT	K	59
3	CONTINUE	- Ř	60
4	CONTINUE	ĸ	61
·	CALL WEIRDO	K	62
	RETURN	ĸ	63
	END	Ķ·	64-
	SUBROUTINE DEMON	î	1
	IMPLICIT REAL+81A-H,0-Z)	- }-	
	COMMON /APE/ D(10), ARONUM, WEEKDY, KDATE(3)	ĭ	3
	REAL*8 THTFS(7)	-:	4.
	* /' TUESDAY'. WEDNSDY'. THURSDY'. FRIDAY	-	5
	+ , SATURDY , SUNDAY . MONDAY .	٠,٠	- 6
	INTEGER MONTH(13)/ ' JAN', ' FER', ' MAR', ' APR', ' MAY', ' JUN'	-	7
	4, JULY, AUGY, SEPY, OCT, NOV, DECY		- 6
	INTEGER JERK(12)/31,28,31,30,31,30,31,30,31,30,31/	- 1	9
		٠,	10
	CALL GETWHO (ARONUM.KYEAR)		11
	KOAY=MOD(KYEAR,1000)	-	12
	KYEAR=KYEAR/1000	-	
		ᆠ	13
	IF(MOD(KYEAR,4) .EO. 0) JERK(2)=29		14
	L = KYEAR - 69	Ļ	15
	J = L/4 + L + KDAY	Ļ	16
	L = MOD(J,7) + 1	<u>\</u>	17
	WEEKDY=TWTFS(L)	ŗ	18
	K=KDAY	<u> </u>	19
	DO 1 J=1,12		20
	MeJ .	L.	21
	IF (K.CE.JERKIJ)) GO TO 2	r.	22
1	K=K-JERK(J)	L	23
	K=0	L	24
	M=13	L	25
7	MUNTH=MUNTH(M)	ι	26
	KDATE(1)=MUNTH	L	27

	KDATE(2)=LULU+256+((K/10)+256+MDD(K-10))	-	28
	KDATE(3) = LUSH + 256+(KYEAR/10) + MDD(KYEAR,10)	Ļ	_29
	RETURN	L	30
	END	L	31
•	SUBROUTINE DOODLE	Ä	1 2
	CDMMON /EROS/ W(21,60,4),P(21,60) COMMON /NEKD/ MF,NF,NT,MUFF,LTMIT	-	3
		M	4
	COMMON /STUPID/ F(21,60)	M	· · · ·
		Ä	6
	DATA_ZERO/0.0/,ONE/1.0/.8IGGY/0.01/.SMALL/-0.01/.HUGE/1.0E+23/		- 5
	XMASNT=XMASS(NT)	-	
	DO 2 J=2,NF	M.	- 8
	JAY=J .		
	IF (JAY.EO.NT) GO TO 2.	M	-10
	XMASJ=XMASS(JAY)	M	11
	ERR=XMASNT-XMASJ	M	12
	REL=ERR/XMASNT	K	13
	00 1 K=1,4F	M	14
	KAY=K	М.	15
	FACTER=RIDDLE(KAY, JAY)	M	16
	IF (FACTER.EQ.ZERO) FACTER=HUGE	M	17
	PAR=REL/FACTER	M	18
	EPAR=PAR	M	19
	IF (EPAR.GT.BIGGY) EPAR=RIGGY	M	20
	IF (SMALL.GT.EPAR) EPAR=SMALL	M	21
	GEEPAR+ONE	M	22 _
	RH()=W(K,J,1)	M	23
	W(K+J+1)=RHO+G	M	24
	CONTINUE	M	25
	CONT INUE	M	26
	CALL ROGUE	M	27
	DO 4 K=1.MF	M	26
	DO 3 J=2,NF	M	
	FUZ Z=F(K,J)	M	30
	RHO=W(K,J,1)	" M	"31 ["]
	RMAX=0.995*RHOMAX(FUZZ)	H	32
	RHO=DUMDUM(RHO,RMAX)	H	33
	CALL FONKY (FUZZ,RHO,PSTAT,VEL,EASY,T)	M	34
	TANG=W(K,J,3)/W(K,J,2)	M.	35
	COSN=TINE/SORTF (ONE+TANG++2)	M	36
	₩(K,J,1)=RHO*R(K,J)	M	37
	W(K,J,2)=W(K,J,1)*VEL*COSN	M	38
	W(K,J,3)=W(K,J,2)*TANG	M	39
	W(K.J.4)=EASY*R(K.J)	M	40
	P(K,J)=PSTAT	M	41
	CONTINUE	H:	42
	RETURN	- M	43
	END	Ä	44-
	SUBROUTINE DOWN	N	1
	COMMON /EROS/ W(21,60,4),P(21,60)	N	2
	COMMON 'NERO' MF,NF,NT, MUFF,LIMIT	- Ñ	- 3
	DO 1 K=1.MF		4
	W(K.NF.1)=W(K.NF-1.1)+0.5*(W(K.NF.1)-W(K.NF-2.1))	N	5 -
			-
	W(K,NF,2)=W(K,NF-1,2)+0.5+(W(K,NF,2)-W(K,NF-2,2)) RETURN	N N	6
			, 0_
	END	N	8-

```
SUBROUTINE ENDJOB
       CALL HEADS
       CALL HEADS
                                                                                     0
      CALL HEADLA
                                                                                     0
      WRITE (6.1)
WRITE (8.2)
                                                                                     0
                                                                                     n
                                                                                         6
      WRITE (14,3)
WRITE (14,4)
                                                                                     ū
                                                                                     O
                                                                                         8
       WRITE (14.4)
                                                                                     0
       CALL ENDPLT
                                                                                     0
                                                                                        10
       RETURN
                                                                                     0
                                                                                        11
                                                                                     0
C
                                                                                        12
       FORMAT
               ('2',40('*'). END OF DATA SET 6 ',40('*') )
ፕ
       FORMAT ('2',40('+'), END OF DATA SET # ',40('+') }
2
                                                                                     0
                                                                                        14
3
      FORMAT
               ('2',40('+'),' END OF DATA SET 14 ',40('+') }
                                                                                     0
                                                                                        15
       FORMAT
                                                                                     O
                                                                                        16
                     * -- *
      1130X* *****
                            **
                                       ****
                                               ****
                                                                *****
                                                                                     0
                                                                                        17
                                                                            . .
       30X * /*
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                                                                                     n
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                     * * *
       30x * ***
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        30X · *
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      5 30X *****
                                                                                     Ŋ
                                                                                        21
       ENO
                                                                                     0
                                                                                        22-
       SUBROUTINE FRIGHA
                                                                                         .1
      COMMON /EROS/ W121,60,4),P(21,60)
COMMON /COUNT/ L,LL
                                                                                     P
                                                                                     p
       COMMON /NERD/ MF.NF.NT
       COMMON /NITHIT/ CLOWN-VULGAR
                                                                                     P
                                                                                         5
       CALL HEADS
                                                                                     ٥
      WRITE (6.6) L'
                                                                                     P
                                                                                         8
       WRITE (6.5)
       CALL COVO (CDT. VOT. PUNTZ.NT)
                                                                                         10
       TF (L.NE.O) GD TO 1
                                                                                         11
       CLOWN=CDT
                                                                                        12
       VULGAR=VOT
                                                                                        13
       00 2 K=1,NF
ı
                                                                                        14
       CALL COVD (A,B,PUNTZ,K)
                                                                                        15
       AX=A/CDT
                                                                                     ρ
       AXX=A/CLOWN
                                                                                     P
       BX=B/VDT
                                                                                     P
                                                                                        18
                                                                                     P
       BXX=B/VULGAR
                                                                                        19
       SUN=PUNTZ+B
                                                                                        20
       THRUST=SUM+3.141593
                                                                                        21
                                                                                     p
       WF=A+3.141593+32.174
                                                                                        22
       WRITE (6,4) WF, AX, AXX, B, BX, BXX, PUNTZ, THRUST, K
                                                                                     D
                                                                                        23
         (K.EO.NT) WRITE (6.7)
       1F
       CONTINUE
                                                                                        25
                                                                                        26
       RETURN
               1/20X, 'DISCHARGE (CD), THRUST (VD), AND PRESSURE (PD) COEFFICIE
3
       FORMAT
                                                                                        28
      INTS - / T
                                                                                        29
       FORMAT (10X,1PG14.5,0PF10.5,4X,F10.5,4X,1P5G14.5,1X,12)
FORMAT (/16X,'WF',11X,'WF/WF*',6X,'WF/WF1',9X,'VD',11X,'VD/VD*',7
                                                                                        30
5
                                                                                     P
                                                                                        31
      1x. 'VD/VD-1'.9x. 'PD'.11x'THRUST(LBF)'/>
       FORMAT (720X, TERATION NO.=1,15/)
                                                                                        33
                                                                                        34
```

	END	P 35-
	SUBROUTINE EQUATE (K, J, NERD)	0 1
	DIMENSION K(1), J(1)	0 2
		0 3
	N=NERD	0 4
	K(L)=J(L)	0 5
	RETURN	
	RETURN	0 6
	END	0 7-
	SUBROUTINE EVAL (A.ISW.ATE)	R 1
	COMMON /FANG/ F(9,4),G(9,4)	R 2
	D(MENSION A(4)	R . 3
	ZERO=0.0	R 4
	ETA=ATE	R 5
	1F (A(1) .NE.ZERO) GO TO 1	R 6
	72=ZERO	R 7
	23=ZERO	R 8
	PR=ZERO	R 9
	GO TO 2	R 10
1	CONTINUE	R 11
	Z2=A(2)/A(1) ,	R 12
	Z3=A(3)/A(1)	R 13
	HO=HZERO(ETA)	R 14
	HO=HZERO(ETA) PR=HO*A(1)-A(4)	R .15
2	CONTINUE	R 16
	F1[SH,))=-4(2)	rai Tiliu
	F((SW+2)=-(Z2+A(2)+PR)	R 18
	F((SW.3)=-22#A(3)	R 19
	F(ISW+4)=-(Z2*(A(4)+PR))	R 20
	G((Sw,1)=-A(3)	R 21
	G((SW,2)=F(1SW,3)	R 22
	G(15K+3)=-(23+A(3)+PR)	B 23
	G((SW+4)=-(Z3*(A(4)+PR))	R 24
	RETURN	R 25
		R 26-
	SUBROUT(NE F(ASCO	
	SUBRUITINE FIASCU	5 1
<u> </u>	SOMMON JOUPERA HAIZIDAHRIZID	S 2
	COMMON /FROS/ W(21.60,4).P(1260)	5 3
	COMMON /NERD/ MF.NF.NT.MUFF.NEWKY	5 4
	COMMON /SPOR/ S(60),SQ(60),SQP(60),SI(60),SIP(60),AREA(60)	S 5
	COMMON /SEXX/ NASTIE.IDIOT	5 6
	DIMENSION X(21)	S 7
	IF (NASTIE.EQ.O) RETURN	5 8
	ZERIJ=0.0	5 9
- —	NX=MF	S 10
	DO 3 J=1,NASTIE	5 11
	DO 1 K=2,MUFF	S 12
~ <u>i</u> —	X(K)=W(K,J,3)/W(K,J,2)	S 13
	X(1)=SIP(J)	S 14
	X(MF)=SOP(J)	S 15
	CALL SMOOTH (X+MF+2)	5 16
	DO 2 K=2, MUFF	\$ 17
	TN=X[K]	S 18
	RWR=SQRTF(W(K,J,2)++2+W(K,J,3)++2)	S 19
	TESTA=X(1)	S 20
	TESTR=X(NX)	S 21
	IF ((TN-TESTA)*(TESTA-TESTB).GE.ZERO) TN=TESTA	3 61

	IF ((TM-TESTB)=(TESTB-TESTA).GE, ZERO) TN-TESTB	5 23
	CN=SQRTF(1.0/(TN+2+1.0))	\$ 24
	SNOCN+TN	\$ 25
	MAN 1 61 AMARIA	\$ 26
2	W(K,J,2)=CN+RWR W(K,J,2)=CN+RWR	5 27
3	CONTINUE	S 28
	PVSSY = P(1)	5 29
		\$ 30
,	U() 4 K=1412OU	
•	DD 4 K=1.1260 P(K)=AMIN1(P(K).PV\$\$Y) (F (ID10T.NE.O) CALL SAM	-
		\$ 32
	RETURN	\$ 33
	ENO ·	S 34
	SUBROUTINE FIRST	T 1
	COMMON /ABLE/ AX(21)	T 2
	COMMON /FLIGHT, PTHROT, PANIC	T 3
	COMMON /NERD/ MF.NF.NT .	T 4
	ONE=1.0	T 5
	2E40=0.0	T 6
	XLOW=PTHROT	7
	XHIGEDANIC	T - 8
	TARGET=XMASS(NT)	T 9
		T 10
	X=(XHIG+X(OW)+0.5	T 11
	00 1 K=1.HF	Ť 12
	PRESS=X*AX(K)	1 13
	PALL DUNT? (W. 1. BDEEC)	T 14
<u> </u>	TEST=TARGET-XMASST1	T 15
	1E3:=18KUE1-XMA33[[]	
	1F (TEST-GT-ZERO) GO TO 2	T 16 T 17
	XLON=X	
	GO TO 3	7 18
2	KIII D- X	1 19
3	CONTINUE	T 20
	RETURN	T 21
	END	T _ 22
	SUBROUTINE FONKY TRUZZ, RHO, PSTAT, VEL, EASY, TEMP)	u1
	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAM2(21),RGAS(21),	ป 2
	1PZ(21),TZ(21),HZ(21)	U 3
	COMMON /THERMO/ CPX(3).CVX(3).RAG	U 4
ι	CONTINUE	U 5
	ONE=1.0	U 6
	7 ZERO=0.0	U 7
	F=F()22	บ 8
	O=RHO	U 9
	IF (F.ED.ZERD) GO TO 3	U 10
	TIF (F.EO.ONE) GO TO 5	υ ii
	IF (F*(ONE-F).LE.ZERO) CALL BOMBER ('FONKY'.1)	ŭ 12
	1	U 12
	NEHKY=X	U 14
	DIGIT=NEWKY	U 15
	F2=X-DIGIT	U 16
	F1=ONE-F2	U 17
	J=NEHXY+1	U 18
	- K=J+1	U 19
		U 20
	PD=F1*P2(J)*F2*P2(K) TD=F1*72(J)*F2*T2(K)	U 20

	CPX(L)=F1*CP(L,J)+F2*CP(L,K)	U	23
	CVX(L)=F1*CV(L,J)+F2*CV(L,K)	U	24
2	CONTINUE	Ü	25
	RAG=F1+RGAS(J)+F2+RGAS(K)	Ü	26
	GO TO 7	Ŭ,	27
3	CONTINUE	ŭ	28
	P()=PZ())	ŭ	29
	TO=TZ(1)	ŭ	30
	00 4 L=1,3	ŭ	31
	CPX(L)=CP(L,1)	Ü	32
	CUV11 _C1(1) - \.	Ü	33
4	CONTINUE	<u>U</u>	34_
	RAG=RGAS(1)	IJ	35
	GO TO 7	U	36
5	CONTINUE	U	37
	PN=PZ(21)	U	36
	TO=TZ(21)	U	39
	DO 6 L=1.3	U	40
	CPX(L)=CP(L,21)	U.	41
	CVX(L)=CV(L,21)	U	42
5	CONTINUE	U	43
	RAG=RGAS(21)	U	44
	GO TO 7	U	-45
7	CONTINUE	Ü	46
	CALL CIPORT (PO,TO,D,F,PRES,TRANK,VELOC,E)	Ū	47
	PSTAT=PRES	ŭ	48
	TEMP=TRANK .	ŭ	49
	EASY=E	ŭ	50
	VEL=VELOC	- ŭ	- 51 -
	RETURN	IJ	52
	END	┰	
		V	53-
	SUBROUTINE FREAK (PRES.RHO.UU.VV.HY.HX.PO.TO.DEG.T.XH.VEL.GAM)		. 1_
	COMMON /COUNT/ L,LL	_ v .	2
	COMMON /NERD/ MF.NF.NT	٧.	3 _
	COMMON /STUPID/ FZ(21,60)	V.	4
	COMMON /THERMO/ CPX(3),CVX(3),RAG		5
	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAHZ(21),RGAS(21)	٧	6
	DATA ONE/1.0/	٧	7
	P=PRES	V	8
	R=RHO	٧	9
		٧	10
	V=VV	v	11
	M=MY	Ť	12
	N=NX	v	13
	0=V**2+U**2	Ÿ	14
	X=FZ(4,N)	v	15
	Y=X+20.0+1.0	- v	16
	N=Y	v	-
		V	17
	IF (X*(ONE-X)) 6,4,1	-	18
<u> </u>	X=N	٧	19
-	F2=Y-X	٧	20
	F1=ONE-F2	¥	21
	RAG=F1+RGAS(N)+F2*RGAS(N+1)	٧	22
	DO 2 K=1.3	V	23
	CPX(K)=F1*CP(K,N)+F2*CP(K,N+1)	V	24
2	CVX(K)=F1+CV(K,N)+F2+CV(K,N+1)	V	25

		٧	20
	CONTINUE	_ v	27
	TEMP=P/(R*RAG)	· v	28
	TZ=TSTAG(CPX,TEMP,Q) ''	V	29
	PZ=PSTAG(CPX,TEMP,TZ,P,RAG)	V	30
	TANG=V/U	V	31
_	RAD=ATANF(TANG)	V	32
	DEGREE=RAD+57.29578	v	3
_	SEX=CSUBP(TEMP)	V	34
	HEX=CSUBV(TEMP)	v	35
-	GAMMA=SEX/HEX	v	30
	SONIC=SORTF (GAMMA+RAG+TEMP)	v	3
	VELOC=SONTF(O)	··	31
		v	
	XMACH=VELOC/SONIC		39
	PO=PZ	V	40
		٧	41
	DEG=DEGREE	٧	42
	T=TEMP '		4:
	XM=XMACH	٧.	4.4
	VEL=VELOC	٧	4
	GAH=GAHMA	٧	4
	RETURN	v	4
	RAG=RGAS(N)	· v	4
	00 5 K=1.3	v	4
_	CPX(K)=CP(K,N)	- ċ	50
	CYX(K)=CY(K•N)	v	5
	GO TO 3	. v	5
		v	5:
_	K=M+1000+N	v	- 54
		v	5
	CALL ROMBER ('FREAK-FZ',K)		
	RETURN .	-	5
		_ V	5
	END -	٧	58
	SURROUTINE FRITO	W	
	COMMON /FUBAR/ FI-F2-F3-F4-F5	W	- 3
	READ (5,1) K1,K2,K3,K4,K5	W	
	WRITE (6.2) K1,K2,K3,K4,K5	W	-
	2 ERO=0.0	W	
		. M	(
	F2=K2	W	•
	F3=K3	W	
	F4=K4	W	i
_	F5=K5	- 	Ti
	SUM=F1+F2+F3+F4+F5	W	i
	TIF (SUM.EQ.ZERO) CALL BOMBER ('FRITO',1)	ũ	12
		M	1
_	WRITE (6,3) F1,F2,F3,F4,F5,SUM	. ••	
	F1=F1/SUM	W	14
	F2=F2/SU4	<u> ₩</u>	1!
	F3=F3/SUM	W	_17
	F4=F4/SUM	W	1
	F5=F5/SUM	W	14
	WRITE (6.3) F1,F2,F3,F4,F5	W	19
_	RETURN	W	20
		W	21
_	FORMAT (1615)	W	-22
_	FORMAT (/20X;'INTERPOLATION FACTORS'//20X;515)	W	

3	FORMAT (/20%,1P6G15.6) END	W_	24 25-
	SUBROUTINE FUBARA	x_	1
	COMMON /FUBAR/ F1,F2,F3,F4,F5 "	X	2
	A1#F1	X	3
	AZ=FZ	×	4
	A3=F3	X	-3
	A4=F4	X	6
	A5=F5	X	7
	F1=0=0	ĸ	8
	F2=0.0	- x-	9
	F3=0.0	X	10
	F4=1.0	- x	ΪĬ
	F5=0.0	ĸ	12
	RETURN	â	13
	ENTRY FURARB	Ŷ	14
	FI=Al	Ž-	15
	F2=A2		_
	F3=A3	x -	16
			17
		X	18
	F5=A5	X	19
	RETURN	X	.20
	END	X	21-
	SURROUTINE GRAFF	Υ	1
	CDMMUN /SPUR/ \$(60),\$0(60),\$0P(60),\$((60),\$1P(60),AREA(60)	γ	2
	COMMON /EROS/ W(100),0(100)	Υ	3
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY	Y	4
	COMMON /DELTAS/ OX	Y	5
	COMMON /WALL/ XWALL(100)	Y	6
	DO 1 K=1.NF	Y	7
	W(K)=K	_ Y	B
	XWALL(K)=W(K)	Y	9
	Q(K)=SD(K)	Y	10
l	Q(K+NF)=SI(K)	Ý	ii
	CALL FARGX (W.NF)	į	12
	CALL FARGY (Q.NF+NF)	Ÿ	13
	RETURN	·	14
	END	Ÿ	15-
	SUBROUTINE GRAPH	·	1
	COMMON /APE/ KITLE, LABEL(19), NASTY(7)	ź	2
	COMMON /SKALE/ X2.YZ.SX.SY	Ž	3
		_	_
	COMMON /TYME/ T.FLIT .	<u>_</u> 2	4
	DIMENSION X(1), Y(1)		5
	_ DATA BIG/-0.0/.HT/0.14/.HH/0.10/.M/90.0/.Z/0.0/.DUDE/20.0/.XW1DE/		6
	16.0/.YHIGH/10.0/.KS/1/	Z	7
;		Z	8
;		Z	9
;		2	10
	CALL CLASS (*SEROO142*)	7	11
	CALL CALCHP (0.5.0.5.0.3)	2	12
	81G=-0.0	2	13
	RETURN	ž	14
		ž	15
		-	16
C			

		-
	N=NPTS	7 19
	CALL SCALE (X,XWIDE,N,KS,DUDE)	2 _ 20
	JUNK=N+KS+1	Z 21
	KRUD-JUNK+KS	2 22
	X2=X(JUNK)	Z 23
	\$X=X(KRUD)	2 24
	CALL HEADS	7 25
	WRITE (6.1) XZ,SX,(X(J),J=1.N)	2 26
	RETURN	2 2?
_	RETURN	
-ç		
		Z 29
<u> </u>		Z 30
	ENTRY FARGY (Y, NPTS)	2 31
	N=NPTS	2 32
	CALL SCALE TY, YHIGH, N. KS, DUDE)	Z 33
	JUNK=N*KS+1	Z 34
	KRUDĒJUNK+KS	Z ~ 35
	SY=Y(KRUD)	2 36
	YZ=Y(JUNK)	2 37
	WRITE (6,2) YZ,SY,(J,Y(J),J=1,N)	·Z -38
	RETURN	2 39
C	•	Z 40
ç		Z 41
Č		7 42
<u> </u>	ENTRY NEWPLY	7 43
		-
	CALL SYMBOL (0.25-10.3.HH.NASTY.Z.B)	2 44
	CALL SYMBOL (0.25,10.1,4H,NASTY(31,2,20)	2 45
	CALL AXIS (Z-Z-XX+-1,XWIDE-Z-XZ-SX+DUDE)	2 46
	CALL AXIS (Z,Z,'Y'.+1,YHIGH,W,YZ,SY,DUDE)	Z 47
	CALL SYMBOL (2.0.10.1.HT.LABEL.2,76)	Z 4B
	CALL SYMBOL (BIG,BIG,HT, TITERATION NO.= 1, Z, 14)	Z 49
	CALL NUMBER (BIG.BIG.HT.FLIT.Z1)	Z 50
	CALL SYMBOL (BIG.BIG.HT.'-TIME=',Z,6)	2 51
	xxxT=T*1000.0	Z 52
	CAL! NUMBER (BIG.BIG.HT.XXXT.Z.2)	Z 53
	CALL SYMBOL (BIG.BIG.HT." MILLISEXS".Z.11)	Z 54
	RETURN	7 55
C.	•	Z 56
<u>.</u> c .		2 57
č		Z 58
	ENTRY LIONIX.Y.NPTS.KSYN)	2 59
	K=KSYM	2 60
	N=NPTS	5 61
	JUNK=N*KS+1	2 62
	" X(JUNK)=XZ	2 63
	Y(JUNK)=YZ	Z 64
	KRUD=JUNK+KS	2 65
	X (KRUD) = SX	Z 66
	YTKR(ID)=SY	Z 67
	CALL LINE (X,Y,N,KS,-1,K)	Z 68
	RETURN	2 69
С	•	Z 70
Č		2 71
Č		2 72
-	ENTRY LOUN(X,Y,NPTS)	7 73
	MILIONE MONTH TO STATE THE STATE STA	

	•	
	JUNK=N*KS+Y	Z 75
	KRUD=JUNK+KS	_Z _76
	X(KRUD)=SX . gent	_Z77
	Y(KRUD)=SY	Z 78
	Y(JUNK)=YZ	Z *** 79 ***
	X(JUNK)=XZ	Z 80
	CALL LINE (X,Y,N,KS,O,O)	2 81
	RETURN	Z 82
_C		Z 83
-c-		Z 84
_c		Z 85
	ENTRY NEXTP	Z 86
	CALL CALCHP (Z,Z,Z,Z)	Z 87
	RETURN	Z 88
C		Z . 89
		Z 90
<mark>c</mark>		Z 91 -
•	ENTRY ENDPLT	Z 92
	CALL CLASS (*SEROO142*)	Z 93
	RETURN	Z 94
<u>c</u>		Z 95
č	•	Z 96
<mark>c</mark>		2 97
ĩ	FORMAT ('0',20x,'X-PLOT PARAMETERS X-ZERO =',1PG15.6,5X,'UNITS/!	Z 98
<u> </u>	INCH = 1.6[5.6//(20X.)P6G[5.6/))	2 99
•	FORMAT ('0', 20X, 'Y-PLOT PARAMETERS Y-ZERO =', 1PG15,6,5X, 'UNITS/!	Z 100
2	INCH = 1.615.6//10(10X,5(15,0PF10.4)/))	Z 101
	END	Z 102-
	SUBROUTINE GRONK (FUZZ.PP.RHO.VEL.EASY)	AA 1 1
		AA 2
	1PZ(21), TZ(21)	AA 3
	F=FUZZ	AA 5
	P=PP	<u> </u>
	ONE=1.0	AA 7
	ZERO=0.0	4A 8
	IF (F.EQ.ZERO) GO TO 2	AA 9
	IF (F.EQ.ONE) GO TO 4	AA 10
	IF (F*(ONE-F).LE.ZERO) CALL BOMBER ('GRONK',1)	AA 11
		AA 12 _
	NEWKY=X	AA 13
	DIGIT=NEWKY	AA 14
	F2=X-DIGIT	AA 15
	F1=0NE-F2	AA 16
	J=NEHKY+1	AA 17
	K=J+1	4A 18
	P0=F1*PZij)+F2*PZ(K)	AA 19
	T0=F1*T2{J)+F2*T2(K)	AA 20
	DO 1 L=1,3	AA 21
	CPX(L)=F1*CP(L,J)+F2*CP(L,K)	AA 22
	CvX(L)=F1*CV(L,J)+F2*CV(L,K)	AA 23
1	CONTINUE	AA 24
	RAG=F1*RGAS(J)*F2*RGAS(K)	AA 25
	GO TO 6	44 26
-2	CONTINUE	AA 27
_		
	PO=PZ(1)	AA 28

<u></u>			
	10=12(1)	- AA	29
	DO 3 L=1,3	AA	30
	CPX(L)=CP(L+1)	AA	31
3	CVX(L)=CV(L,1)	AA	32
3	CONTINUE	AA	33
	RAG=RGAS(1)	AA	34 35
4	CONTINUE	AA	36
4	PO=PZ(21)	AA	
		AA	37
- —	T0=TZ(21)	- 44	38
	00 5 L=1,3	AA	39
	CPX(L)=CV(L,21) CVX(L)=CV(L,21)	AA AA	40
•	CONTINUE	AA	42
			_
	RAG=RGAS(21)	AA	43
- ,	GO TO 6	AA	44
6		AA	45
	CALL TROPIC (PO.TO.P.F.OEN.VELOC.E)	AA	46
	RHO-DEN ,	AA	47
	VEL=VELOC	AA.	48
	EASY=E	AA	49
- —-	RETURN	AA	50
	END	AA	51.
	FUNCTION HANKY (A.PANKY, TO, SAGR)	AR	. 1
	DIMENSION A(1)	AR	2
	AZ=A(1)	AB	3
	A1=A(2)	AB	4
	A2=A(3)	- AB	5 6
	X=PANKY TZ=TO	AB	7
	RGAS=SAGR	AA	- 8
	POWER=RGAS/AZ	AR	å
	FUDGE=X**POWER	· AB	10
	BARF=A1/AZ	AB	11
	TRAF=A2+0.5/AZ	- AB	12
	Tet?	AB	13
	DO 1 K=1,5	AB	14
	172=7/72	AB	15
	EPAR=172-T)+(BARF+172+T)+TRAF5		- 16
		AB	17
	XLAX=EXP(EPAR) TRAT=XLAX*FUDGE	- AB	18
	TCOMP=TRAT+TZ	AB	19
	ERROR=TCOMP-T	AB	20
	T=TCDMP	AB	21
-ı-	CONTINUE	A8	22
1	HANKY=T	AB	23
	RETURN	AB	24
	END	AB	25
	SUBRIUTINE HURNY	AC	1
	COMMON /NERO/ M.N.NT.MUFF/STUPID/F(21.60)/SUPER/R(21.60)	AC	2
		···· AC	3
	COMMON /SPOR/ 5(60) TSD(60) TSDP(601, ST(60), STP(601, AREA(60) CALL OREZ (F.1260)		4
	CALL HEAD6	- AC	- 3
	On 2 J=1.N	AC	
		AC	- 6
	F(M,J)=1.0) ROGER=1.0/AREA(J)		8
	KUUCK-I OV/ AKCAI J /	AC	8

_	DO 1 K=2, MUFF	AC	9
1	F(K,J)=(R(K,J)+R(1,J))+(R(K,J)-R(1,J))+ROGER	AC .	10
	WRITE (6,3) J. (F(K,J),K=1,M)	AC	11
2	CONTINUE	AC	12
	RETURN	AC	13
C	LY LYNNA	_	
-		AC.	14
5	FORMAT (10x,15,2x,11F10,4/17x,10F10,4/)	AC	15
•	END	AC	16
	FUNCTION HOTS (CP.TSTAT.TZERO)	AD	1
	DIMENSION CP(1)	AD	2
	A=CP(1)	AD	3
		_	
	B=CP(2)+0.5	AD.	4
	C=CP(31*0.3333333	AD	5
	Y=TSTAT	AD	6
	X=TZERO	AD	7
		AD	ı
	H=(X-Y)*(A+B*(X+Y)+C*(X**2+X*Y+Y**2))		_
	HOTS=H	AD	9
	RETURN	AD	_10
	END	AD	11
	SURROUTINE HUNT	AÈ	1
		AE	2
	COMMON /SPOR/ S160),SD160),SDP160),S1160),S1P160),AREA160).		
	COMMON /NERD/ MF.NF.NT	AE	3
	DO 1 K=1.NF	AE .	4
	\$(K)=\$0(K)~\$((K)	AE	5
	AREA(K)=S(K)+(SO(K)+SI(K))	ĀĒ	-6
•			7
	LITTLE=1	AE	-
	SMALL=AREA(1)	ΑE	8
	DO 2 K=2.NF	AF	9
	IF (SMALL.LE.AREA(K)) GO TO 2	AE	10
	SMALL=AREA(K)	AF	11
	LITTLE=K	4 E	12
2	CONTINUE	AE	13
	AGONY=SORTF(SMALL)	AF.	14
	CALL HEADS	AE	15
		ĀĒ	= -
	HRITE (6,4) LITTLE, SMALL, AGONY		16
	WRITE (6.5)	AE	17
	DD 3 K=1.NF	AE	7.8
	AGDNY=AREA (K)/SMALL	AE	19
	SNAFU=SORTF(AGONY)	AE	20
	WRITE (5.6) K.AREAIK), AGONY, SNAFU	AE	21
3	CONTINUE	AE	22
	NT=LITTLE	AF	23
	RETURN	ĀE	-54
	NE LUNG		
		AE	25
C	·	AE	26
	FORMAT (/20x - MIN X-STA = 1,14,3X - MIN AREA = 1,F9.4.3X, EFFECTIVE	AE	27
	TRADIUS = + F10.4 /)	AE	28
-			
5	FORMAT (/33x - 'AREA' -12x - 'A/A+' -11X - 'R/R+' /)	AE	29
5	FORMAT (20x, 15,3F15.4)	AE	30
	END	AE	31
	FUNCTION HZERO (ETA)	AF	ĩ
			-
	_ COMMON_/STAG/ A(8.21),CP(3,21),GV(3,21),WTM(21),GAMZ(21),RGAS(21),		2
	1PZ(21),TZ(21),HZ(21)	AF	3
	ONE=1.0	AF	4
		AF	
	ZERO=0.0		2
	HZERO=HZ(21)	AF	6

X=ETA 15 (X.EQ.ONE) RETURN	AF AF	7
IF IX.LT.ZERO) CALL BONNER ("HZERO",1)	AF	و
IF IX.GT.ONE) CALL BOMBER ('HZERO'.2)	AP	10
x=x+20.0	AF	· ii
N=X	ĀF	12
R=N	AF	13
R=X-R	AF	14
F2=R	AF	15
E1=0ME_E2	ĀF	16
HOHO=HZ N+1)*F1+HZ(N+2)*F2	AF	17
HZERD=HOHO	AF	18
WEYURN	AF	19
ENO	AF	_ 20
SURROUTINE ICHI	AG	_ 1
COMMON /COUNT/ L.LL	AG	Z
COMMON /NERD/ MF.NF.NT	AG	3
COMMON /P\$1A/ PS1A(16).NPS1A	AG	4
COMMON /TYME/ T.FLIT	ΔG	- 5
ZERO=0.0	AG.	
MPS I A = 0	AG	٠,
READ (5.3) PSIA	4 G	8
00 1 K=1.16	AG	9
IF IPSIAIK)-LE-ZERO) GO TO 1	AG	-10
NPSTA=NPSTA+T	AG	'n
PSIAINPSIA)=PSIAIK)	AG	12
CONTINUE 1		13
IF (NPSIA.NE.O) WRITE (6.4) NPSIA, IK, PSIA(K), K=1.NPSIA)	AG	14
T=0	AG	i:
LL=0	AG	16
T=0.0	AG	1
	AG	18
FUITEL		
CALL FRITO	AG	19
CALL NAVSEA	AG	20
CHEC CONT.	AG	21
CALL STAGG	AG	22
CALL STATIC	AG	2:
CALL HORNY	AG	24
CALL BEDLAM	AG	2 !
CALL FIRST	AG	26
DO 2 K=2.NF	- AG	27
IF (K.NE.MT) CALL PHINOU IK)	AG	28
CONTINUE	AG	- 24
CALL TRICKY	AG	30
CALL OUTPUT	AG	31
RETURN	AG	32
	AG	33
FORMAT 18E10.0)	AG	34
	AG	- 3:
FURMAT (/20X, NO. PSTA LINES = 1,13/(1P8G15.6))		
END	AG	36
SUBROUTINE ISOBAR	AH	
COMMON /EROS/ W(21,60,4),P[21,60)	AH	3
COMMON THERDY ME, NE, NE, NUFF, LIMIT, NASTY	AH	3
COMMON /SPOR/ S(60).SD(60).SD(60).S1(60).SIP1601.AREA(60)	AH	4
COMMON /PSIA/ PSIA(16).NPSIA	HA	-:
COMMON /SUPER/ R121.60)	AH	- (

	COMMON /WALL/ XWALL(100)	AH AH	7
	DIMENSION X(100), Y(100) IF (NPSIA.EO.O) RETURN	AH-	
	IF [INPSIA.LE.O).OR. (NPSIA.GT.16)) CALL BOMBER [SOBAR ++ 1.1]	AH	10
	ZERO=0.0	ÄH	ii -
	ONE=1.0	AH	12
	MAX=95	AH	13
	CALL HEADS	AH	14
	WRITE (8.7)	HA	15
	CALL NEWPLT	AH	lo'
	CALL LOON (XWALL,SO,NF)	- AH	17-
	CALL LOON (XWALL,SI,NF)	AH	18
	DO 6 JERK=1.NPSIA	AH	19
	KOUNT=0	ĀH	20
	JAZZ=JERK	AH	21
	TARGET=PS (A(JERK)	AH	22
	TARGET=TARGET+144.0	ΔH	23
	DO 2 K=1.MF	AH	24
	DO 1 J=2.NF	AH	25
	OP=P(K,J)-P(K,J-1)	AH	26
	IF (DP.EQ.ZERO) GO TO 1	HA	27 -
	F=P(K,J)-TARGET	ΔH	28
	F=F/DP	AH	29
	IF ((F.LT.ZERD).DR.(F.GT.DNE)) GO TO 1	AH	30
	FVC1=DNE-F	AH	31
	KOUNT=KOUNT+1	AH	32
	X(KOUNT)=XWAEL(J-1)*F-XWALL(J)*FVCT	AH.	33
	Y(KOUNT)=R(K,J-1)*F+R(K,J)*FVCT	AH	34
	IF (KOUNT.EQ.MAX) GO TO 5	HA	35
1	CONTINUE	AH	36
•	CONTINUE	AH	37
2	DO 4 J=1.NF	AH	38
	XJ=XWALL{J})	AH	39
		100	
	DO 3 K=2+MF	- AH	40 -
	DP=P(K,J)-P(K-1,J)	AH	41
	IF (DP.EO.ZERO) GO TO 3	AH	42
	F=P(K,J)-TARGET	AH	43
	_ F=F/DP	AH	44
	IF ((F.LT.ZERO).OR.(F.GT.ONE)) GO TO 3	AH	45
	KOUNT=KOUNT+1	AH	46
	X(KOUNT)=XJ	AH	47
	Y(KOUNT)=R(K-1,J)+F+R(K,J)+(ONE-F)	AH	48
_	IF (KDUNT.GT.MAX) GO TO 5	AH	49
3	CONTINUE	AH	50
4	CONTINUE	AH	51
5	CONTINUE	AH.	52
	IF (KOUNT.EQ.D) GO TO 6	AH	53
	WRITE 18.8) PSIA(JERK), TARGET	AH	54
	WRITE (8,9) (K,X(K),Y(K),K+1,KOUNT)	AH	55
	CALL LION (X+Y+KOUNT+JAZZ)	AH	56
6	CONT INUE	AH	57
	CALL NEXTP	AH	58
	WRITE (8,10)	AH	59
302	RETURN	AH	60

A	FORMAY (/20X, 'ISOBAR =', F10, 3, '(PS1A)', 5X, F10, 1, 'PSFA'/)	AH	63
)	FORMAT (/20(20x,5(15,F8.3,F7.3)/))	AH	64
0	FORMAT (/20x, RETURN FROM MISOBARM 1/)	AH	65
	END	AH	66-
	FUNCTION LIBARY (SORFT)	AT	1
•	SDRFT=0.0	ĀĪ	2.
	LIBARYED	AI	3
	RETURN	AI	4
	ENTRY COSRF(X)	ΑI	5
	COSRF=COS(X)	ΑĪ	ó
	RETURN	Āİ	7
	ENTRY SINRF(X)	Al	8
	SINRF=SIN(X)	- ÂÎ	- 6
	RETURN	ĀĪ	10
	ENTRY COSF(X)	Āİ	ii
	COSF=COS(X)	AI	12
	RETURN	AI	13
	ENTRY STAF(X)	AI	14
	SINF= SIN(X)	AT	15
	RFTURN	A I	16
	ENTRY TANF(X)	AI	17
	TANF=TAN(X)	AI	18
	RETURN	Al	19
	ENTRY SORTF(X)	AI	20
	SOPTF=0.0	AI	21
	IF (X-LE-0-DD+D) RETURN	AI	22
	SORTF=SORT(X)	AI	23
	RETURN	Äİ	24
-	ENTRY ATANE(X)	ÂÌ	25
		ĀĪ	26
	ATANF=ATAN(X)	- 11-	27
	REY(IRN	-	28
	ENTRY DUHDUM(X,Y)	AI	
	Drindin=A	ΑI	29
	IF (X-LT-Y) DUMDUM=X	AI	30
	RETURN	ΑI	31
	ENTRY TANDF(X)	AI	32
	WDRGH=X/57.29578	AT	33
	TANDF=TAN(WDRGH)	A I	34
	RETURN	A I	35
	END	AI	36-
-	SUBROUTINE LINEAR (TARGET, X, MASTY, F1, F2, J1, J2, NOCON)	AJ	1
	DIMENSION X(1)	AJ	2
	ZERG=0.0	X3-	- 3
	NX=NASTY	AJ	4
_	NUCUN=1	AJ	5
	IF (NX.LT.2) RETURN	A.J	6
	NOCDN=2	LA	ž
		AJ	8
	IF (NX.GT.21) RETURN		- 9
	NUCUN=3	AJ	
	G1=TARGET-X(1)	AJ	10
	G2=X(NX)-TARGET	AJ	11
	SUM=G2+G1	AJ	12
	1F (SUM.LT.ZERO) RETURN	LA	13
	DO 1 K=2.NX	LA	14
	J=K	AJ	15
	G2=TARGET-X(K-1)	AJ	16

	G1=X(K)-TARGET	AJ	17
1	IF ((G1+G2)-GE-ZERO) GD TO 2	. AJ	18
L	CONTINUE NDCON=4 PETIEN	AJ	19
	NDCDN=4	A.J	20
2	AL FUNIT	~ 0	21
<u></u>	NOCON=5 SUM=G1+G2	AJ	22
	TE TELM EN TERM DETING	AJ	24
_	IF ISUM.EO.ZERO) RETURN	LA	25
			26
	F1=G1/SUM	LA	27
		LA	28
	J1=J-1 J2=J	AJ	29
	RETURN	AJ	30
	END	AJ	31
	SUBROUTINE MAINP	AK	1
	2008000 INC HAIRS	AK	2
•	COMMON /DELTAS/ DX.DY.DY.DY2.DT2.DT4	AK	3
	COMMON /COUNTY L.LL	AK	- 3
	COMMON /GEORY/ ME.NT	AK	5
	COMMON /NERD/ MF.NF.NT	AK	6
			7
	KOUNT=0	AK	. 8
	*****	AK	9
	CALL START	AK	10
	CALL SIRVI	AK	11
	SEA 16.41 MINES MEUVIS IDIOT	AK	12
:	CALL GRAPH READ (5,6) NTIMES, NEWKIE, IDIOT		13
<u> </u>	IF (IDIOT.NE.O) GO YO 1	- AK	14
	CALL ICHI	AK	15
	co to 3	AK	16
	CALL RESTOR	AK	17
	CALL RESTOR IF (IDIOT-LT-O) CALL MEYER	AK	18
		AK	19
	IF ((NTIMES+NEWKIE) .EQ.O) GD TO 5	AK	. 50
•		AK	21
	HOTTE 16 7) NYTHEC MENUTE INTOX	- 40	22
,	DO 4 K=1,NTIMES	Y K	23
	DO A K=1.NTIMES	AK	24
	DO 3 J=1+NEHK1E	AK	25
	T=T+DT	AK	26
	T=T+DT L=L+1 FLTT=L	AK	27
	FLITEL	AK	28
	CALL CYCLE	AK	29
	CALL BNDRY	AK	30
	CALL FIRST		31
	CALL DOWN	AK	32
		AK	33
	CALL DODDIE CALL FIASCO	AK	34
			35
-	CALL STREAM CALL TRICKY	- AK	36
		AK	37
_	CALL OUTPUT	AK	38
	CONTINUE	AK	39
	CALL STORE	AK	40
	RETURN	AN	70

		AK	42
_		AK_	-43 -44
	FORMAT (1615)	AK	45
;—	FORMAT (/20x, 'NUMBER OF PERIODS=', 15, 3x, 'ITERATIONS/PERIOD=', 13, 3		46
,		AK	47
	1X, *RESTART = ', 1/) END:	AK	48-
	SUBROUTINE MAXIE (X.NDEX)	AL.	1
	DIMENSION WALLS	AL	;
	DIMENSION X(1)		3
	N=NDEX	AL.	3
	J=1 IC (N C 1) DETUDM	AL	5
	In Tracelly Retord	AL.	
	BJG=X(1)	_	6
	DO 1 K=2,N	AL.	- 7
	IF IBIG.GT.X(K)) GO TO 1	AL	8
	J±K	AL	- 9
	BIG=X(K)	AL,	10
	CONTINUE	AL.	11
	NDEX=J	AL	12
	RETURN	AL	-13
	ENIKY MINALE(X, NUEX)	AL	14
	J=[' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' ' '	AL	15
	N=NUEX	AL	16
	IF (N.LE.1) RETURN	AL	17
	SMALL=X(I)	AC	18
	On 2 K=2,N	AL	19
	IF (SMALL.CT.XIN)) GO TO 2	AL	20
	J=K	AL	21
	SMALL=X{N}	AL	22
	CONTINUE	AL	23
	NDEX=J	AL	24
	RETURN	AL	25
	END .	AL	26-
	SUBROUTING MEYER	AM	. 1
		AM	. 5
	COMMON /NERD/ MF.NF.NT	AM	3
	COMMON /PRNOTL/ PROUND(60).PMAXB.NANKER.NLAST		
	COMMON /STAG/ A(8,21).CP(3,21),CV(3,21),HTM(21),GAMZ[21),RĞAS[21],	AM	5
	1PZ121),TZ(21),HZ(21),RHOZ(21)	AM	6
	DIMENSION X(60)		
		АМ	7
	ONE=1.0	AH	8
	PSTAG = PZ(MF)		
	READ (5,20) NANKER, NLAST, PMAXB		
	T N = NLAST - NANKER + 1		
	REAO (5+21) (X(K)+K=1+B)		
	IF IX(1) :GT: 0.0) GO TO 23		
	X(1) = - X(1)		
	DO 22 K=2,N		
	DO 22 K=2,N		
_	DD 22 K=2,N 22 X(K) = X(K-1) - GD TD 24 23 IF (N alfa 8) GD TD 24		
_	DD 22 K=2,N 22 X(K) = X(K-1) - GD TD 24 23 IF (N alfa 8) GD TD 24		
_	DO 22 K=2;N 22 X(K) = X(K-1) 		· • · ·

		_	
	J = NANKER - 1 + K		
	PROUND(J) = PSTAG/X(K)		
25	FONTINUE		
	IF (NLAST .GE. NF) GO TO 27		
	M = NF - NLAST		
	DO 26 K=1',M		
26	PBOUND(NLAST+K) = PBOUND(NLAST+K-1)		
27	WRITE (6,28) (K,PBDUND(K),K=NANKER,NF)		
	RETURN		
20	FORMAT (215.G10.0)		
	FORMAT (8G10.0)		
٠.	END		
	SUBROUTINE MOND (X.NX)	AN	
			1
	DIMENSION X(1)	AN	2
	N=NX	AN	3
	DO 1 K=2+N	AN	4_
1	X(K)=DUMDUM(X(K-1),X(K))	AN	5
	RETURN	AN	6
	END	AN	7-
	SUBROUTINE NAVSEA	AO	1
C .—		AO	2
	COMMON /FRAN/ AD(60),AI(60),BD(60),BI(60)	40	3
	COMMON /DELTAS/ DX.DY.DY.DY.DY2.DT2.DT4	AO	4
	COMMON /DUPER/ H4(21) +H8(21)	40	5
	CDMMON /EROS/ D(60,4), MAT(20), KODE(4), SDYDX(60)	AO.	- 6
	COMMON /FLEX/ NFLX	AO	7
	COMMON /NDEX/ INDEX(9)	AO	6
	COMMON /NERD/ MF.NT.MUFF.LIMIT.NEWKY	AD	9
_			_
	COMMON /SPUR/ S(60), SD(60), SDP(60), SI(60), SIP(60), AREA(60)	AO	10
	COMMON /SUPER/ R(21,60)	AO	11
	COMMON /SEXX/ NASTIE-IDIOT	AO	12
	DATA ZERO/O.O/.ONE/1.O/.ZUBER/57.29578/	ΑŒ	13
С		AO	14
	CALL OREZ (S.360)	AO	15
	CALL DREZ (D+264)	AΩ	16
	READ (5,18) MF,NF	AO	17
	KEAU 1592UJ DX:DI	AO	18
	WRITE (6,19) MF,NF	AO	19
-c		AO	20
	LIMIT=NF-1	AO	21
	MUFF=MF-1	AO	22
	NEWKY=MUFF-1	AD	23
	DY=MUFF	ÃO	-24
	DY=ONE/DY	AO	25
	DY2=DY+0.5	AO	26
	OTA BTAG	_	_
	072=DT*0.5	AO	27
	DT4=DT2+0.5	AO	28
	WRITE (6,12) DT,0X,DY	AO	29
	READ (5,23) ((DIK,J),J=1,4),K=1,NF)	AO	30
	CALL EQUATE (SO.D.240)	AO	31
C	· ·	AO	32
	ENTRY HOAX	AO	33
	WRITE (6,10)	AD	34
	WRITE (6,13)	AD	35
	WRITE (6,14) (K,SO(K),SOP(K),SI(K),SIP(K),K,K=1,NF)	AD	36
С		40	37
-		- 1 ,	

	BUZZ=MF-1	AO	38
	FUZZ=ONE/BUZZ	AO	39
	DO 2 K = 1 - ME	AO	40
	Fl=MF-K	AO	41
	HA(K)=F1/BUZZ	AO	42
	F2=K-1	AD	43
	M8 (K)=F2/8U22	AU	44
_	DN 1 J=1,NF	AO	45
<u>1</u>	R(K,J)=(F1*SI(J)+F2*SO(J))*FUZZ	AD	46
2	CONTINUE	AO.	47
<u> </u>		AD.	48
	CALL HEAD6	AD	49
	WRITE (6,15)	AO	50
	DO 3 J=1.NF	AD	51
3	WR(TE (6,21) J, (R(K,J),K=1,MF)	AO	52
<u>c</u>		AO	53
	CALL HUNT	AD	54
<u>c</u>		AO	55
	READ (5,18) NASTIE, IDIOT	40	56
	(DIOT=MINOLIDIOT+NT)	AO	57
	IF (NAST(E.LT.O) NAST(E=NT	AO	58
	WRITE (6,16) NT.NASTIE.IDIOT	AO	59
_	CALL HEADS	AD	60
<u>c</u>		A0	61
	WRITE (6,10)	AO	62
	WRITE (6,17)	AO	63
	K=1	AD	64
	DOK=0.0	AD	65
	U(K#U.O	AO	66
	OEGIK=0.0	40	67
	DEGUK 0.0	AO	68
	X=ZERO	AD	69
	WRITE (6,22) K, X, AREA (K), S (K), SU (K), DOK, SOP (K), DEGOK, S (K), D (K, S I P		70
	1(K),DEGIK .	AD	71
C	7010 0 F 10V	AD	72
	EPAR=0.5/OX	AD	73
	EPARDY=EPAR*DY	AO	74
	DO 4 K=2,LIMIT	AD	75
	SOYDX(K)=S(K)+EPAROY	AD	77
	DIK=(S1(K+1)-S1(K-1))+EPAR	DA	78
	DOK=(SO(K+1)-SO(K-1))+EPAR	AD	79
	DEGIK=ZUBER*ATANF(SIP(K)) DEGDK=ZUBER*ATANF(SOP(K))	AD	80
	X= (K-1) *()X	AO	81
	HRITE (6,22) K.X.AREA(K).S(K).SO(K).DOK.SOP(K).DEGOK.SI(K).DIK.SIP		82
	1(K) DEGIK	AO	83
<u></u>	CONTINUE	AD	84
•	K=NF	AD	85
	X=(K-1)+DX	AU	86
	D()K=0 •0	AD	87
	DIK=0.0	AD	88
	DEGIKED - O	AD	89
	DEGOK=0.0	ÃO	90
	WRITE (6,22) K,X,AREA(K),S(K),SO(K),DOK,SOP(K),DEGOK,SI(K),DIK,SIP	AD	91
	1(K) DEGIK	AU	92
c	* to the oto	AD	93

	00 5 K=2+NT	AO	94
	NFLX=K-1 1F (SOP(K)-SOP(K-1)) 5.5.6 CONTINUE	- 20-	- 73
5	CONTINUE	ÃO	97
_	WRITE (6,11) NFLX	AO	98
č	THE COURT HIER	AO	99
•	CALL NAVSTO		100
C	*****		101
	INDEX(1)=1	46	102
	INDEX(2)=4	ĀŪ	103
	INDEX(3)=NT-5	ĀŪ	104
	INDEX(4)=NT-3	-	105
	INDEX(4)=NT-3 INDEX(5)=NT-1		106
	INDEX (6) = NT		107
	INDEX(7)=NT+1		108
	INDEX(8)=NT+3 INDEX(9)=NT+5		109
_		-	110
<u>-</u>	COUNTY AND FE		111
6	COMPUTE ANGLES. DO 7 K=1.NF BO(K)=ATANF(SDP(K))		112
	DO 7 K=1,NP		113
	BO(K)=ATANF(SDP(K))		114
	HI(K)=AIANF(S(P(K))		115
, -	CONTINUE		116
<u> </u>			117
	00 8 K=2,LIM(T	AC	116
	ANIK)=SNYDX(K)=(BN(K+1)=BN(K-1)) A((K)=-SNYDX(K)=(B((K+1)=B)(K-1))	ΑO	119
	A((K)=-SDYDX(K)+(B((K+1)-B](K-1))	AO	120
8	CONTINUE	ΑD	121
		AO	122
	BO(K)=SDYDX(K)*SINRF(80(K)+80(K))	ΑO	123
	BO(K)=SDYDX(K)*SINRF(BO(K)+BO(K)) BI(K)=-SDYDX(K)*SINRF(B((K)+B)(K)) CONTINUE BETURN	OA OA	124
9	CONTINUE	ΑN	125
Ċ			126
_	RETURN		127
C			126
10	FORMAT (/20x, MOZZLE GEOMETRY 4 /)	AO	1 20
iΪ	FORMAT (/20X, INFLECTION POINT NO. = 1.13)	77	150
12	FORMAT (/20x, 'DT =',3PF10.4,'(M(LLISECONDS)',5x,'DX =',0PF9.5,3x,		
· · ·	1'DY = 1.69.5)		132
13	FORMAT (/36X.'SO'.13X.'SOP!.13X.'SI'.13X.'SIP'/)	_	133
14	FORMAT (5(20X-15-2X-4F15-6-5X-(5/))		134
15	FORMAT (/20x+19+2x+9+19+2+19/)		139
16			
10	FORHAT (/20X, THROAT INDEXINT) = 1, 13, 4X, LAST FLOW SMOOTH = 1, 13,		
	14x, LAST PRESSURE SMOOTH STATION =1,13)		137
17	FORMAT [26x, 'X', 8X, 'AREA', 7X, 'S', 8X, 'SO', 6X, 'DSO/DX', 5X, 3HSO', 6X,		
	16HSO (D) -7X - S(' -5X - 'DSI/DX' -4X -3HSI ' -6X -6HSI '(D) /)		139
18	FORMAT (1615)		140
19	FORMAT 1/20x, "NO. PUINTS ON VERTICAL LINEINF)=".13.5x, "NO. OF WAL		
	1L POINTS(NF) =', 13/)		142
20ຼຸ	_ FORMAT (?E12.0)		143
21	FORMAT (10x.15.2x,12f9.4/17x,12f9.4)	AO	144
22	FORMAT (5(10X+(5+5X+11F10+4/))	AO	145
23	FORMAT (4G15.0)	AD	146
	END	AU	147
	SUBROUTINE NAVSTO	AP	
	CONMUN /NEKD/ MF.NF	AP	2

	COMMON /DELTAS/ DX.DY.OT	AP	3
	COMMON /NAVIER/ DTDX,DTDX2,DTDX4,DTDX8,DTDY,DTDY2,DTDY4,DTDY8	AP	_4_
	CDMMON /STDKES/ A(60) ,B(60) ,H(60)	AP	-5-
	COMMON /SPOR/ \$160).\$0(60).\$0P(60).\$1(60).\$1P(60).AREA(60)	AP	6
	CALL OREZ (A.180)	AP	7
	NNE=1.0	AP	8
	DTDX=DT/DX	AP	9
	DTDx2=DTDx+0.5	AP	10,
	DTDX4=DTDX2+0.5	AP	11
	DTDX8=DTDX4+0.5	AP	12
	DIDY=DI/DY	AP	13
	DTDY2=DTDY+0.5	AP	14
	DTDY4=DTDY2*0.5	AP	15
	DTDY8=DTDY4+0.5	AP	16
	00 1 K=1.NF	AP	17
	A(K)=(SOP(K)-S[P(K))/S(K)	AP	18
	B(K)=SIP(K)/S(K)	AP	19
	H(K)=DNE/S(K)	AP	20
•	CONTINUE	AP	21
	CALL HEAD6	AP	
			22
	WRITE (6,3)	AP	23
	WRITE (6,5) (K,A(K),B(K),H(K),K=1,NF)	AP	24
_	DO 2 K=1,180	AP	25
2	A(K)=A(K)+DTDY2	AP	26
	CALL HEADS	AP	27
	WRITE (6,4)	4P	28
	WRITE (6,5) (K,A(K),B(K),H(K),K=1,NF)	AP	29
	RETURN	AP	30
ζ		AP	31
3	FORMAT (29X, *(SDP-SIP)/5*, 8X, *SIP/5*, 10X, *1/5* / }	AP	32
3	FORMAT (29X, (SOP-SIP)/5', 8X, 'SIP/5', 10X, '1/5', 15X, '+0, 5+07/0Y'/)	AP	33
5	FORMAT (20%.15.2%,1P3G15.6)	AP	34
	FND	AP '	35-
	SURROUTINE NORMAL (X.NERD)	AQ	1
	DIMENSION X(1)	ÃO.	<u>2</u> -
	N=NERD .	AO	3
		ÃÖ	4
	DO 1 K=1.N	40	5
 -	SUM=SUM+X(K)	AO	- 6 -
l	IF (SUM.LE.O.O) RETURN	ÃÔ	7
	DO 2 K=1.N	ÃÔ	8 .
•			9
<u>2 </u>	X(K)=X(K)/SUM .	AO	
	RETURN	AQ	10
	END	AO	11-
	SUBADUTINE DREZ (X, NERD)	AR	1
	DIMENSION X(1)	AR	2
	N=NERO	AR	3 "
	DD 1 K=1.N	AR	4
T	X(K)=-0.0	AR	5
	RETURN .	AR	6
	END.	AR	7-
	SUBROUTINE OUTPUT	AS	1
	COMMON 7COUNTY LILL	AS	. 2 -
	COMMON /NERD/ MF.NF.NT	AS	3
	N6=6	Ã5-	
	1120.2	_	
	N8=8 _	AS	5

		AS 6
	DD 2 K=1.NF	AS7
	CALL HEADS	AS 8
	CALL GROG (K)	AS 9
	DO 1 0-110c	AS 10
,	CALL PLINE (J.K.N6)	AS 11
•	CONTINUE	AS 12
	CALL ENIGMA	AS 13
	CALL HEADS	AS 14
	WRITE (8,5) L GALL FROG	AS _ 15
		AS 16
	00 3 K=1.NF	4S 17
	CALL PLINE (1.K.N8)	AS 18
	GALL HEADS WRITE (4,6) L	4S 19
	WRITE (8.6) L	AS 20
_	LACE PRUG	N2 SI
	00 4 N-29W	~~ 62
	CALL PLINE (MF,K,N8)	45 23
	CALL ISORAR	AS 24
	RETURN	AS 25
:		AS 26
i	FORMAT (/20x, AXIS [TERATION NO=+, [5 /)	AS 27
	FORMAT (/20X, WALL TERATION NO=1.15 /)	AS 28
	END	45 29
	SUBROUTINE PARAB(\$X,\$Y,\$)	AT 1
	IMPLICIT REAL+8(A+H,O-Z)	AT 2
	DIMENSTON \$X(1),\$Y(1),\$(1)	AT" 3
	\${1} = -0.0	AT 4
	\$(1) = -0.0 \$(2) = -0.0	AT " 5
	\$(3) = -0.0	· AT 6
	\$(2) = -0.0 \$(3) = -0.0 X1 = \$X(1) X2 = \$x(2)	AT 7
	X2 = \$X(2)	AT 9
	x3 = \$x(3)	AT 9
	F1 = x1 - x2	AT 10
	F2 = X2 - X3	AT 11
		AT 12
	h = 61#62#63	, AT 13
	IF (D .EQ. Q.OD+O) RETURN	AT 14
	D * -1.0/0	AT 15
	Y1 = \$Y(1)	AT 16
	Y2 = \$Y(2)	AT 17
	Y3 = SY(3)	. AT 18
	Y1 = Y1+F2	AT 19
	Y2 = Y2*F3	
	15 - 15-1	AT 21
	\$(1) = D+(Y1+X2+X3 + Y2+X1+X3 + Y3+X1+X2)	AT 22
	\$(2) = -D*(Y1*(X2+X3) + Y2*(X1+X3) + Y3*(X1+X2))	AT 23
	\$(3) = D*(Y1+Y2+Y3)	AT 24
	RETURN	AT 25
	END	AT 26
-	SUBROUTINE PCLASS	AU 1
	COMMON /SPY/ KCLASS.KGROUP	AU 2
	INTEGER+4 JERK(3,3) /	AU 20
	* 'UNCL', 'ASSI', 'FIED'	AU 21
	*, 'CONF', 'IDEN', 'TIAL'	AU 22
	*• 'S','ECRE','T' /	AU 23

	DIMENSION M(3)	AU	3
	CALL EQUATE (M.JERK11.KCLASS+1).3)	AU	4
-	GALL DATE (KDAY-KYR)	ĀŪ	··· •
	RETURN	ĀŪ	Ž.
	ENTRY PCL6	AU	- 5
		AU	Á
	WRITE (6.1) M		- 6
	WRITE (6.2) KDAY, KYR, KGROUP, M	AU	
. —	RETURN	AU	10
	ENTRY PCLB	AU	11
	WRITE (0.1) M	AU	12
	WRITE (8,2) KDAY,KYR,KGROUP,H	AU	13
	RETURN -	ΑU	14
	ENTRY PCL14	AU	15
	WRITE (14.1) M	AU	16
	WRITE (14.2) KDAY, KYR. KGROUP.M	ΑU	17
	RETURN	AU	18
· C	KCIUNN		
		AU	19
1	FORMAT ('2', T58, 18('*')/T58, '*', T75, '*'/T58, '* ', 3A4, T75, '*'/	AU	20
	1758.***,175.***/758.18(***))	AU	21
2	FORMAT(*0*/' DATE=',13,*/',12,T58,181'*')/' GROUP',12,T58,'*', T	AU	. 22
	175.***/* ARO INC.*.T58.** *,384.' **/* ARNOLD AIR FORCE STATION,	AU	23
	2TENN.*, T58.***, T75.***/T58.18(***) /)	AU	24
	END	AU	25-
	SUBROUTINE PHINQU (NXSTA)	AV	
	COMMON /FLIGNR/ WEIGHT.PTHROT.PANIC	ÄV	- 2
			_
	COMMON /NERD/ MF.NF.NT.NUFF.LIMIT	AV	3.
	NX=NXSTA	AV	4
	TARGET=WEIGHT	AV	5
	IF (NX.LT.NT) GO TO 1	AV	6
	IF (NX.GT.NT) GO TO 2	AV	.7
	CALL BUMBER ('PHINQU',1)	AV	. 8
	RETURN	AV	9
- <u>1</u>	CONTINUE	AV	10
_	IF (Nx.LE.O) CALL BOMBER (*PHINQU*.NX)	AV	11
	DIODLE=+1.0376	AV.	12-
	XLOW=PTHROT	AV	13
	XHIG=PANIC	AV	14
			-
	GO TO 3	AV	15.
5	CONTINUE	AV	16
	(F (NX.GT.NF) CALL BOMBER ('PHINQU'.NX)	AV	17
	XLOM=0.0	AV	18
	XHIG=PTHROT	AV	19
	D100LE=-2.06	AV	20
	GO TO 3	AV	21
3	CONTINUE	ĀV	22
2	KOUNT=-20	ĀV	
			23
4	KOUNT=KOUNT+1	AV	24
	IF (KOUNT.EQ.O) GO TO 6	AV	25
	X=(XLUN+XHIG)+0.5	AV	26
	CALL ZETWP (X+NX)	AV	27
	XMAZZ=XMASS(NX)	AV	28
	FONK=TARGET-XMA2Z	AV	29
	TEST=FONK/OIDDLE	AV	30
	1F (TEST.GT.O.O) GO TO 5	AV	31
	XLUW=X	ÂV	-31 -
	GO TO 4	AV	33
	1917 115 -	A 7	23

	XHIG=X	AV	34
	GO TO 4	AV.	35
	ENTRY FINK(POUNDS)	AV	36
	TARGET=POUNDS	AV	37
	NX=1	AV	38
	GO TO 1	AV	39
<u>, </u>	CONTINUE	AV	40
	CALL SETWP (X.NX)	AV	41
. —	RETURN	AV	47
	END	ĀV	43
	SUBROUTINE PLINE (MY.NX.NUNIT)	AW	ī
	COMMON /COUNT/ L.LL	AW	ż
	CHMMON /EROS/ W(21,60,5) .	AW	$-\frac{5}{3}$
	CINMON /SPOR/ \$(60),\$0160),\$0P(60),\$1(60),\$1P(60),AREA(60)	AW	4
	COMMON /STUPID/ F(21.60)	AW	5
	COMMON /SUPER/ R(21.60)	ÂW	6
	M=MY	AW	7
	N=NX	AW	8
	NU=NINIT .	AW	9
	P=N(M.N.5)	AW	10
	W1=W(M,N,1)	AW	11
	W2=H [M , N , 2)	AW	12
-	W3=W(M,N,3)	AW	13
	₩4=W(M,N,4)	AW	14
_	RHO=W1/R(MaN)	AW	15
•	U=W2/W1	AW	16
	V=W3/W1	AW	17
	CALL FREAK (P.RHO.U.V.H.N.PZERO.TZERO.DEGRE.T.XM.VEL.GAM)	AW	18
_	FUZZ=F(H.N)	AW	19
	1F (NU.NE.6) GO TO 1	AW	20
			- 2 1
	MRITE (6,2) M. FUZZ. WI. WZ. WZ. WA. P. T. XM. GAM, RHO, U. V. DEGRE, PZERO, TZER		
	10,VEL	AW	??
	RETURN	AW	23
	CONTINUE	AW	24
	IF (NU, NE. 8) CALL BOMBER ('PLINE'.1)	AW	25
	HRITE (8,2) N.FUZZ.H1.H2.H3.H4.P.T.XH.GAM,RHO.U.Y.DEGRE.PZERO.TZER	AH	26
	10, VEL	AW	27
	RETURN .	AW	28
•	ENTRY GROG(NASTY)	AW	29
	N=NA STY	AW	30
	WRITE (6.3) L.N.SI(N).SD(N).LL	AW	31
	WRITE (6.4)	AW	32
_	RETURN	AW	33
	ENTRY FROG	AW	34
	WRITE (8.4)	AN	35
	RETURN	AW	36
	FROMET AND RE ON ORGER & DAY ADDRESS CALLED ADDRESS CALL	AW	37
	FORMAT (3x,[5,2x,2PF12,2,3x,1P7G15,5/10x,1PRG15,5/)	AW	36
	FORMAT 1/20X, "ITERATION NO.=", 14, 3X, "X-STATION NO.=", 13, 3X, "Y-INN		39
	1ER =',F9.4,3X,'Y-NUTER =',F9.4,5X,'NUTPUT ND. =',15 /)	AW	40
5	FORMAT _ (11x, 'STREAMLINE % ', 8x, 'W1', 14x, 'W2', 12x, 'W3', 14x, 'W4', 10		41
	1x, P-STAT - 10x, TEMP(R) - 7x, MACH NO /15x, CP/CV - 9x, DENSITY - 11	AW	42
•	2x,'U',13x,'V',10x,'FLOH ANG(D)',7x,'P-STAG',10x,'T-STAG',7x,'VELOC	AW	43
	31TY' /)	AW	44
	END	AN	4:
	END	~ ~	

COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WYM(21),GAMZ(21),RGAS(21)		3
1PZ(21),TZ(21)	AX_	
X=P2(1)	AX	4
DO 1 K=2,21	AX_	5_
1F (X.GT.PZ(K)) X=PZ(K)	AX	6
CONTINUE	AX.	
PH=X	AX	8
RETURN	_ AX	9
END	AX	1 n-
FUNCTION PSTAG (CP.TSTAT.TZERO.PSTAT.SAGR)	AY	. 1
DIMENSION CP(3)	AY	2
CPZ=CP(1)	AY	3
CPA=CP(2)	AY	4
CPB=CP(3)	AY	5
T=TSTAT	AY	. 6
TZ=TZERO	AY	7
PERSTAT	- AY	. a
RGAS=SAGR	AY	9
BARF=CPA/CPZ	ÂÝ	10
TRAF=0.5*CPB/CPZ	AY	iĭ
TRAT=TZ/T	AY	12
POWER=CPZ/RGAS	AY	13
EPAR=(TZ-T)*(BARF+(TZ+T)*TRAF)	AY	14
	AY	15
XLAX=EXP(EPAR)		
PRAT=(TRAT+XLAX)++POWER	AY	16
PZERO=PRAT*P	AY	17
PSTAG=PZERO	AY	18
RETURN	AY	19
ENO	AY	20-
SUBROUTINE PUNTZ (NY.NX.PRES)	AZ	1
COMMON /EROS/ W(21,60,4),P(21,60)	AZ	2
COMMON /NERD/ MF,NF,NT,MUFF,LIMIT	AZ	3
COMMON /STUPID/ F(21,60)	AZ	4
COMMON /SUPER/ R(21,60)	AZ	5
COMMON /SPOR/ 5(60),50(60),50P(60),51(60),51P(60),AREA(60)	AZ	- 6
COMMON /DUPER/ HA(21).HB(21)	AZ	7
J#NY	AZ	à
K=NX	·AZ	9
PP=PRES	AZ	10
FU2Z=F(J,K)	AZ	ii
SLOPE=HA(J)*SIP(K)+HB(J)*SOP(K)	AZ	12
COSIN=SQRTF(1.0/(1.0+SLOPE**2))	AZ	13
CALL GRONK (FUZZ, PP. RHO, VEL , EASY)	AZ	14
W1=RHO*R(J.K)	AZ	15
		16
MA=M1 = AEF	AZ	
WZ=WV+COSIN	AZ	17
W3=W2+SLOPE	AZ	18
W4=EASY*R(J,K)	AZ	19
W(J,K,1)=W1	AZ	20
W(J,K,2)=W2	AZ	21
W(J,K,3)=H3	SA	22
₩(J,K,4)=₩4	AZ	23
P(J,K)=PP	AZ	24
RETURN	AZ	25
END	AZ	26-
		-

	COMMON /SUPER/ R(21,60)	BA	3
		BA	
	WE - WE COUR	BA	5
	M=MAMA	BA	6
	N=NERK	BA	7
	FIIZZ=F(N,N)	AA	Ä
	HD=HZERO(FUZZ)	BA	9
	P=(H0+N1-W4)/R(M,N)	BA	10
	PVNT S=P	BA	ii
	RETURN	BA	12
	END ·	BA	13-
	FUNCTION RHOMAX (FUZZ)	BB	1
	COMMON /STAG/ A(8-21),CP(3,21),CV(3,21),WTM(21),GAM2(21),RGAS(21),		2
 ,	1PZ(21),TZ(21),HZ(21),RHOZ(21)	BB	3
	ONE = 1.0	88	4
	ZERO=0.0	BB	5
	F=FUZZ	BB	6
	IF (F.EQ. (NE) GO TO 3	BB	.7
	IF (F.EQ.ZERO) GO TO 2	BB	8
	IF (F*(ONE-F).LE.ZERO) CALL BOMBER (**RHOMAX***,1)	88	ğ
	X=F*20.0	BB	10
	NEWKY= X	88	ii
	DIG(T=NEWKY	BB	12
	F2=X-DIGIT	89	- 13
•	F1=DNF-F2	BB	14
	J=NEWKY+1	BB	15
	K=J+1	BA	16
	RZ=F1*RHOZ (J)*F2*RHOZ(K)	BB	17
	RHOMAX=RZ	BB	18
	-RETURN	BB	19
?	RZ=RHOZ(1)	AB	20
<u> </u>	GO TO 1	BB	21
	RZ=RHOZ(21)	BB	
<u> </u>	GO TO 1	BB.	- 22
	END		23
	• March 1997 1997 1997 1997 1997 1997 1997 199	BB	24.
	FUNCTION RIDDLE (NY, NX)	BC ·	_
	COMMON /STUPID/ F(21,60)	BC	2
	CDMMON /FROS/ W(21,60,4),P(21,60)	BC	3
	COMMON /SUPER/ R(21,60)	BC	2
	COMMON /THERMO/ CPX(3),CVX(3),RAG	BC	5
	ONE=1.0	BC	6
	ZERO=0.0 .	BC	7
	K=NY	BC	8
	J=NX	BC	9
	RIDDLE=ZERO	BC	10
	FUZZ=F(K,J)	BC	11
	RHO=W(K,J,1)/R(K,J)	BC	12
•	CALL FONKY (FUZZ,RHO,PSTAT, VEL, EASY, T)	BC	13
	VV=VEL**2	BC	14
	IF (VV.EO.ZERO) CALL BOMBER ("RIDDLE" , 2)	BC	15
	GAMMA=CSUBP(T)/CSUBV(T)	BC	16
	BETA=GAMMA+RAG+T/VV	BC	17
	XM=SQRTF(ONE/BETA)	BC	1.9
	RID=ONE-RETA	BC	19

	RETURN	BC	21
	END	BC.	22-
	SUBROUT INE ROGUE	BD	i
	COMMON /EROS/ W(21,60,5)	80	2.
	COMMON /NERD/ MF.NF.NT	BO	3
	COMMON /SUPER/ R(21,60)	BD	4
	00 1 J=1.5	BD	•
<u> </u>	CALL EQUATE (W(1,60,J),W(1,1,J),MF)	AD	6
	00 3 K=1.MF	ВD	7
	OO 2 J=1.NF	30	8
2	W(K,J,1)=W(K,J,1)/R(K,J)	80	- 9
3	CONTINUE	BD	10
	00 4 J=1.NF	BD	711
	K=NF+1-J	BD	12
4	K±NF+1-J CALL EDUATE (W(1•K+2•1)•W(1•K•1)•MF) CALL SLICK	80	13
	CALL SLICK	BD	14
	On 5 let 5	BO	15
5	CALL EQUATE (W(1,1,J),W(1,6D,J),MF)	BD	16
	RETURN	BD	17
	END	BD	18-
	SUBROUTINE SAM	BE	1
	COMMON /FROS/ #(21,60,4),P(21,60)	BE	2
	COMMON /NERO/ MF.NF.NT.MUFF	BE	3
	COMMON /STUPID/ F(21,60)	BE	
	COMMON /SUPER/ R(21,60)	BE	- 5
	COMMON /MORK/ X(60)	BE	6_
_	COMMON /SEXX/ NASTIE, IDIOT	BE	7
<u>c</u>	PRESSURE SMOOTHING	BE	8
	IF ((IDIOT-LT.2).OR. (IDIOT-GT.NT)) CALL BOMBER (SAMIDIOT , O	BE	. 9
	00 3 K=2.MUFF	BE	10
	.DO 1 J=1,10101	ВE	11
1	X(J)=P(K,J)	B.F.	12
<u>C</u>		" BE	13
	CALL SMOOTH (X+1010T+4)	BE	14
	MORDN=ID1DT-1	RE	15
	DO 2 J=2.MORDN .	BE	16
	CALE GRONK (F(K,J),X(J),RHO,VEL,EASY)	BE	17
	RWR=SDRTF(W(K.J.2)**2+W(K.J.3)**2)	BE	18
	CSN=W(K.J.2)/RWR	8 E	19"
	SN=W(K.J.3)/RWR	BE	20
	₩(K•J•1)=RHO‡R(K•J)	BE	21
	W(K.J.Z)=W(K.J.1)*VEL*CSN	BE	22
	W(K,J,3)=W(K,J,1)+VEL+SN	BE	23
		BE	24
		BE	25
•	P(K+J)=X(J)		
2	CONTINUE	BE	26
5	CONTINUE	BE	27
	RETIJRN	BE	28
	END	BE	29-
	SUBROUTINE SER142	85	1
	CALL ERRSET (207, 256,-1,1)	BF	2
	CALL ERRSET (208,256,-1,1)	BF	3
	CALL ERRSET (209, 256, -1,1)	BF	4
	CALL MAINP	BF	5
	RETURN	BF	6-
			7-

	SUBROUTINE SETWP (PRES,NXSTA)	BG	1
	ENTRY ZETWP(PRES.NXSTA)	BG	2
	COMMON /NERD/ MF	BG	3
.1	NX=NXSTA	BG	4
	PP=PRES	BG	5 -
	DO 2 K=1.MF	BG	6
5	CALL PUNTZ (K.NX.PP)	AG	
	RETURN	BG	A
	END	BG	9-
	SURROUTINE SLICK	BH	1
	COMMON /EROS/ W(21.60.4)	BH	2
	COMMON /NERD/ MF.NF.NT.MUFF.NEWKY	BH	3
	DO S 7=5 VEMKA	ВН	
	00 1 K=2,MUFF	ВН	5
	L=J+2	BH	6 -
	RII=x(K+1,L,1)	BH	7
- - -	KD=H(K-1,L,1)	BH	R
		RH	9
	Rt=W(K,t-1,1)	BH	10
	R=W(K ₂ L ₂ 1)	-	
	RR=W(K,L+1,1)	ВН	11
1	W(K,J,1)=RANDIT(RU,RD,RL,R,RR)	BH	12
2 _	CONTINUE	BH	13
	00 3 J=2,NF	ВН	14
55	W(1,J,1)=W(1,J+2,1)	AH	15
3	W[MF,J,1]=WINF,J+2,1)	ВН	16
	DO 4 K=2,MUFF	ВН	17
4	W(K,NF,1)=W(K,NF+2,1)	BH	16
	RETURN	BH	19
	ENI)	BH	20-
	SUBROUTINE SHOOTH (X+NX+NTIMES)	B1	_1_
	DIMENSION X(1), Z(100)	BI	2
	N=NX ·		
—		81	3
	NERO=N-1	BI	4
	LIMIT=NTIMES	8 I	5
		BI	4
	LIMIT=NTIMES	8 I	5
··	LIMIT=NTIMES	81 81	5
· · · · · ·	LIMIT=NTIMES F=0.4125 FNN=0.5-0.5*F	81 81 81	5 6 7
	LIMIT=NTIMES F=0.4125 FNO=0.5-0.5*F DO 2 J=1.LIMIT	BI BI BI	5 6 7
	LIMIT=NTIMES F=0.4125 FNO=0.5-0.5*F NO 2 J=1.LIMIT CALL EDUATE (2.x.N)	BI BI BI BI	5 6 7 8 9
1	LIMIT=NTIMES F=0.H125 FNQ=0.5-0.5*F NO 2 J=1.LIMIT CALL EQUATE (Z.x.N) NO 1 K=2.NERD	BI BI BI BI BI	5 6 7 8 9
	LIMIT=NTIMES F=0.H125 FNO=0.5=0.5=F DO 2 J=1.LIMIT CALL EQUATE (2.x.n) NO 1 K=2.NERD X(<)=F+Z(K)+F0O+(Z(K+1)+Z(K-1))	18 81 81 81 81 81 81	5 6 7 8 9 10 11 12
	LIMIT=NTIMES F=0.H125 FNO=0.5=0.5*F DO 2 J=1.LIMIY CALL EQUATE (2.x.N) DO 1 K=2.NERD X(X)=F*2(K)+FOO*(Z(K+1)+Z(K-1)) CONTINUE	BI BI BI BI BI BI	5 6 7 8 9 10
	LIMIT=NTIMES F=0.H125 FNO=0.S=0.S=F DN 2 J=1.LIMIT CALL EQUATE (2.x.n) NO 1 K=2.NERD X(<)=F*2(K)+FOO*(Z(K+1)+Z(K-1)) CINTINUE RETINN END END	BI BI BI BI BI BI BI	5 6 7 8 9 10 11 12 13
	LIMIT=NTIMES F=0,H125 FOQ=0,5=0,5=F DO 2 J=1,LIMIT CALL EQUATE (Z,X,N) DO 1 K=2,NERD X(<)=F*Z(K)+FOQ*(Z(K+1)+Z(K-1)) CONTINUE RETURN END SUBROUTINE SNAFU (MM,NN)	81 81 81 81 81 81 81 81	5 6 7 8 9 10 11 12 13
	LIMIT=NTIMES F=0.H125 FOQ=0.5=0.5=F DO 2 J=1.LIMIT CALL EQUATE (2.x.n) DO 1 K=2.NERD X(<)=F+Z(K)+FOQ*(Z(K+1)+Z(K-1)) CONTINUE RETIORN END SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ W(21.60.4)	BI BI BI BI BI BI BJ BJ	5 6 7 8 9 10 11 12 13 14- 1
	LIMIT=NTIMES F=0.H125 FOQ=0.5=0.5*F DO 2 J=1+LIMIY CALL EQUATE (2,x,N) OO 1 K=2.NERD X(\)=F*2(K)+FOO*(Z(K+1)+Z(K-1)) COUNTINUE RETIJRN END SUBROUITINE SNAFU (MM.NN) COMMON /FROS/ W(21.60.4) COMMON /STUPID/ F(21.60)	BI BI BI BI BI BI BJ BJ	5 6 7 8 9 10 11 12 13
	LIMIT=NTIMES F=0.H125 FOQ=0.5-O.5*F DO 2 J=1.LIMIT CALL EQUATE (2.x.n) DO 1 K=2.NERD X(<>=F*2(K)+FOO*(Z(K+1)+Z(K-1)) CINTINUE RETIJEN EN() SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ W(21.60.4) COMMON /STUPID/ F(21.60) DIMENSION A(4)	BI BI BI BI BI BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3
	LIMIT=NTIMES F=0.H125 FOQ=0.5-0.5*F DO 2 J=1.LIMIT CALL EQUATE (2.x.N) DO 1 K=2.NERD X(4)=F*Z(K)+FOQ*(Z(K+1)+Z(K-1)) CONTINUE RETURN EN() SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ N(21.60.4) DIMENSION A(4) M=MM	BI GI GI GI GI GI GI GI GI GI GI GI GI GI	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5
	LIMIT=NTIMES F=0,H125 FOQ=0,5-0,5+F DO 2 J=1+LIMIY CALL EQUATE (2,X,N) DO 1 K=2,NERD X(<)=F+Z(K)+FOO+(Z(K+1)+Z(K-1)) CONTINUE RETURN EN() SUBROUTINE SNAFU (MM,NN) COMMON /FROS/ W(21,60,4) COMMON /STUPID/ F(21,60) DIMENSION A(4) M=MM N=NN	BI BI BI BI BI BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3
	LIMIT=NTIMES F=0.H125 FOQ=0.5=0.5=F DO 2 J=LIMIT CALL EQUATE (Z.x.n) DO 1 K=2.NERD X(<)=F+Z(K)+FOQ*(Z(K+1)+Z(K-1)) CONTINUE RETURN ENU SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ W(21.60.4) COMMON /STUPID/ F(21.60) DIMENSION A(4) M=MM N=NN KOUNT=0	BI BI BI BI BI BJ BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5
	LIMIT=NTIMES F=0.H125 FNO=0.5-0.5=F DO 2 J=1.LIMIT CALL EQUATE (2.x.n) DO 1 K=2.NERD X(<)=F=2(K)+FOO=(Z(K+1)+Z(K-1)) CINITINUE RETIJEN EN() SUBRRUITINE SNAFU (MM.NN) COMMON /FROS/ W(21.60.4) COMMON /STUPID/ F(21.60) DIMENSION A(4) M=MM N=NN KOUNT=0 DO 2 KRUD=1.3	BI BI BI BI BI BI BJ BJ BJ BJ BJ BJ BJ BJ BJ BJ BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5
	LIMIT=NTIMES F=0.H125 FOQ=0.S=0.S=F DO 2 J=1+LIMIT CALL EQUATE (2.x.n) DO 1 K=2.NERD X(<)=F=2(K)+FOQ=(Z(K+1)+Z(K-1)) CINTINUE RETINEN EN() SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ W(21.60.4) COMMON /STUPID/ F(21.60) DIMENSION A(4) M=MM N=NN KOUNT=0 DO 2 KRUD=1.3 K=M+KRUD-2	BI BI BI BI BI BJ BJ BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5
	LIMIT=NTIMES F=0.H125 FOO=0.5=0.5=F DO 2 J=1.LIMIT CALL EQUATE (Z.x.N) OD 1 K=2.NERD X(X)=F*Z(K)+FOO*(Z(K+1)+Z(K-1)) CINITINUE RETURN ENI) SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ M(21.60.4) COMMON /FROS/ M(21.60.4) DIMENSION A(4) M=MM N=NN KOUNT=0 DO 2 KRUD=1.3 K=M+KRUD=2 OO 1 JOLLY=1.3	BI BI BI BI BI BJ BJ BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5
	LIMIT=NTIMES F=0,H125 FOQ=0,5=0,5=F DO 2 J=1+LIMIY CALL EQUATE (Z,x,n) DO 1 K=2,NERD X(<)=F+Z(K)+FOQ*(Z(K+1)+Z(K-1)) CONTINUE RETURN EN() SUBROUTINE SNAFU (MM,NN) COMMON /FROS/ W(21,60,4) COMMON /FROS/ W(21,60,4) COMMON /STUPID/ F(21,60) DIMENSION A(4) M=MM N=NN KOUNT=0 DO 2 KRUD=1,3 K=M+KRUD=2 OO 1 JO(LY=1,3 J=N+JOLLY=2	BI BI BI BI BI BJ BJ BJ BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5 6 7 8 9 10 11
	LIMIT=NTIMES F=0.H125 FOO=0.5=0.5=F DO 2 J=1.LIMIT CALL EQUATE (Z.x.N) OD 1 K=2.NERD X(X)=F*Z(K)+FOO*(Z(K+1)+Z(K-1)) CINITINUE RETURN ENI) SUBROUTINE SNAFU (MM.NN) COMMON /FROS/ M(21.60.4) COMMON /FROS/ M(21.60.4) DIMENSION A(4) M=MM N=NN KOUNT=0 DO 2 KRUD=1.3 K=M+KRUD=2 OO 1 JOLLY=1.3	BI BI BI BI BI BJ BJ BJ BJ BJ	5 6 7 8 9 10 11 12 13 14- 1 2 3 4 5

A(3)=H(K,J,4) A(4)=H(K,J,4) FUZZ=F(K,J) ČAĽL EVAĽ (A,KOÚNT,FUŽZ)	BJ	15
FUZZ=F(K,J)		_ •
	BJ	16
CALL SUAT LA MOUNT SUITT	BJ	17
CHLL CYML IMANUMIAFULL/	BJ	18
1 CONTINUE	BJ	19
2 CONTINUE	BJ	20
RETURN	BJ	21
END	BJ	22-
SUBROUTINE STAGG	BK	1
COMMON /STAG/ A(8,21).CP(3,21),CV(3,21),WTM(21),GAM2(21),RGAS(21),		2
1P2(21),T2(21),H2(21),RH02(21)	BK	3
COMMON /CPDATA/ CPSPEC(3,8),SPCHHT(8),NAME(8)	8K	4
COMMON /EROS/ B(8,50),X(50),P(50),T(50),F(50),NSTAG	BK	5
COMMON /LIMITS/ VMIN	BK	- 6
CALL CPEVAL	BK	7
CALL OREZ (A,420)	BK	6
GCJ=32.174*777.648	BK	9.
GR1NCH=1.98726	BK	10
WENCH=GR (NCH+GCJ	BK	·ii
WENCH-OR INCHIOLS		
NS=21 .	BK	12
ONE=1.0	8K	13
CALL HEAD6	BK	.14
WRITE (6,21)	BK	15
READ (5,13) NSTAG	PK	16
WRITE (6-14) NSTAG	BK	17
NX=NSTAG	BK	18
READ (5,15) (X(K),P(K),T(K),(B(J,K),J=1,8),K=1,NSTAG)	BK	Į 19
WRITE (6.9) NAME	BK	20
WRITE (6,16) (K,X(K),P(K),T(K),(B(J,K),J=1,B),K≈1,NSTAG)	BK	21
CALL HEAD6	RK	23
WRITE (6,21)	BK	23
DO 1 K=1.NSTAG	BK	24
P(K)=P(K)*144.0	ЭK	25
1 CALL NORMAL (B(1.K).8)	BK	26
WRITE (6,10) NAME	BK	27
WRITE (6,16) (K,X(K),P(K),T(K),(B(J,K),J=1,87,K=1,NSTAG) -	BK	28
FURGENS-1	BK	29
DD 4 K=1.NS	BK	30
TARGET=K-1	BK	31
TARGET=TARGET/FURD	BK	32
CALL LINEAR (TARGET, X, NX, F1, F2, J1, J2, NOCON)	BK	33
IF (NUCON.NE.O) CALL BOMBER ('STAGG', NOCON)	BK	34
PZ(K)=P(J1)*F1+P(J2)*F2	8K	35
TZ(K)=T(J1)+F1+T(J2)+F2	BK	36
12(K)=1(J1)+F1+1(J2)+F2 F(K)=TARGET	BK	37
··		
SUM=0.0	BK	38
NO 3 J=1,8	BK	39
A(J,K)=H(J,J1)*F1+B(J,J2)*F2	HK	40
DO 2 L=1,3	BK	41
CP(L,K)=CP(L,K)+A(J,K)+CPSPEC(L,J)	BK	42
SUM=SUM+A(J-K)/SPCMWT(J)	BK	43
3 TT " CONTINUE TT TT	BK	44
WTM(K)=NNE/SUM	BK	45
# 1 D f V + 1 N L / 2 N D	BK	46

DO 6 K=1,63	<i>(</i> 1)	DO 5 K=1,NS	BK	48
6 CP (K, 1) = CP (K, 1) = CG.] DO 7 K=1, MS CV(1, K) = CP(1, K) = RGAS(K) CV(1, K) = CP(1, K) = RGAS(K) CV(1, K) = CP(1, K) CV(1, K) = CP(1, K) R(1) = (C) =	5			
DO 7 K=1,MS				
CVI1,K1=CPI1,K1=RCAS(K) CVI3,K1=CPI2,K1 CVI3,K1=CPI3,K1 RK 55 CONTINUE MRITE 16,10) NAME MRITE 16,10) NAME MRITE 16,10) NAME MRITE 16,11) RAME MRITE 16,21) RAME MRITE 16,211 RAME MRITE 16,211 RAME MRITE 16,211 RAME MRITE 16,17) (K,MTM(K),RGAS(K),(CPIJ,K),J=1,3),(CVIJ,K),J=1,3),K=1 RK 60 MRITE 16,17) (K,MTM(K),RGAS(K),(CPIJ,K),J=1,3),(CVIJ,K),J=1,3),K=1 RK 62 J.MS) MRITE 16,18) RK 60 DO 8 K=1,MS HRITE 16,18) RK 60 GCPI1,K1)=TZ(K)+TZ(K)+TZ(K)+TZ(K)+CPI3,K)] RK 61 GCPI1,K1)=TZ(K)+TZ(K)+TZ(K)+TZ(K)+CPI3,K)] RK 61 GAMMA=G/H GAMMA=G/H GAMMA=G/H K14)=SORTF(GAMZ(K)+RGAS(K)+TZ(K)) RK 71 MRITE 16,12) K-GAMMA-G,H-MZ(K)-XIK) RK 72 K21' CALL MAX(E (X,K) RK 74 AMAX=X(K) RK 75 KMAX-K AMAX=X(K) RK 76 CC RETURN RETUR	_6			
CV(2;K)=CP(2;K) CY(3;K)=CP(2;K) CY(3;K)=CP(3;K) CY(3;K)=CP(3;K) CONTINUE MRITE (6,10) MAME MRITE (6,10) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,21) MRITE (6,21) MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,11) MAME MRITE (6,12) MAME MRITE (6,12) MAME MRITE (6,12) MAMA MRI				
CY(13,K)=CP(13,K) RK 55 CONTINUE RR 11E 16,10) MAME RR 11E 16,10) MAME RR 11E 16,10) MAME RR 11E 16,10) MAME RR 11E 16,10) MAME RR 57 RR 11E 16,10) MAME RR 58 RR 58 RR 58 RR 59 RR 60 RR 61 618) RR 61 618) RR 62 RR 63 RR 64 RR 65 RR 66 RR 66 RR 67 RR 68 RR 68 RR 69 RR 79 RR 7				
7 CONTINUE WRITE (6,10) MAME WRITE (6,10) MAME WRITE (6,10) (K,FIK),P2(K),TZ(K),(A(J,K),J=1,8),K=1,MS) RK 58 CALL HEAD6 WRITE (6,21) KK 60 WRITE (6,11) KK 60 WRITE (6,11) KK 60 WRITE (6,11) KK 60 WRITE (6,11) KK 60 BK 61 WRITE (6,11) KK 60 BK 61 DO 8 K=1,NS HZ (K)=TZ(K)*(CP(I,K)+TZ(K)*(CP(I,K),J=1,3),(CV(J,K),J=1,3),K=1 BK 62 HZ (K)=TZ(K)*(CP(I,K)+TZ(K)*(CP(2,K)*0.5*0.3333333*CP(3,K)*TZ(K))) KK 66 G=CP(1,K)+TZ(K)*(CP(I,K)+TZ(K)*CV(3,K)) H=CV(I,K)+TZ(K)*(CP(I,K)+TZ(K)*CV(3,K)) KK 60 GAMMA=G/H GAMMA=G/H GAMZ(K)*GAMMA,GH,HZ(K)*TZ(K)*CV(3,K)) KK 70 X(N)*SORTF(GAMZ(K)*RGAS(K)*TZ(K)) KR 70 X(N)*SORTF(GAMZ(K)*RGAS(K)*TZ(K)) KR 71 CALL MAX(E (X,K) KR 72 CALL MAX(E (X,K) KR 73 K=21 CALL MAX(E (X,K) KR 74 WAX=AMAX=X(K) WAX=AMAX=X(K) C K=21 CALL MINNIE (X,K) KR 76 KR 76 CALL MINNIE (X,K) KR 76 KR 76 CALL MINNIE (X,K) KR 76 KR 76 CALL MINNIE (X,K) KR 76 KR 76 CC RETURN RETURN RET				
MRITE 16,10) MAME MRITE 16,10) (K,FIK),P2(K),TZ(K),(A(J,K),J=1,8),K=1,MS) MRITE 16,21) MRITE (6,21) MRITE (6,21) MRITE (6,11) MRITE (6,12) MRITE (6,1				
MRITE	,			
CALL HEADA WRITE (6,21) WRITE (6,21) WRITE (6,21) WRITE (6,17) (K,WTM(K),RGAS(K),(CPIJ,K),J=1,3),(CV(J,K),J=1,3T,K=1) 8K 61 WRITE (6,18) WRITE (6,18) WRITE (6,18) WRITE (6,18) WRITE (6,18) WRITE (6,18) WRITE (6,18) RK 63 HZ(K)=TZ(K)*(CP[1,X)+TZ(K)*(CP[2,K)*0.5*0.3333333*CP[3,K)*TZ(K))) 8K 66 G=CP(1,K)+TZ(K)*(CP[2,K)*TZ(K)*CP[3,K)) 8K 67 H=CV[1,K)+TZ(K)*(CV[2,K)*TZ(K)*CV[3,K]) 8K 68 GAMMA=G/H GAMMA=G/H WRITE (6,12) K,GAMMA,G,H,HZ(K), X(K) WRITE (6,12) K,GAMMA,G,H,HZ(K),X(K) 8K 73 K=21 CALL MAXE (X,K) 8K 73 K=21 CALL MAXE (X,K) 8K 74 MAX=X(K) 8K 76 MRITE (6,19) KMAX,AMAX,VMAX 9K 78 CR=21 CALL MINNIE (X,K) 8K 78 WRITE (6,19) KMAX,AMAX,VMAX 9K 88 WHIN=X(K) 8K 80 K=10 K=21 CALL MINNIE (X,K) 8K 83 WHIN=X(K) 8K 86 WHIN=X(K) 9K 86 WHITE (6,20) KMIN,AMIN,VMIN 8K 88 WHIN=AMIMO,05 WRITE (6,20) KMIN,AMIN,VMIN 9K 88 FORMAT (/20X,*PSFA*,TX,*T=*,*RIS,XA+1/) 9K 91 FORMAT (/20X,*PSFA*,TX,*T=*,*RIS,XA+1/) 8K 91 FORMAT (/20X,*PSFA*,TX,*T=*,*RIS,XA+1/) 8K 91 FORMAT (/20X,*PSFA*,TX,*T=*,*RIS,XA+1/) 8K 91 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO. INPUT POINTS=*,15/) 8K 95 FORMAT (1615) FORMAT (10X,15,F3,X+F8,*,2X,1P4G15.6) 8K 96 FORMAT (10X,15,F3,				
WRITE [6,21]				_
WRITE (6,11) WRITE (6,17) (K,WTM(K),RGAS(K),(CP(J,K),J=1,3),(CV(J,K),J=1,3),K=1 NRITE (6,18) WRITE (6,18) BK 62 DO 8 K=1,NS HZ(K)=TZ(K)*(CP(1,K)+TZ(K)*(CP(2,K)+0.5+0.3333333*CP(3,K)+TZ(K))) BK 64 BC G=CP(1,K)+TZ(K)*(CP(2,K)+TZ(K)*CP(3,K)) BC GAP(1,K)+TZ(K)*(CP(2,K)+TZ(K)*CP(3,K)) BC GAMMA=G/H H=CV(1,K)+TZ(K)*(CV(2,K)+TZ(K)*CV(3,K)) BC GAMMA=G/H SC GAMMA-G/H X(Y)=SORTF(GAMZ(K)*RGAS(K)*TZ(K)) BC CONTINUE CONTINUE CONTINUE CALL MAX(E (X,K) BK 73 R=21 CALL MAX(E (X,K) BK 76 AMAX=X(K) BK 76 AMAX=X(K) BK 76 AMAX=X(K) BK 76 CALL MINITE (X,K) BK 76 CALL MINITE (X,K) BK 76 BK 76 CALL MINITE (X,K) BK 76 BK 7				
WRITE (6,17) (K,WTM(K),RGAS(K),(CP[J,K],J=1,3),(CV(J,K),J=1,3],K=1 8K 62 1,NS)				
1,NS				
WRITE (6-18)				
DO 8 K=1,NS HZ(K)=TZ(K)*(CP[1,K)+TZ(K)*(CP[2,K)*0.5+0.3333333*CP[3,K]*TZ(K))) BX 66 G=CP[1,K)+TZ(K)*(CP[2,K)+TZ(K)*CP[3,K)) H=CV11,K)+TZ(K)*(CP[2,K)+TZ(K)*CP[3,K)) KX 67 H=CV11,K)+TZ(K)*(CP[2,K)+TZ(K)*CP[3,K)) KX 68 GAMMA=G/H GAMZ(K)=GAMMA X(Y)=SORTF(GAMZ(K)*RGAS(K)*TZ(K)) HRITE (4,12) K,GAMMA,G,H,HZ(K),XIK) K=21 CALL MAX(E (X,K) KA 73 KA 73 KA 74 CALL MAX(E (X,K) KA 74 CALL MAX(E (X,K) KA 75 KA 76 KA 76 KA 77 CALL MAX(E (X,K) KA 77 CALL MAX(E (X,K) KA 77 CALL MAX(E (X,K) KA 78 KA 79 CALL HINNIE (X,K) KA 79 KA 79 CALL HINNIE (X,K) KA 81 CALL HINNIE (X,K) KA 81 CALL HINNIE (X,K) KA 82 AM(N-X(K) VMIN=AMIN+0.05 KA 83 AM(N-X(K) VMIN=AMIN+0.05 KA 84 AM(N-X(K) VMIN=AMIN+0.05 KA 86 CALL MAX(B)				
HZ(K)=TZ(K)=(CP(1,K)=TZ(K)=(CP(2,K)=0.5+0.3333333*CP(3,K)*TZ(K)))				-
G=CP(1,K)+TZ(K)*[CP(2,K)+TZ(K)*CP(3,K)) H=CV/I,K)+TZ(K)*[CV(2,K)+TZ(K)*CV(3,K)) H=CV/I,K)+TZ(K)*[CV(2,K)+TZ(K)*CV(3,K)) GAMMA=G/H GAMZ(K)=GAMMA X(X)=SGAMMA X(X)=SGAMMA X(X)=SGAMMA X(X)=SGAMMA X(X)=SGAMMA X(X)=SGAMMA X(X) BK 72 BC CONTINUE BK 74 CALL MAX(E (X,K) BK 76 AMAX=X(K) BK 76 AMAX=X(K) BK 76 BK 77 VMAX=AMAX=0.05 BK 78 BK 78 C				
H=CV11_K)+TZ(K)+tCV(2,K)+TZ(K)+CV(3,K)				
GAMMA=G/H GAMZ(K)=GAMMA X1(Y)=SORTF(GAMZ(K)*RGAS(K)*TZ(K)) B CONTINUE B CONTINUE R=21 CALL MAX(E (X,K) AMAX=X(K) AMAX=X(K) B WRITE (6,19) KMAX,AMAX,VMAX C K=21 CALL MINNTE (X,K) BK 76 WRITE (6,19) KMAX,AMAX,VMAX C R=1 GALL MINNTE (X,K) BK 78 KMN=K AM(N=X(K) BK 78 BK 78 BK 78 BK 78 BK 78 BK 79 C C R=21 GALL MINNTE (X,K) BK 81 CALL MINNTE (X,K) BK 82 KMN=K AM(N=X(K) VMIN=AMIN*0.05 WRITE (6,20) KMIN,AMIN,VMIN BK 85 AM(N=X(K) BK 86 C RETURN C RETURN C RETURN C RETURN BK 88 9 FORMAY (/16X,*SYREAM FRACT.*,8X,*SYAGNAYION*,19X,*RELAYIVE MASS O BK 90 1F SPECIE'/30X,*PSIA*,7X,*T=R*,8(5X,A4)/) BK 88 9 FORMAY (/20X,*PSIA*,7X,*T=R*,8(5X,A4)/) BK 91 FORMAT (/20X,*MDL MT*,5XL*GAS CON*,17X,*GP COEFFICIENTS*,22X,*CV 9K 93 1COEFFICIENTS*/ BK 94 1COEFFICIENTS*/ FORMAT (10X,15,5X,F8.4,2X,1P4G15.6) BK 95 15 FORMAT (10X,15,5X,F8.4,2X,1P4G15.6) BK 96 16 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BF FORMAT (10X,15,F8.4,F1				
GAMZ(K)=GAMMA				
X(X)=SORTF(GAMZ(K)+RGAS(K)+TZ(K)) RTITE (6,12) K,GAMMA,G,H,HZ(K),XIK) R CONTINUE AK 73 K=21 CALL MAX(E (X,K) AMAX=X BK 76 AMAX=X(K) WAX=AMAX+0.05 WRITE (6,19) KMAX,AMAX,VMAX C K=21 CALL MINNIE (X,K) KM,N=K AM (N=X(K) WHITE (6,20) KMIN,AMIN,VMIN C RETURN RETURN RETURN RETURN RETURN RETURN RETURN RETURN BK 86 9 FORMAT (/16X,*SYREAM FRACT.*,8X,*SYAGNATION*,19X,*RELATIVE MASS 0 8K 90 1F SPECIE*/30X,*PSIA*,7X,*T=R,8(5X,A4)/) BK 89 1COFFFICIENTS*/ FORMAT (/20X,*MOL MT*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV 8K 93 1COFFFICIENTS*/ FORMAT (/20X,*MOL MT*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV 8K 94 1COFFFICIENTS*/ FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) 8K 94 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) 8K 95 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 96 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 97 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 96 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 97 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 96 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 97 FORMAT (10X,15,5X,F8,4,2X,1P4G15.6) BK 97 FORMAT (10X,15,5X,F1,2X,1P4G13.4) BK 97 FORMAT (10X,15,5X,1P4G13.4) BK 100 LCV*,10X,*ENTHAL*,6X,*SPEED OF SOUND*/] BK 102				
## ## ## ## ## ## ## ## ## ## ## ## ##				
### CONTINUE				
R=21	A			
CALL MAX(E (X,K) RMÁX=K AMAX=X(K) VMAX=AMAX*O.05 WRITE (6,19) KMAX,AMAX,VMAX C K=21 CALL MINNIE (X,K) RM RS AM(N=K AM(N=K) WRITE (6,20) KMIN,AMIN,VMIN C RETURN RETURN RETURN RETURN BK 88 75 FORMAY (/16X,*SYREAM FRACT,*,8X,*SYAGNATION*,19X,*RELATIVE MASS O RK 90 1F SPECIE*/30X,*PSFA*,7X,*T=R*,8(5X,A4)/) FORMAT (/30X,*PSFA*,7X,*T=R*,8(5X,A4)/) TO FORMAT (/20X,*MOL MI*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV RK 93 TO FORMAT (/20X,*MOL MI*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV RK 93 TO FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 95 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 96 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 97 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 97 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 97 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 99 17 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 100 1CV*,10X,*ENTHAL*,6X,*SPEED OF SOUND*/)				
RMAX=K				
AMAX=X(K) VMAX=AMAX+0,05 WRITE (6,19) KMAX,AMAX,VMAX C K=21 CALL MINNTE (X,K)				
VMAX=AMAX+0.05 WRITE (6,19) KMAX,AMAX,VMAX K=21 CALL MINNIE (X,K) BK 82 KM1M=X AM(N=X(K) VMIN=AMIN*0.05 WRITE (6,20) KMIN,AMIN,VMIN C RETURN RETURN RETURN RETURN BK 86 9 FORMAY (/16X,*STREAM FRACT.*,8X,*STAGNATION*,19X,*RELATIVE MASS O 8K 90 1F SPECIE*/30X,*PSIA*,7X,*T-R*,8(5X,A4)/) BK 89 10 FORMAT (/20X,*MOL NI*,5X,*GAS CON*,17X,*GP COEFFICIENTS*,22X,*CV 8K 93 10 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO. INPUT POINTS=*,15/) 8K 95 13 FORMAT (/20X,*STAGNATION PARAMETERS*,5X,*NO. INPUT POINTS=*,15/) 8K 95 16 FORMAT (3E12.0,4X,8E5.0) BK 96 17 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 99 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90 10 FORMAT (10X,15,F8,4,F12.3,F10.1,8F9.4) BK 90		• 11 17 3		
## WRITE (6,19) KMAX,AMAX,VMAX C				
C K=21				
K=21 CALL MINNIE (X,K) BK 82 KMN=K BK 83 AM(N=X(K) WMIN=AMIN*0.05 WRITE (6,20) KMIN,AMIN,VMIN BK 86 C RETURN C RETURN C RETURN C FORMAT (/16X,*STREAM FRACT.*,8X,*SYAGNATION*,19X,*RELATIVE MASS O 8K 90 1F SPECIE*/30X,*PSIA*,7X,*T-R*,8(5X,A4) /) BK 89 10 FORMAT (/30X,*PSFA*,7X,*T-R*,8(5X,A4) /) BK 91 11 FORMAT (/20X,*MOL MT*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV 8K 93 1COEFFICIENTS* /) BK 94 12 FORMAT (20X,*MOL MT*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV 8K 93 1COEFFICIENTS* /) BK 95 13 FORMAT (1615) BK 96 14 FORMAT (1615) BK 97 15 FORMAT (10X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) 8K 97 16 FORMAT (10X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) 8K 97 17 FORMAT (10X,*STAGNATION PARAMETERS*,5X,*NO,*INPUT POINTS=*,15/) 8K 97 18 FORMAT (10X,*STAGNATION PARAMETERS*,5X,*NO,*CP*,12X,**BK 101 16 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 101 17 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 101 18 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 101 18 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 101 18 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 101 18 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 101 18 FORMAT (10X,*STAGNATION EVALUATION*,732X,*GAMMA*,10X,*CP*,12X,**BK 10X,**CP*,12X,**BK 10X,**CP*,12X,**BK		William Control of the Control of th		
CALL MINNIE (X,K) KM1M=K AM(N=X(K) VMIN=AMIN*0.05 WRITE (6,20) KMIN,AMIN,VMIN C RETURN C RETURN C FORMAT (/16X,*STREAM FRACT.*,8X,*SYAGNATION*,19X,*RELATIVE MASS O BK 80 1F SPECIE*/30X,*PSIA*,7X,*T-R*,8(5X,A4) /) BK 88 FORMAT (/20X,*MOL MI*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV BK 93 ICOEFFICIENTS* /) FORMAT (20X,*MOL MI*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV BK 93 ICOEFFICIENTS* /) FORMAT (10X,15,5X,F8.4,2X,1P4G15.6) BK 96 FORMAT (120X,*STAGNATION PARAMETERS*,5X,*NO, INPUT POINTS=*,15/) BK 96 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 96 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 96 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 100 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 100 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 100 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 100 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 101 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 100 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 100 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BK 101	•	K=21		
KMIN=K AM(N=X(K) VMIN=AMIN*0.05 BK 84 WHITE (6,20) KMIN,AMIN,VMIN C RETURN BK 88 9 FORMAY (/16X,*STREAM FRACT.*,8X,*STAGNATION*,19X,*RELATIVE MASS O 8K 90 1F SPECIE*/30X,*PSIA*,7X,*T-R*,8(5X,A4)/) BK 91 10 FORMAT (/30X,*PSFA*,7X,*T-R*,8(5X,A4)/) BK 92 11 FORMAT (/20X,*MOL MT*,5X,*GAS CON*,17X,*CP COEFFICIENTS*,22X,*CV 8K 93 ICOEFFICIENTS*/; BK 94 12 FORMAT (20X,*STAGNATION PARAMETERS*,5X,*NO. INPUT POINTS=*,15/) 8K 95 13 FORMAT (1615) BK 96 14 FORMAT (120X,*STAGNATION PARAMETERS*,5X,*NO. INPUT POINTS=*,15/) 8K 95 15 FORMAT (3E12.0,4X,8E5.0) BK 98 16 FORMAT (10X,15,F3,4,F12.3,F10.1,8F9.4) BK 98 17 FORMAT (10X,15,F3,4,F12.3,F10.1,8F9.4) BK 90 18 FORMAT (10X,15,F3,4,F12.3,F10.1,8F9.4) BK 100 1CV*,10X,*ENTHAL*,8X,*SPEED OF SOUND*/) BK 102			-	
AMIN=X(K) VMIN=AMIN*0.05 WRITE (6,20) KMIN,AMIN,VMIN C RETURN BK 88 BK 89 FORMAT (/16X, 'STREAM FRACT.'.8X, 'STAGNATION',19X, 'RELAYIVE MASS 0 8K 90 IF SPECIE'/30X, 'PSIA',7X, 'T-R',8(5X,44)/) FORMAT (/20X, 'MOL MT',5X, 'GAS CON',17X, 'GP COEFFICIENTS',22X, 'CV 8K 93 ICOEFFICIENTS'// FORMAT (20X,15,5X,F8.4,2X,1P4G15.6) BK 94 FORMAT (20X, 'STAGNATION PARAMETERS',5X, 'NO, INPUT POINTS=',15/) 8K 95 FORMAT (3E12.0,4X,8E5.0) BC 98 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 99 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) BC 90 FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,F12.3,F10.1,8F9.4) FORMAT (10X,15,F8.4,				
VMIN=AMIN*0.05 WRITE (6,20) KMIN,AMIN,VMIN RETURN RETURN FORMAT (/16x,*STREAM FRACT.*,8x,*SYAGNATION*,19x,*RELAYIVE MASS O 8K 80 1F SPECIE'/30x,*PSIA*,7x,*T-R*,8(5x,A4)/) FORMAT (/30x,*PSFA*,7x,*T-R*,8(5x,A4)/) FORMAT (/20x,*MGL MT*,5x,*IGAS CON*,17x,*CP COEFFICIENTS*,22x,*CV 8K 93 1COEFFICIENTS*/ FORMAT (20x,15,5x,F8.4,2x,1P4G15.6) RETURN 12 FORMAT (1615) FORMAT (1615) FORMAT (162x,*STAGNATION PARAMETERS*,5x,*NO. INPUT POINTS=*,15/) 8K 95 15 FORMAT (3E12.0,4x,8E5.0) 16 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) 17 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) 18 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) RETURN 8K 86 8K 86 8K 86 8K 89 99 17 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) BK 99 17 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) BK 101 1CV*,10x,*ENTHAL*,8x,*SPEED OF SOUND*/ BK 102				
RETURN				_
RETURN				
RETURN C 9 FORMAY (/16x, 'STREAM FRACT.', 8x, 'STAGNATION', 19x, 'RELATIVE MASS O 8K 89 1F SPECIE'/30x, 'PSIA', 7x, 'T-R', 8(5x, 44) /)	C	ALTE TOYEO, WILLIAM THE TOTAL TO THE TOTAL THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO THE TOTAL TO T		
C	-	RETURN		
9 FORMAT (/16x, *STREAM FRACT, *, 8x, *STAGNATION*, 19x, *RELATIVE MASS O 8K 90 1F SPECIE'/30x, *PSIA', 7x, *T-R*, 8(5x, 44) /) 8K 91 10 FORMAT (/30x, *PSIA', 7x, *T-R*, 8(5x, 44) /) 8K 92 11 FORMAT (/20x, *MOL MT', 5x, *GAS CON', 17x, *CP COEFFICIENTS*, 22x, *CV 8K 93 1COEFFICIENTS* /) 8K 94 12 FORMAT (20x, 15, 5x, F8.4, 2x, 1P4G15.6) 8K 95 13 FORMAT (1615) 8K 95 14 FORMAT (1615) 8K 95 15 FORMAT (/20x, *STAGNATION PARAMETERS*, 5x, *NO. INPUT POINTS=*, 15/) 8K 97 15 FORMAT (3E12.0, 4x, 8E5.0) 8K 98 16 FORMAT (10x, 15, F9.4, F12.3, F10.1, 8F9.4) 8K 99 17 FORMAT (10x, 15, F9.4, F12.3, F10.1, 8F9.4) 8K 99 18 FORMAT (/20x, *STAGNATION EVALUATION* //32x, *GAMMA*, 10x, *CP*, 12x, **8 101 1CV*, 10x, *ENTHAL*, 8x, *SPEED OF SOUND*/} 8K 102	C	NE TONA		
1F SPECIE'/30X, PSIA', 7X, 'T-R', 8(5X, 44) /) 10 FORMAT (/30X, PSFA', 7X, 'T-R', 8(5X, 44) /) 11 FORMAT (/20X, MOL MT', 5X, 'GAS CON', 17X, 'CP COEFFICIENTS', 22X, 'CV	ŏ -	STIRMAT (//AY. ISTREAM EDACT. I.BY. ISTACHATIONI. 19Y. IBELATIVE MASS O		
10 FORMAT (/30x,*PSFA*,7x,*T-R*,8(5x,44)/) FORMAT (/20x,*MOL MT*,5x,*GAS CON*,17x,*CP COEFFICIENTS*,22x,*CV BK 93 1COEFFICIENTS*/) FORMAT (20x,+15,5x,F8.4,2x,1P4G15.6) BK 95 13 FORMAT (1615) FORMAT (1615) BK 96 14 FORMAT (/20x,*STAGNATION PARAMETERS*,5x,*NO. INPUT POINTS=*,15/) BK 97 15 FORMAT (3E12,0,4x,8E5.0) BK 98 16 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) BK 99 17 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) BK 99 18 FORMAT (10x,15,2x,1P8G13.4) BK 100 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101 18 FORMAT (/20x,*STAGNATION EVALUATION*//32x,*GAMMA*,10x,*CP*,12x,* BK 101	•	1F SPECIFICATOR - PSIA - 7X - 1 - R - A 15 X - A 4 3 / 1		_
11 FORMAT (/20X, 'MOL MT', 5X, 'GAS CON', 17X, 'CP COEFFICIENTS', 22X, 'CV	10	FORMAT 1/307 - PSCAL-7Y - T-01 - 8/5Y - A41/1		
1COEFFICIENTS* /)				
12 FORMAT (20x,15,5x,F8.4,2x,1P4G15.6) 13 FORMAT (1615) 14 FORMAT (1/20x,*STAGNATION PARAMETERS*,5x,*NO. INPUT POINTS=*,15/) 8K 97 15 FORMAT (3E12.0,4x,8E5.0) 16 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) 17 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) 18 FORMAT (10x,15,2x,1P8G13.4) 18 FORMAT (1/20x,*STAGNATION EVALUATION* //32x,*GAMMA*,10x,*CP*,12x,* 8K 101 1CV*,10x,*ENTHAL*,8x,*SPEED OF SOUND*/] 8K 102		The state of the s		
13 FORMAT (1615) 14 FORMAT (/20x,*STAGNATION PARAMETERS*,5x,*NO. INPUT POINTS=*,15/) 8K 97 15 FORMAT (3E12.0,4x,8E5.0) 16 FORMAT (10x,15,F8.4,F12.3,F10.1,8F9.4) 17 FORMAT (10x,15,2x,1P8G13.4) 18 FORMAT (/20x,*STAGNATION EVALUATION* //32x,*GAMMA*,10x,*CP*,12x,* 8K 101 1CV*,10x,*ENTHAL*,8x,*SPEED OF SOUND*/) 8K 102	12	** ** ** ** ** ** ** ** ** ** ** ** **		-
14 FORMAT (/20%, STAGNATION PARAMETERS, 5%, NO. INPUT POINTS=, 15/) 8K 97 15 FORMAT (3E12.0, 4%, 8E5.0) 8K 98 16 FORMAT (10x, 15, F8.4, F12.3, F10.1, 8F9.4) 8K 99 17 FORMAT (10x, 15, F8.4, F12.3, F10.1, 8F9.4) 8K 100 18 FORMAT (/20%, STAGNATION EVALUATION, //32%, GAMMA, 10%, CP, 12%, 8K 101 10x, 10x, ENTHAL, 8X, SPEED OF SOUND, 8K 102				
15 FORMAT (3E12.0.4X.8E5.0) 16 FORMAT (10X.15.FB.4.F12.3.F10.1.8F9.4) 17 FORMAT (10X.15.PB.613.4) 18 FORMAT (/20X.*STAGNATION EVALUATION* //32X.*GAMMA*,10X.*CP*,12X.* 9K 101 1CV*,10X.*ENTHAL*,8X.*SPEED OF SOUND*/) 8K 102				
16 FORMAT 10x,15,F8.4,F12.3,F10.1,8F9.4 BK 99 17 FORMAT (10x,15,2x,198G13.4) BK 100 18 FORMAT (/20x,'STAGNATION EVALUATION' //32x,'GAMMA',10x,'CP',12x,' BK 101 1CV',10x,'ENTHAL',8x,'SPEED OF SOUND'/] BK 102		FORMAT (3F12.0.4X.8F5.0)	RK	
17 FORMAT (10x,15,2x,1P8G13.4) 18 FORMAT (/20x,'STAGNATION EVALUATION' //32x, GAMMA', 10x, CP', 12x, 8k 101 1CV', 10x, ENTHAL', 8x, SPEED OF SOUND'/) 8k 102				
18 FORMAT (/20%, *STAGNATION EVALUATION* //32%, *GAMMA*, 10%, *CP*, 12%, * 8K 101 1CV*, 10%, *ENTHAL*, 8%, *SPEED OF SOUND*/) 8K 102		FORMAT (10X-15-2X-1986)3-4)		
1CV*,10%, ENTHAL *,6%, SPEED OF SOUND*/) BK 102				
	<u></u>			
	19	FORMAT (A20X, INDEX OF MAX. STAGNATION SOUND SPEED =1,13,3x, SPEE		

20	10 = '.F9.2, '(FT/SEC)', 5X, 'VMAX = ', F9.2, '(FT/SEC)' / }		104
20	FORMAT (/20x, INDEX OF MIN. STAGNATION SOUND SPEED = 1,13,3x, SPEE ID = 1,F9.2, (FT/SEC) 1,5x, VMIN = 1,F9.2, (FT/SEC) /)	BK	105
	ID =',F9.2,'(FT/SEC)',5X,'VMIN =',F9.2,'(FT/SEC)' /)	BK	106
21	FORMAT (/20X+' GAS PROPERTIES'/)		107
	ENI)		10B
	SURROUTINE START	BL	1
	COMMON /APE/ LINE(30)	BL	2
	DIMENSION LUSH(27) - KARO(20)	RL.	3
	EQUIVALENCE (LINE, LUSH, KARD)	BL	4
	DATA KRUD/'1 **'/.MUNG/'****'/.MUD/'%*<'/	BL	5
ĭ —	READ (5.3 (END=2) KARD	BL	- 5
-	TE THARDALL EO MINICE CO TO 2	BL	6
_	IF (KARD(1).NE.KRUD) GO TO 1	BL.	7
	KARD(1)=MUD	BL	В
	ENTRY HEADS	BL	- 9
	ENTRY HEAD	BL	-
			10
	CALL PCL6	BL	11
	CALL TIME (IDIOT, NSECS)	BL	12
	MINUTE=NSECS/60	BL	13
	NSEC=NSECS-MINUTE+60	BL	14
	KHDUR=MINUTE/60	BL	15
	MINUTE=MINUTE-KHOUR+60	BL	16
	LINE (28) = KHOUR	BL	17
	LINE(29)=MINUTE	BL	18
	LINE(30)=NSEC	BL	19
	WRITE (6.3) LINE	BL	20
_	RETURN	BL	21
	ENTRY HEADR	BL	22
	CALL PCL8	BL	23
	UDITE 10 23 AUGU	BL	24
	WRITE (8,3) LUSH RETURN	BL	25
		BL	26
	ENTRY HEAD14 CALL PCL14 WRITE (14-3) LUSH RETURN	BL	
	CALL PCL14		~ 27
	WRITE (14,3) LUSH	BL	2 B
	11 - 17 - 17	BL	29
2	CALL ENDJOB	BL	30
	RETURN	BL	31
C		BL	32
3	FORMAT (27A4,14,11,12,1,12)	BL	33
	END	BL	34
	SUBROUTINE STATIC	BM	1
	COMMON /ABLE/ AX(21)	BM	2
-	COMMON /EROS/ B(8,50),X(50),P(50),T(50),F(50),NSTAT	BM	- 3
	COMMON /NERD/ MF.NF.NT	BM	4
	FURD=MF-1	BM	9
	CALL HEADS	BM	6
	WRITE (6,10)	BM	រី
	00 1 K=1,21	81	
	AX(K)=1.0	BN	- 6
۴.		BM	10
	DD 2 K=1,MF TARGET=K-1		
	IAKGE =K-1	BM	11
	TARGET=TARGET/FURD	BM	12
2	F(K)=IARGEI	BM	13
	READ (5-13) NSTAT	BM	14
-	IF (NSTAT) 9,7,3	BM	75
	IF (NSTAT-21) 4.4.B	BM	16

4	N=NSTAT	BM	17
	READ (5,14) (X(K),P(K),K=1,N)		18
	WRITE (A.111	BM	19
	WRITE (6.15) (K.X(K).P(K).K=1.N).	BM	20
•	NX=N	BM	21
	00 6 K≈l•Mf	BM	22
	TARGET=F(K)	BM	23
	CALL LINEAR (TARGET, X, NX, F1, F2, J1, J2, NOCON)	814	24
	IF (NOCON) 8.5.8	BM	25
	AX(K)=P(J1)*F1+P(J2)*F2	BM	26
,	CONTINUE	BM	27
,		AM	28
	WRITE (6,12) WRITE (6,15) (K,F(K),AX(K),K=1,MF) GETIDN	BM	29
	RETURN	81	30
	CALL BOMBER (BH STATIC ,5)	BM	31
	RETURN	BM	32
		BM	33
	CORMAN A CORM CONTROL STATES DOSSESSOS DESTRUCTION SACTORS	BM	-
0	FORMAT (/20X,43H INLET STATIC PRESSURE DISTRIBUTION FACTORS/)	BM	34
1	FORMAT (18X,5HINPUT,6X,4HR/RW,6X,11HPRES, FACT,/)		35
2	FORMAT 1/16x,8HCOMPUTED,5x,4HR/RW,6x,11HPRES. FACT./)	BM	36
3	FORMAT (1615)	BM	37
4	FORMAT (2612.0)	BM	3E
5 "	FORMAT (20X,15,2X,2F10.5)	ВМ	35
	END	BM	40
	SUBROUTINE STORE	BN	1
	COMMON /ABLE/ AX(21)	BN	2
_	COMMON /APE/ KITLE.LABEL(19)	BN	3
	COMMON /COUNT/ L.LL	BN	4
	COMMON /CPDATA/ TGFH(40)	BN	-
	COMMON /DELTAS/ DX,DY,DT,BY2,DT2,0T4	BN	6
	-COMMON /DUPER/ HA(21) -HB(21)	BN	_
	COMMON /EROS/ W(21.60.4).P(21.60)		ě
	COMMON /EROS/ W121.60.41.P121.601 COMMON /FANG/ F19.41.G19.41	BN	
	COMMON /FLIGHT, WEIGHT, PTHROT, PANIC	BN	10
		BN	·ii
	COMMON /FRAN/ AC(60),AI(60),BD(60),BI(60)	-	
	COMMON /FUBAR/ F1,F2,F3,F4,F5	BN	12
	COMPON /FURD/ WMP(4), WMM(4), WNP(4), WMM(4), WMM(4)	BN	13
	COMMON /LIMITS/ VMIN	BN	14
	COMMON /NAVIER/ DTDX.DTDX2,0TDX4,0TDXB,DTDY.DTDY2,DTDY4,DTDY8	BN	15
	COMMON /NERD/ MF.NF.NT.MUFF.LIMIT.NASTY	BN	16
	COMMON /NITWIT/ CLOWN.VULGAR	BN	17
	COMMON /SPOR/ 5160),50(60),50P(60),51(60),51P(60),AREA(60)	BN	16
	COMMON /SPY/ KCLASS.KGROUP	BN	-19
	COMMON /STAG/ AA(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21)	BN	20
	Ti.PZ(21).TZ(21).HZ(21).RHOZ(21)	BN	21
	COMMON /STOKES/ A(60),B(60),H(60)	BN	22
	COMMON /STUPID/ FOOL(21,60)	BN	2
	COMMON /SUPER/ R(21,60)	BN	24
	COMMON / THERMO/ RHFJ(7)	BN	2
	COMMON / TYME/ T.FLIT	BN	20
	COMMON /WORK/ XTRA(99)	BN	2
	COMMON /SKALE/ SIMPLE(4)	BN	21
	COMMON /PSIA/ PSIA(I6).NPSIA	BN	29
	COMMON /WALL/ XMALL[100] COMMON /SEXX/ NASTIE-IDIDY	BN	-30 -31

CDMMON /FLEX/ NFLX REWIND 9 WRITE (9) KITLE-LABEL-L-LL-TGFH-DX-DY-DT-DY2-DT2-DT4-MA-MB-W-P-F-G BN 1-WEIGHT-PTHRDT-PANIC-F1-F2-F3-F4-F5-WMP, WMM, WNP, WMM, WNN. DTDX-DTDX2 BN 2-DTDX4-DTDX8-DTDY-DTDY2-DTDY4-DTDY8-MF-NF-NT-MUFF-LIMIT-NASTY-CLOW BN 3N, VULGAR-S-SO-SOP-SI-SIP-AREA-KCLASS-KGROUP-AA-CP-CV-MTM-GAMZ-RGAS BN 4-P2-TZ-HZ-RHDZ-A-B-H-FOOL-R-RHF-IT-FLIT-XTRA-PSIA-NPSIA-SIMPLE-XWA BN 5LL-VMIN-AX-WASTIE-IDIDT-FPRAT-PBDUND, NANKER, INDEX-NFLX-AO, AI-BO-BI BN EMD FILE 9 REWIND 9 REWIND 9 RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE-LABEL-L-LL-TGFH-OX-DY-DT-DY2-DT2-DT4-HA-HB-N-P-F-G-BN DEIGHT-PTHROT-PANIC-F1-F2-F3-F4-F5-WMP-WMM, WNP-WNN-WMN-DTDX-DTDX2-BN 20TDX4-DTDX8-DTDY-DTDY2-DTDY4-DTDY8-MF-NT-MUFF-LIMIT-NASTY-CLOWN BN 3, VULGAR-S-SO-SOP-SI-SIP-AREA-KCLASS-KGROUP-AA-CP-CV-MTM-GAMZ-RGAS-BN 4PZ-TZ-HZ-RHOZ-A-B-H-FOOL-R-RHFJ-T-FLIT-XTRA-PSIA-NPSIA-SIMPLE-XWAL BN REWIND 9 WRITE (6-13) REWIND 9 WRITE (6-13) REWIND 9 WRITE (6-13) RETURN EITRY FREEP IF (FPRAT) 2-1-2 BN CONTINUE NEWP-NANKER ONE=1-0 CALL HEAD6 WRITE (6-1) (K-SO(K)-SOP(K)-K=1-NF) BN CALL HEAD6 WRITE (6-19) BN WRITE (6-19) BN WRITE (6-9)	34 35 36 37 38 39 40 42 43 445 45 46 47 48 49 50 51 52 53 55 56 57 58 60 61
## ITE (9) KITLE-LABEL, L, LL, TGFH, DX, DY, DT, DY2, DT2, DT4, MA, MB, W, P, F, G 1	36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 60 61
TWEIGHT.PTHROT.PANIC.F1,F2.F3,F4.F5,WMP,WMM,WNP,WNM,DTDX,DTDX2	37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 60 61
2,0T0X4,DT0X8,DT0Y,DT0Y2,DT0Y4,DT0Y8,MF,NF,NT,MUFF,LIMIT,NASTY,CLOW BN 3N,VULGAR,S,SO,SOP,SI,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,MTN,GAMZ,RGAS BN 4,PZ,TZ,HZ,RHDZ,A,B,H,FOOL,R,RHFJ,TT,FLIT,XTRA,PS1A,NPS1A,SIMPLE,XMA BN 5LL,VMIN,AX,NASTIE,IDIDT,FPRAT,PBDUND,NANKER,INDEX,NFLX,AD,AI,BO,BI BN EMD FILE 9 REMIND 9 RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE,LABEL,L,LL,TGFH,OX,DY,DT,DYZ,DTZ,DT4,HA,HB,N,P,F,G,BN 1WEIGHT,PTHROT,PANIC,F1,FZ,F3,F4,F5,HMP,HMM,HNP,HNM,HMN,OTDX,DTDXZ,BN 2OTOX4,DTDX8,DTDY,DTDYZ,DTDY4,DTDY8,MF,NF,NT,MUFF,LIMIT,NASTY,CLOWN BN 3,VULGAR,S,SD,SDP,ST,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,HTM,GAMZ,RGAS,BN 4PZ,TZ,HZ,RHDZ,A,B,H-FOOL,R,RHFJ,T,FLIT,XTRA,PSIA,NPSIASIMPLE,XWAL BN SL,VMIN,AX,NASTIE,IDIOT,FPRAT,PBOUND,NANKER,INDEX,NFLX,AO,AI,BO,BI BN REWIND 9 WRITE (6,13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN 2 CONTINUE NEWP=NANKER DNE=100 CALL HEAD6 WRITE (6,11) (K,SOIK),SOPIK),K=1,NF) BN CALL HEAD6 WRITE (6,9)	38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 55 56 60 61
2,0T0X4,DT0X8,DT0Y,DT0Y2,DT0Y4,DT0Y8,MF,NF,NT,MUFF,LIMIT,NASTY,CLOW BN 3N,VULGAR,S,SO,SOP,SI,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,MTN,GAMZ,RGAS BN 4,PZ,TZ,HZ,RHDZ,A,B,H,FOOL,R,RHFJ,TT,FLIT,XTRA,PS1A,NPS1A,SIMPLE,XMA BN 5LL,VMIN,AX,NASTIE,IDIDT,FPRAT,PBDUND,NANKER,INDEX,NFLX,AD,AI,BO,BI BN EMD FILE 9 REMIND 9 RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE,LABEL,L,LL,TGFH,OX,DY,DT,DYZ,DTZ,DT4,HA,HB,N,P,F,G,BN 1WEIGHT,PTHROT,PANIC,F1,FZ,F3,F4,F5,HMP,HMM,HNP,HNM,HMN,OTDX,DTDXZ,BN 2OTOX4,DTDX8,DTDY,DTDYZ,DTDY4,DTDY8,MF,NF,NT,MUFF,LIMIT,NASTY,CLOWN BN 3,VULGAR,S,SD,SDP,ST,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,HTM,GAMZ,RGAS,BN 4PZ,TZ,HZ,RHDZ,A,B,H-FOOL,R,RHFJ,T,FLIT,XTRA,PSIA,NPSIASIMPLE,XWAL BN SL,VMIN,AX,NASTIE,IDIOT,FPRAT,PBOUND,NANKER,INDEX,NFLX,AO,AI,BO,BI BN REWIND 9 WRITE (6,13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN 2 CONTINUE NEWP=NANKER DNE=100 CALL HEAD6 WRITE (6,11) (K,SOIK),SOPIK),K=1,NF) BN CALL HEAD6 WRITE (6,9)	39 40 41 43 44 45 46 47 48 49 50 51 52 53 54 55 55 56 60 61
4,PZ,TZ,HZ,RHDZ,A,B,H,FOOL,R,RHFJ,T,FLIT,XTRA.PSIA,NPSIA,SIMPLE,XWA BN SLL,VMIN,AX,NASTIE,IDIDT,FPRAT,PBOUND,NANKER,INDEX,NFLX,AD,AI,80,8I BN EMD FILE 9 REWIND 9 REWIND 9 RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE,LABEL,L,LL,TGFH,OX,DY,DT,DYZ,DTZ,DT4,HA,HB,W,P,F,G,BN 1WEIGHT,PTHROT,PANIC,F1,F2,F3,F4,F5,WMP,WMM,WMN,WMN,DTDX,DTDX2,BN 20TDX4,DTDX8,DTDY,DTDY2,DTDY4,DTDY8,MF,NF,NT,MUFF,LIMIT,NASTY,CLOWN AN 3,VULGAR,S,SD,SDP,ST,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,WTM,GAMZ,RGAS,BN 4PZ,TZ,MZ,RHOZ,A,B,H,FOOL,R,RHFJ,T,FLIT,XTRA,PSIA,NPSIA,SIMPLE,XWAL BN 5L,VMIN,AX,MASTIE,IDIOT,FPRAT,PBDUND,NANKER,INDEX,NFLX,AD,AI,BO,BI BN REWIND 9 WRITE (6,13) RETURN 1 RETURN 2 CONTINUE BN CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) CALL HEAD6 WRITE (6,9) BN CALL HEAD6 WRITE (6,9)	40 41 42 44 45 46 47 48 49 50 51 52 53 55 56 57 58 60 61
SLL, VMIN, AX, NASTIE, IDIDT, FPRAT, PBDUND, NANKER, INDEX, NFLX, AD, AI, 80, BI 8N EMD FILE 9	41 42 43 45 46 47 48 49 50 51 52 53 54 55 56 57 58 60 61
SLL, VMIN, AX, NASTIE, IDIDT, FPRAT, PBDUND, NANKER, INDEX, NFLX, AD, AI, 80, BI 8N EMD FILE 9	42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 60 61
EMD FILE 9 REWIND 9 WRITE (14,12) RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE, LABEL, L, L, TGFH, OX, DY, DT, DY2, DT2, DT4, MA, HB, W, P, F, G, BN 1WEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WNP, WNM, WMN, DTDX, DTDX2, BN 2OTDX4, DTDX8, DTDY, DTDY2, DTDY4, DTDY8, MF, NF, NT, MUFF, LIMIT, NASTY, CLOWN BN 3, VULGAR, S, SD, SOP, SI, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAM2, RGAS, BN 4PZ, TZ, HZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN SL, VHIN, AX, MASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NFLX, AO, AI, BO, BI RETURN ENTRY FREEP IF (FPRAT) 2,1,2 CONTINUE NEWPENANKER ONE=1,0 CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) BN CALL HEAD6 WRITE (6,9) BN CALL HEAD6 WRITE (6,9)	42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 60 61
REWIND 9 WRITE (14,12) RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE, LABEL, L, LL, TGFH, OX, DY, DT, DY2, DT2, DT4, MA, MB, W, P, F, G, BN WRITE (6,12) READ (9) KITLE, LABEL, L, LL, TGFH, OX, DY, DT, DY2, DT2, DT4, MA, MB, W, P, F, G, BN WRITE (BHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WMP, WMM, WMH, DTDX, DTDX2, BN 20TDX4, DTDX8, DTDY, DTDY4, DTDY4, DTDY8, MF, NT, IMIT, NASTY, CLOWN BN 3, VULGAR, S, SD, SDP, SI, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAM2, RGAS, BN 4P2, T2, MZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE XWAL, BN 5L, VHIN, AX, WASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NFLX, AO, AI, BO, BI REWIND 9 WRITE (6,13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN BN CONTINUE NEWP=NANKER ONE=1,0 CALL HEAD6 WRITE (6,11) (K, SO(K), SOP(K), K=1, NF) CALL HEAD6 WRITE (6,9) BN BN BN CALL HEAD6 WRITE (6,9)	43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 60 61
WRITE (14,12)	44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 60 61
RETURN ENTRY RESTOR REWIND 9 READ (9) KITLE-LABEL, L, LL, TGFH, OX, DY, DT, DY2, DT2, DT4, HA, HB, W, P, F, G, BN 1WEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WMP, WMM, WMN, DTDX, DTDX2, BN 2OTDX4, DTDX8, DTDY, DTDY2, DTDY4, DTDY8, MF, NF, NT, MUFF, LIMIT, NASTY, CLOWN BN 3, VULGAR, S, SD, SDP, ST, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAM2, RCAS, BN 4PZ, TZ, HZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN 5L, VMIN, AX, MASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NFLX, AO, AI, BO, BI REWIND 9 WRITE (6,13) RETURN BN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN 2 CONTINUE BN ONE=1,0 CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) BN CALL HEAD6 WRITE (6,9) BN BN BN BN BN BN BN BN BN BN BN BN BN	45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60
ENTRY RESTOR REWIND 9 READ (9) KITLE, LABEL, L, L, TGFH, OX, DY, DT, DY2, DT2, DT4, MA, HB, W, P, F, G, BN 1WEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WNP, WNM, MMN, DTDX, DTDX2, BN 2OTDX4, DTDX8, DTDY, DTDY2, DTDY4, DTDY8, MF, NF, NT, MUFF, LIMIT, NASTY, CLOWN BN 3, VULGAR, S, SD, SOP, SI, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAM2, RGAS, BN 4PZ, TZ, HZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN REWIND 9 WRITE (6, 13) RETURN ENTRY FREEP IF (FPRAT) 2, 1, 2 BN CALL HEAD6 WRITE (6, 11) (K, SO(K), SOP(K), K=1, NF) CALL HEAD6 WRITE (6, 9) BN CALL HEAD6 WRITE (6, 9)	46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61
REWIND 9 READ (9) KITLE; LABEL, L, LL; TGFH, OX, DY, DT, DY2, DT2, DT4, HA, HB, W, P, F, G, BN INEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WHP, WHM, WNP, WNM, WHN, DTDX, DTDX2, BN 20TDX4, DTDX8, DTDY, DTDY2, DTDY4, DTDY8, MF, NF, NT, MUFF, LIMIT, NASTY, CLGWN BN 3, VULGAR, S, SD, SDP, ST, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WYM, GAM2, RGAS, BN 4PZ, TZ, HZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN SL, VHIN, AX, NASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NFLX, AO, AI, BO, 8I REWIND 9 WRITE (6, 13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 BN CONTINUE NEWPENANKER ONE=1,0 CALL HEAD6 WRITE (6, 11) (K, SO(K), SOP(K), K=1, NF) BN CALL HEAD6 WRITE (6, 9)	47 48 49 50 51 52 53 54 55 56 57 58 59 60 61
READ (9) XITLE, LABEL, L, LL, TGFH, OX, DY, DT, DY2, DT2, DT4, MA, HB, W, P, F, G, BN 1WEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WNP, WNM, WMN, DTDX, DTDX2, BN 2OTDX+, DTDX8, DTDY2, DTDY4, DTDY8, MF, NF, NT, MUFF, LIMIT, NASTY, CLOWN BN 3, VULGAR, S, SD, SDF, SI, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAM2, RGAS, BN 4PZ, TZ, HZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN 5L, VMIN, AX, NASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NFLX, AO, AI, BO, BI REWIND 9 WRITE (6,13) RETURN BN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN CONTINUE NEWP=NANKER ONE=1,0 BN CALL HEAD6 WRITE (6,13) (K, SO(K), SOP(K), K=1, NF) CALL HEAD6 WRITE (6,9)	48 49 50 51 52 53 54 55 56 57 58 59 60 61
NEIGHT, PTHROT, PANIC, F1, F2, F3, F4, F5, WMP, WMM, WNP, WNM, WMN, DTDX, DTDX2, BN 20TDX4, DTDX8, DTDY2, DTDY4, DTDY8, MF, NF, NT, MUFF, LIMIT, NASTY, CLOWN BN 3, VULGAR, S, SD, SDP, SDP, SAREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAY2, RGAS, BN 4PZ, TZ, MZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FLIT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN 5L, VMIN, AX, WASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NHLX, AO, AI, BO, BI 8N REWIND 9 BN WRITE (6,13) BN RETURN BN ENTRY FREEP BN IF (FPRAT) 2,1,2 BN 1 RETURN	49 50 51 52 53 54 55 56 57 58 59 60 61
20TDX4,DTDX8,DTDY,DTDY2,DTDY4,DTDY8,MF,NF,NT,MUFF,LIMIT,NASTY,CLOWN AN 3,VULGAR,S,SO,SOP,SI,SIP,AREA,KCLASS,KGROUP,AA,CP,CV,WTM,GAMZ,RCAS, BN 4PZ,TZ,HZ,RHOZ,AB,H,FOOL,R,RHFJ,T,FLIT,XTRA,PSIA,NPSIA,SIMPLE,XWAL BN 5L,VMIN,AX,NASTIE,IDIOT,FPRAT,PBOUND,NANKER,INDEX,NFLX,AO,AI,BO,8I BN REWIND 9 WRITE (6,13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN 2 CONTINUE BN NEWP=NANKER ONE=1.0 BN CALL HEAD6 WRITE (6,13) (K,SO(K),SOP(K),K=1,NF) BN CALL HEAD6 WRITE (6,9)	50 51 52 53 54 55 56 57 58 59 60 61
3, VULGAR, S, SD, SDP, ST, SIP, AREA, KCLASS, KGROUP, AA, CP, CV, WTM, GAMZ, RGAS, BN 4PZ, TZ, MZ, RHOZ, A, B, H, FOOL, R, RHFJ, T, FL LT, XTRA, PSIA, NPSIA, SIMPLE, XWAL BN 5L, VHIN, AX, WASTIE, IDIOT, FPRAT, PBOUND, NANKER, INDEX, NFLX, AO, AI, BO, BI BN REWIND 9 WRITE (6,13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 BN 1 RETURN 2 CONTINUE BN NEWP=NANKER ONE=1.0 BN CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) BN CALL HEAD6 WRITE (6,9) BN	51. 52 53 54 55 56 57 58 59 60 61
4PZ,TZ,HZ,RHOZ,A,B,H,FOOL,R,RHFJ,T,FLIT,XTRA,PSIA,NPSIA,SIMPLE,XWAL BN 5L,VMIN,AX,MASTIE,IDIOT,FPRAT,PBOUND,NANKER,INDEX,NFLX,AO,AI,BO,BI BN REWIND 9 WRITE (6,13) RETURN ENTRY FREEP IF (FPRAT) 2,1,2 1 RETURN 2 CONTINUE NEWPENANKER ONE=1.0 CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) CALL HEAD6 WRITE (6,9) BN BN BN BN BN BN BN BN BN BN BN BN BN	52 53 54 55 56 57 58 59 60 61
SL, VMIN, AX, WASTIE, IDIOT, FPRAT, PROUND, NANKER, INDEX, NFLX, AO, AI, BO, BI BN REWIND 9 BN WRITE (6,13) BN RETURN AN ENTRY FREEP BN IF (FPRAT) 2,1,2 BN IRETURN BN CONTINUE BN ONE=1.0 BN ONE=1.0 BN CALL HEAD6 BN WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) BN BN URITE (6,9) BN BN URITE (6,9) BN BN BN URITE (6,9) BN BN BN URITE (6,9) BN BN BN BN URITE (6,9) BN BN BN BN BN BN BN BN BN BN BN BN BN	53 54 55 56 57 58 59 60 61
REWIND 9 WRITE (6,13) RETURN RETURN FITTY FREEP IF (FPRAT) 2,1,2 1 RETURN 2 CONTINUE NEWP=NANKER ONE=1.0 BN CALL HEAD6 WRITE (6,13) (K,SO(K),SOP(K),K=1,NF) BN CALL HEAD6 WRITE (6,9) BN BN BN BN BN BN BN BN BN BN BN BN BN	54 55 56 57 58 59 60 61
WRITE (6,15) BN RETURN BN ENTRY FREEP BN IF (FPRAT) 2,1,2 BN RETURN BN RETURN BN CONTINUE BN BN CONTINUE BN CONTINUE BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN BN CALL HEAD6 BN CAL	55 56 57 58 59 60 61
RETURN ENTRY FREEP IF (FPRAT) 2,1,2 RETURN CONTINUE NEWP=NANKĒR ONE=1.0 CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) CALL HEAD6 WRITE (6,9) BN BN BN BN BN BN BN BN BN B	56 57 58 59 60 61
ENTRY FREEP IF (FPRAT) 2,1,2 RETURN CONTINUE NEWP=NANKER ONE=1.0 CALL HEAD6 WRITE (6,11) (K,SO(K),SOP(K),K=1,NF) CALL HEAD6 WRITE (6,9) BN HRITE (6,9) BN BN BN BN BN BN BN BN BN B	57 58 59 60 61
IF (FPRAT) 2,1,2	58 59 60 61
1 RETURN BN 2 CONTINUE BN NEWP=NANKËR BN ONE=1.0 BN CALL HEAD6 WRITE (6.11) (K.SO(K).SOP(K).K=1.NF) BN CALL HEAD6 WRITE (6.9) BN	59 60 61
1 RETURN BN 2 CONTINUE BN NEWP=NANKER BN ONE=1.0 BN CALL HEAD6 BN WRITE (6.11) (K,SQ(K),SQP(K),K=1,NF) BN CALL HEAD6 BN WRITE (6.9) BN	. 60 61
NEWP=NANKER	61
NEWP=NANKER	
ONE=1.0 BN CALL HEAD6 WRITE (6.11) (K,SO(K),SOP(K),K=1,NF) CALL HEAD6 WRITE (6.9) BN	
CALL HEADS WRITE (6.11) (K,SO(K),SOP(K),K=1,NF) CALL HEADS WRITE (6.9) BN WRITE (6.9)	62
WRITE (6,11) (K,SQ(K),SQP(K),K=1,NF) CALL HEAD6 BN WRITE (6,9)	- 66-
CALL HEAD6 . BN	64
WRITE (6.9)	65
4K11E 10171 . DN	66
The state of the s	
DD 3 K=YEHP, NF	67
RHD=W(MF,K,1)/R(MF,K) 9N	68
U=W(MF,K,2)/W(MF,K,1)	69
V=N(NF,K,3)/W(MF,K,1) BN	70
PX=P(MF,K)	71
CALL FREAK (PX,RHA,U,V,MF,K;PD,TD,DEG,T,XM,VEL,GAM) BN	72
BETA=(XM+ONF)*(XM-DNE)	73
BET4=ABS(4ETA) BN	74
BETA=SQRTF(BETA) BN	75
DP = PX - PBDUND(K)	
DGNU=DP+BETA/(RHO+VEL+VEL)" BN	77
SOP(K)=SOP(K)+DGNI) BN	76
WRITE 16,10) PX,RHD,VEL,XM,BETA,DP,DGNU,K	79
3 CONTINUE BN	80
SOP (NEWP) = AHIN1 (SOP (NEWP), SOP (NEWP+1)) 8N	81
SP24=SOP(NENP)	82
SPLOW=0.5*SDP(NEWP-1)+0.5*SOP(NEWP+1)	
	84
SPHIG=0.1*SOP(NEWP-1)+0.9*SOP(NEWP+1)	
TEST=(SP24-SPLON)*(SPLDH-SPHIG)	
IF (TEST) 5,5,4 BN	86
4 SOPINEWPY=SPCOW BN	
GO TO 7 BN	87 88

5	TEST=(SP24-SPHIG)+(SPHIG-SPLOW)	BN	89
	IF (TEST) 7.7.6	BN	90
6	SOP (NEWP) = SPHIG	BN	91
7	CONTINUE	BN	92
	WRITE (6,11) (K,SO(K),SOP(K),K=1,NF)	BN	93
	DINGLE=DX+0.5	BN	94
	DO R K=NEWP.NF	BN	95
	SO(K)=SO(K-1)+DINGLE+(SOP(K-1)+SOP(K))	BN	96
_	CONTINUE	BN	41
	CALL HOAX	BN	98
	RETURN	BN	99
<u> </u>		BN	100
)	FORMAT (/21x, PSFA 11x, RHO 12x, VEL 10x, MACH NO. 18x, BETA 1	AN	101
	111x, D-PRES', 8x, D-PMA'/)	AN	102
ō-	FORMAT (10x,F15.2,E15.5,F15.2,F15.4,F15.5,F15.2,F15.5,18)	BN	103
ī	FORMAT (20X-(5-5X-2F15-5)	_	104
ž	FORMAT ('1', 20%, 'STORED ON NINE' /)	_	105
3	FORMAT ('1',ZOX, 'RESTORED FROM NINE'/)		106
	END	BN	107
	SUBROUTING STREAM	80	1
	COMMON /EROS/ W(21,60,5)	BO	2
	COMMON /NERD/ MF.NF.NT	AO	3
	COMMON /STUP(D/ F(21.60)	BO	4
	DO 3 NX=1,NF	BO	5
	F(1.NX)=0.0	BO	- 6
	00 1 K=2.MF	80	ž
			-
L	F(K,NX)=F(K-1,NX)+0.5*(W(K-1,NX,2)+W(K,NX,2))	80	8
_	00 2 K=1+MF	80	9
2 -	F(K,NX)=F(K,NX)/F(MF,NX)	BO	10
3	CONTINUE	30	11
	RETURN	60	12
	END	BO	13
	SUBROUTINE TRICKY	BP	ĭ
			_
	COMMON /EROS/ W(21,60,4),P(21,60)	AP	2
	COMMON /NDEX/ INDEX(9)	BP	3
	COMMON /COUNT/ L.EL	BP	
	COMMON · / NERD / ME , NF , NY	BP	3
	COMMON /STAG/ A(8,21),CP(3,21),CV(3,21),WTM(21),GAMZ(21),RGAS(21),	BP	6
	1P2(21),TZ(21),HZ(21),RHOZ(21)	BP	- 7
	DINENSION X(9) + Y(9)	BP	8
	IF (L) 2.1.2	BP	9
		_	_
	WRITE (14,6) INDEX	AP	10
	CONTINUE	BP	11
	nn 3 K=1,9	BP	12
	J=INDEX(K)	AP	13
	X(K)=P(MF,J)/PZ(MF)	BP	14
-	Y(K)=P(1,J)/PZ(1)	BP	15
1	CONTINUE	BP	16
	WRITE (14,4) X.L	8P	17
	WRITE (14,5) Y	AP	18
	RETURN	BP	19
;		BP	20
	FORMAT (1x,9F12.4,18)	AP	21
•			
5	FURMAT (7X.9F12.4)	BP	22
5	FORMAT (7X,9F12.4) FORMAT (/20X,30H(P/PO) WALL/AX(S RESPECTIVELY//1X,9(12/)	BP	- 22 23

	SUBROUTINE TROPIC (PO.TO.PSYAT.F.DEN.VEL.EASY)	80	
	COMMON_/STAG/_A(8,21),CP(3,21),CV(3,21),HTM(21),GAMZ(21),RGAS(21),	80	
	1P2(21),T2(21)	BO	
	COMMON /THERMO/ CPX(3).CVX(3).RAG	80	
	COMMON /LIMITS/ VMIN	80	
	2ERO=0.0	90	
	PO=PO	BQ	Τ
	10=10	80	
	PEPSTAT	BΩ	
	FUZZ=F	BQ	
	PRAT=P/PO	BO	
	T=HANKY(CPX,PRAT,TO,RAG)	BO	
	RHD=P/(T*RAG)	BQ	_
	DEN=RHD	80	
	DH=HOTS(CPX.T.TO)	80	
	VELOC=SORTF(DH+DH)	80	
	VELOC = AMAXI (VELOC , VMIN)	BQ	
	VEL=VELOC	BO	
	HO=HZERO(FUZZ)	BO	_
	E=I(I)*RHO-P	BO	
	FASYEE	BO	
	RETURN	BQ	
	END	BO	
	FUNCTION TSTAG (CP.TSTAT.YSQR)	BR	
	DIMENSION CP(3)	BR	_
	T=TSTAT	BR	
	W=VSQR +0.5	BR	
	A=CSUBP(TSTAT)	BR	
	T2=T+W/A	BR	-
	00 1 K=1.5	BR	
	H=HOTS(CP,T,TZ)	BR	_
	FRROR=W-H	BR	
	FDT7=C SUBDITT	BR	-
	DT=ERROR/CPT2	BR	
	T2=T2+DT	BR	-
1	CONTINUE	BR	
<u></u>		BR	_
	RETURN	5R	
	END	BR	
	SUBROUTINE WEIRDO	85	
	COMMON /EROS/ W(21.60.4).P(21.60)	BS	
	COMMON /NERD/ M.N.NT.MUFF, LIMIT.NEWKY	RS	
		B5	_
	DO 3 I=1.NEWKY		
	K2M-1	BS	
	OO 2 J=2.LIMIT	BS	
	NO 1 L=1,4	BS	_
1	W(K,J,L)=H(K-1,J-1,L)	RS	
2	CONTINUE	BS	
3	CONTINUE	B5	
	DO 5 K=2.MUFF	BS	
	00 4 J=2.LIMIT	BS	
<u> </u>	P(K+J)=PNTS(H(K+J+1)+H(K+J+4)+K+J)	95	
5	CONTINUE	BS	
	RETURN	AS	
	END	B 5	_

	COMMON /EROS/ H(21.60,4),P(21,60)	BT	2
	COMMON /NERD/ MF.NF.NT.MUFF	BT	3
	COMMON /SPOR/ S(60)	BT	4
	K=NXST#	BT	5
	SUM=(W(1.K.2)+W(MF,K.2))+0.5	BT	6
551	OO 1 J=2,MUFF	BT	7
1	SUM=SUM+W{J,K,2}	8T	8
	XMASS=SUM+S(K)	BT	9
	RETURN	BT	10
	END	BT	11-
	BLOCK DATA	BU	1
	COMMON /CPDATA/ CP(3.8),WTM(8),NAME(8)	BU	2
7	CP COEFFICIENTS FOR EACH CHEMICAL SPECIE	RU	_3_
C	UNITS OF BTU/LB.MASS	BU	4
	TATA CP/0.231800.1.040000E-05.7.166000E-09.0.120765.1.720251E-04	BU	5
	14.235305E-08.0.2615315.179134E-05.1.0750BE-07.0.430062.1.676842E	BU	6
	~~~05,2~778587E-08,0~190481,5.646879E-05,-9.812500E-09,0.246445,-3.5	BU	7
	364750E-06,1.251100E-08,0.124349,0.0,0.0,3.22600,1.757600E-04,1.0E-	AU	8
	408/	BU	9
	DATA WTM/28.97,44.011,28.011,18.016,32.000,28.000,39.944,2.016/	BU	10
	DATA NAME/ AIR , CO2', CO', H20', OZ', N2', A', H2'/	BU	11
	ENO	BU	12-

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An analytical technique based on the time-dependent flow equations

An analytical technique based on the time-dependent flow equations has been developed to predict the inviscid transonic flow field in axisymmetric propulsion nozzles. The analysis includes the treatment of axisymmetric nonuniform nozzle inlet profiles of total pressure, total temperature, specific heat, and molecular weight. The analysis is also capable of considering convergent-divergent, convergent, and shrouded or unshrouded plug nozzle geometries. A computer listing and three sample calculations are presented to illustrate some of the capabilities of the program.

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